"TRADER" SERVICE SHEET

PITTED with self-contained frame aerials, the Pye P78 is a 3-valve (plus rectifier) 2-band transportable superhet designed to operate from A.C. mains of 200-250 V, 40-100 c/s. The waveband ranges are 187-560 m and 1,000-

Release date and original price: September 1953; £12 14s 5d. Purchase tax extra.

CIRCUIT DESCRIPTION

Tuned frame aerial input by L1, C28 (M.W.) or L1, L2, C28 (L.W.) to triode hexode valve (V1, Mullard ECH42) which operates as frequency changer with in-ternal coupling. Provision is made for the connection of an external aerial and earth, the aerial being coupled to the tuned circuits via the common impedance of C2.

Oscillator anode coils L4 (M.W.) and L5 (L.W.) are tuned by C30. Parallel trimming by C29 (M.W.) and C11 (L.W.); series tracking by C9 (M.W.) and C10 (L.W.). Reaction coupling across the

common impedance of the trackers with additional coupling on M.W. via L3.

Second valve (V2, Mullard EBF80) is a double diode R.F. pentode, its pentode section operating as intermediate frequency amplifier with tuned transformer

A.C. Transportable Superhet

couplings C5, L6, L7, C6 and C15, L8, L9,

Intermediate frequency 470 kc/s

One diode section of V2 operates as signal detector, the audio frequency component in its rectified output being developed across volume control R13 and passed via C19 to grid of V3a (triode section of V3, Mullard ECL80).

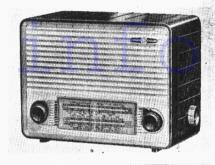
Second diode of V2 is fed from V2 pentode anode via C14, and the resulting

D.C. potential, developed across R7, is

(Continued col. 1 overleaf)

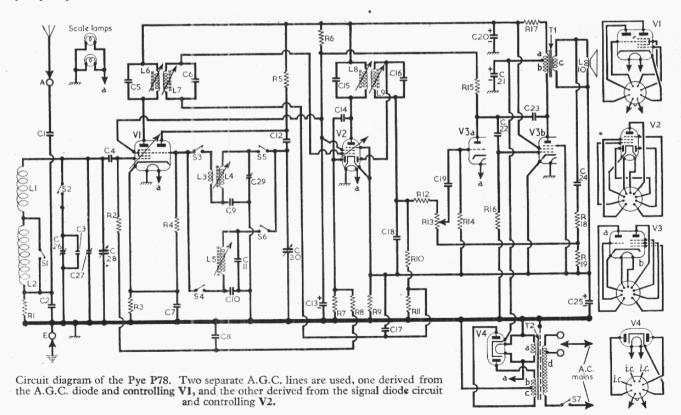
COMPONENTS AND VALUES

RESISTORS		Values	Loca- tions
R1 R2 R3 R4 R5 R6 R7 R8 R9 R10	Aerial shunt V1 C.G. V1 G.B. V1 osc. C.G. Osc. anode load S.G. H.T. feed A.G.C. dtode load A.G.C. decoupling V2 G.B. A.G.C. pot. divider A.G.C. pot. divider	$\begin{array}{c} 22 k \Omega \\ 2 \cdot 2 M \Omega \\ 2 \cdot 20 \Omega \\ 47 k \Omega \\ 47 k \Omega \\ 22 k \Omega \\ 1 M \Omega \\ 1 M \Omega \\ 330 \Omega \\ 2 \cdot 2 M \Omega \end{array}$	G3 F4 F4 G4 F4 E3 E3 F4 E3 F4
R11 R12 R13 R14 R15 R16 R17 R18 R19	I.F. stopper Volume control V3a C.G V3a anode load V3b C.G H.T. smoothing Neg. feed-back {	6·8ΜΩ 100kΩ 800kΩ 10ΜΩ 100kΩ 470kΩ 1·8kΩ 1kΩ 470Ω	F4 E3 D3 E3 E3 E4 E3 D3 E3



	CAPACITORS	Values	Loca- tions
C1 -) 4 1	470pF	G4
C2	Aerial couplers {	2,400pF	G3
Č3	L.W. aerial trim.	82pF	G3
C4	V1 C.G	100pF	G4
Č5) 1st I.F. trans.	$100 \mathrm{pF}$	B2
Č6	tuning	100pF	B2
Č7	V1 cath, by-pass	$0.04 \mu F$	G4
Č8	A.G.C. decoupling	$0.02 \mu F$	F4
Č9	M.W. osc. tracker	360pF	G3
C10	L.W. osc, tracker	180pF	F3
C11	L.W. osc, trimmer	200pF	G4
C12	Osc. anode coupling	100pF	G4
C13*	S.G. decoupling	$16\mu F$	B1
C14	A.G.C. coupling	$100 \mathrm{pF}$	E4
C15	2nd I.F. trans.	100pF	B2
C16	tuning	100pF	B2
C17	A.G.C. decoupling	$0.02 \mu F$	F4
C18	I.F. by-pass	470pF	E3
C19	A.F. coupling	$0.01 \mu F$	D3
C20*	1	$16\mu F$	B1
C21*	H.T. smoothing }	$16\mu F$	B1
C22	A.F. coupling	$0.01 \mu F$	E4
C23	1	100pF	F4
C24	Neg. feed-back {	$1.0 \mu F$	E3
C25*	V3 cath, by-pass	$50\mu F$	E3
C261	L.W. aerial trim.	50pF	F3
C271	M.W. aerial trim.	50pF	F3
C28†	Aerial tuning	528pF	A1
C291	M.W. osc, trimmer	50pF	F3
C30+	Oscillator tuning	528pF	A2

* Electrolytic. † Variable. ‡ Pre-set.



отн	ER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1	} Frame aerials {	3.0	A2
L_2)	20.0	A2
L3	M.W. osc. reaction	0.4	G3
L4	Oscillator tuning	2.0	G3
L_5	f coils	7.5	F3
L6	1st I.F. trans. { Pri.	10.0	$_{\rm B2}$
L7) (Sec.	10.8	B2
L8	2nd I.F. trans. { Pri.	10-0	B2
$_{\rm L9}$	(1500.	10.8	B2
L10	Speech coil	2.5	According to
	(a	5.0	
T1	O.P. trans. < b	465.0	B1
	le		
	(a		
T2	Mains b	150.0	C2
12	trans) c	160.0	
	d, total	56.0	
S1-S6	Waveband switches		G3
S7	Mains sw., g'd R13		D3

Circuit Description-continued.

fed back as bias to V1, giving automatic gain control. A second source of A.G.C. voltage is obtained from the signal diode circuit via potential divider R10, R11, and is fed as bias to V2.

Resistance-capacitance coupling by R15, C22 and R16 between V3a and pentode output valve (section b of V3). Tone correction is obtained via two negative feedback paths, one between the anodes of V3b and V3a via C23, and the other between TI secondary circuit and the volume control via potential divider C24, R18,

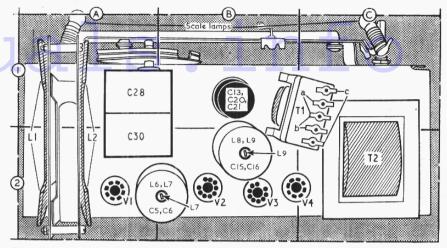
H.T. current is supplied by full-wave I.H.C. rectifier (V4, Mullard EZ40). Smoothing by R17 and electrolytic capacitors C20, C21. Residual hum is neutralized by passing H.T. current through section a of TI primary winding.

CIRCUIT ALIGNMENT

As the tuning scale is fixed in the cabinet, the following adjustments should be carried out with the chassis in the cabinet. All the adjustments are made easily accessible upon the removal of the cabinet back and base covers.

1.F. Stages.—Switch receiver to M.W. and turn gang to maximum capacitance. Connect output of signal generator, via an $0.1 \, \mu\text{F}$ capacitor in each lead, to control grid (pin 6) of V1 and to chassis. Feed in a 470 kc/s (638.3 m) signal and adjust the cores of L9 (location reference B2), L8 (F3), L7 (B2) and L6 (F4) for maximum output. Repeat these adjustments until no further improvement results. improvement results.

R.F. and Oscillator Stages.—Transfer signal generator leads, with isolating capacitors, to A and E leads. Check that with gang at maximum capacitance the cursor coincides with the cali-



Plan view of chassis. The windings of the O.P. transformer are coded a, b, c here to agree with the markings in the circuit diagram overleaf.

ganged in chassis.

bration dot at the high wavelength end of the L.W. tuning scale.

bration dot at the high wavelength end of the L.W. tuning scale.

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the core of L4 (G3) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust C29 (F3) and C27 (F3) for maximum output. Repeat these adjustments until no further improvement results.

L.W.—Switch receiver to L.W., tune to 1,400 m, feed in a 1,400 m (214 kc/s) signal and adjust C26 (F3) and the core of L5 (F3) for maximum output.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those derived from the manufacturer's information. They were measured with the receiver operating from 210 V A.C. mains and tuned to a point at the high wavelength end of M.W. where there was no signal input. Voltage readings were taken on the 10 V and 250 V ranges of a Model 8 Avometer, classis being the negative connection in each case.

Valve	Anode		Screen		Cath.	
varve	v	mA	v	mA	v	
V1 ECH42	$\begin{cases} 197 \\ \text{Oscil} \\ 70 \end{cases}$	$\left\{\begin{array}{c} 2.0 \\ \text{lator} \\ 2.7 \end{array}\right\}$	90	3.3	1.7	
V2 EBF80	197	3.4	90	1.3	8.0	
V3 ECL80 {a	32	0.6			8.0	
V4 EZ40	218 204*	15.0	197	2.8	8:0 204:0	

* A.C. reading, each anode. † Cathode current, 31:1 mA.

Diagram of the waveband switch unit. In

the associated switch table below, a dash

indicates open, and C, closed.

GENERAL NOTES

Switches.—S1-S6 are the waveband switches, anged in a single rotary unit beneath the hassis. This is indicated in our underside



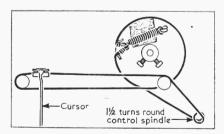
drawing of the chassis, and shown in detail in the small diagram above, where it is drawn as seen in the direction of the indicating arrow in the chassis illustration.

S7 is the Q.M.B. mains switch, ganged with the volume control R13.

Scale Lamps.—These are 6.5 V 0.3 A lamps with small clear spherical bulbs and M.E.S. bases.

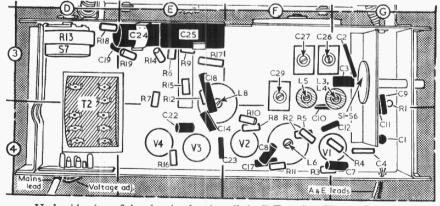
Dases.

Drive Cord Replacement.—Three feet of nylon-braided glass yarn is required for a new tuning drive cord, this length leaving an ample margin for tying off. It should be run as shown in the sketch below, where the system is drawn as seen when viewed from the front with the gang at minimum capacitance.



Sketch of the tuning drive system.

Printed in England by Cornwall Press Ltd., Paris Garden, London, S.E.1.



Underside view of the chassis, showing all the R.F. and oscillator adjustments.