"TRADER" SERVICE SHEET

	CAPACITORS	Values	Loca- tions
C1	Aerial and earth { isolators { Aerial series L.W. aerial shunt	0.005µF	H4
C2		0.01µF	H4
C3		50pF	H4
C4		800pF	G4
C5	S.W. aerial trim	20pF	H4
C6	L.W. aerial trim	60pF	G4
C7	V1 C.G	50pF	G4
C8	A.G.C. decoupling	0·1μF	G4
C10 C11 C12	} lst I.F. trans. tun- ing { V1 cath. by-pass V1 osc. C.G	110pF 110pF 0·05μF 45pF	B2 B2 G3 G4
C13	M.W. osc. tracker	556pF	G3
C14	L.W. osc. tracker	390pF	G3
C15	L.W. osc. trim	180pF	G3
C16	H.T. decoupling	0.05µF	G4
C17	A.G.C. decoupling	$0.05 \mu F \\ 0.05 \mu F \\ 0.05 \mu F \\ 110 p F$	G4
C18	V2 S.G. decoupling		G4
C19	H.T. decoupling		F4
C20	2nd I.F. trans.		C2
C21 C22 C23* C24	tuning { Cathode by-passes { I.F. by-pass	110pF 0.05µF 50µF 100pF	F4 F3 F4
C25	P.U. isolators { A.F. coupling A.G.C. coupling	0·005μF	H4
C26		0·1μF	F3
C27		0·01μF	F3
C28		50pF	F4
C29 C30 C31 C32	Tone corrector A.F. coupling Neg. feed-back {	$0.002 \mu F$ $0.01 \mu F$ $0.1 \mu F$ $0.05 \mu F$	F4 E4 E4
C34 C35	Part tone control	$0.05 \mu F$ $0.001 \mu F$ $0.01 \mu F$	E3 E4

H.T. Smoothing Mains R.F. filter ...

Aerial tuning ... Oscillator tuning ...

S.W. osc. trim. M.W. osc. trim. L.W. osc. trim.

C38

C39† C40†

C41: C42: 32μF 16μF

40pF 40pF 40pF

0.01 aF

C1 C1 D2 A2 A1 H3

G4

# BUSH DAC34

A.C./D.C. Transportable Superhet

THE Bush DAC34 is a 3-band 4-valve (plus rectifier) transportable table receiver, designed to operate from A.C. or D.C. mains of 200-250 V, 40-100 c/s in the case of A.C. The total mains consumption is approximately 35 watts. The waveband ranges are 16-50 m, 182-560 m and 833-2,068 m.

Release date and original price: August, 1953, £20 0s 3d. Purchase tax extra.

### CIRCUIT DESCRIPTION

Aerial input via coupling coils L2, L3, L4 to single-tuned circuits L5, C39 (S.W.) L6, C39 (M.W.) and L7, C39 (L.W.), which precede triode hexode valve (V1, Mullard UCH42)

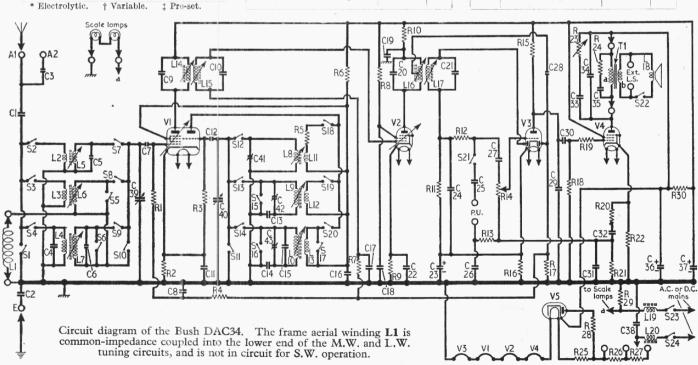
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		RESISTORS	Values	Loca- tions
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R1	V1 C.G	470kΩ	G4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R2		$220\Omega$	G4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R3	V1 osc. C.G	$47 \mathrm{k}\Omega$	G4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R4	A.G.C. decoupling	$1M\Omega$	F4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R5	Osc. stabilizer	$47\Omega$	H4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R6	H.T. feed	$15 \mathrm{k}\Omega$	G4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			$47 \mathrm{k}\Omega$	F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Signal diode load		F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R13		$47 \mathrm{k}\Omega$	F3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				$\mathbf{F4}$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		V4 C.G. stopper	$47 \mathrm{k}\Omega$	F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		)		$\mathbf{E4}$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Neg. feed-back		E4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		J_		E4
$ \left. \begin{array}{c} {\rm R25} \\ {\rm R26} \\ {\rm R27} \\ {\rm R27} \\ {\rm V5} \end{array} \right\} {\rm Heater\ ballast}  \dots \left\{ \begin{array}{c} {\rm 950\Omega} \\ {\rm 150\Omega} \\ {\rm 150\Omega} \\ {\rm D} \\ {\rm D} \\ {\rm 250\Omega} \\ {\rm D} \\ {\rm C} \\ {\rm D} \\ {\rm D} \\ {\rm C} \\ {\rm D} \\ {\rm $				E3
$ \left. \begin{array}{c} \overrightarrow{R26} \\ \overrightarrow{R27} \\ \overrightarrow{R28} \end{array} \right\} \begin{array}{c} \text{Heater ballast} & \dots \left\{ \begin{array}{c} 150\Omega \\ 150\Omega \\ \end{array} \right. \begin{array}{c} \overrightarrow{D} \\ \overrightarrow{D} \\ \overrightarrow{D} \end{array} $		Tone corrector		-
$\begin{bmatrix} R27 \\ R28 \end{bmatrix}$ V5 surge limiter $\begin{bmatrix} 150\Omega \\ 250\Omega \end{bmatrix}$ D		1 (		D2
R28 V5 surge limiter $250\Omega$ D		Heater ballast		D2
		J		D2
				D2
				D1
R30 H.T. smoothing $10k\Omega$ E	R30	H.T. smoothing	$10 \mathrm{k}\Omega$	E4

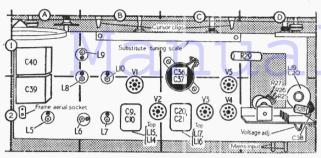
operating as frequency changer. Reception from an internal frame aerial L1 is provided on M.W. and L.W., the winding being connected in series with the chassis end of the two tuning coils.

Oscillator grid coils L8, L9 and L10 are tuned by C40. Parallel triming by C41 (S.W.), C42 (M.W.) and C43 (L.W.); series tracking by

(Continued col. 1 overleaf)

ОТЕ	ER COMPONENTS	Approx Values (ohms)	Loca tions
L1	Frame aerial	0.5	
L2	Aerial coupling		H4
$L_3$		0.6	G4
L4	Cons	32.0	G4
$L_5$	) (	-	H4
L6	Aerial tuning coils {	4.0	G4
L7		16.0	G4
$_{L8}$	Oscillator tuning	-	G3
L9	coils	$3 \cdot 2$	G3
L10	) coms (	4.0	G3
L11	Oscillator reaction	-	G3
L12	coils	0.6	G3
L13		1.5	G4
L14	1st I.F. trans. ${ Pri. \\ Sec. }$	12.5	B2
L15	Sec.	12.5	B2
L16	2nd I.F. trans. Sec. Sec. Sec.	12.5	C2
L17	Sec.	12.5	C2
L18	Speech coil	2.5	D2
L19 L20	Mains R.F. filters {	3.0	D2
L20		500·0	DZ
T1	O.P. trans. $\begin{cases} \mathbf{a} & \cdots \\ \mathbf{b} & \cdots \end{cases}$	0.5	-
81-	Waveband/gram.		
S21	switches	No. of Contrast	H4
S22	Speaker switch	MI 11 12 12	
323,			
S24	Mains sw., g'd R14		F3





Plan view of the chassis showing the substitute tuning scale referred to in "Circuit Alignment" below.

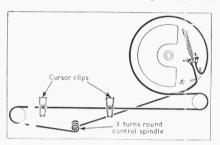
#### Circuit Description—continued

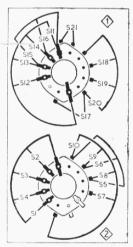
C13 (M.W.) and C14 (L.W.). Reaction coupling from anode by L11, L12 and L13.

Second valve (V2, Mullard UF41) is a variablemu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C9, L14, L15, C10 and C20, L16, L17, C21

Intermediate frequency 470 kc/s.

Diode signal detector is part of double diode triode valve (V3, Mullard UBC41). Audio fre-





Above: Sketch of the tuning drive cord system as seen from the front of the chassis.

Left: Diagrams of the waveband switch units, drawn as seen in the direction indicated by the arrows in the under - chassis illustration.

quency component in its rectified output

quency component in its rectified output is developed across load resistor R11, and passed via C27 and volume control R14 to grid of triode section. I.F. filtering by C24, R12 and the capacitance of the screened leads.

Second diode of V3 is fed from V2 anode via C28, and the resulting D.C. potential developed across load resistor R17 is fed back as bias to V1 and V2, giving automatic gain control.

Resistance-capacitance coupling by R15, C30 and R18 between V3 and pentode output valve (V4, Mullard UL41). Tone correction in anode circuit by C34, R24 and C35. Variable tone control by R23 and C33. Negative feed-back tone correction between V4 cathode circuit and V3 grid circuit via R22, R20, C32, R21, C31 and R13.

V3 grid circuit via R22, R20, C32, R21, C31 and R13.

H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Mullard UY41).

H.T. smoothing by R30 and electrolytic capacitors C36, C37. Valve heaters, together with ballast resistors R25, R26, R27 and scale lamps, are connected in series across the mains input. Mains R.F. filtering by C38 and chokes L19, 120

## CIRCUIT ALIGNMENT

CIRCUIT ALIGNMENT

1.F. Stages.—Switch receiver to medium waves and tune it to 300 m. Connect output of signal generator, via an 0.1 μF capacitor in each lead, to control grid (pin 6) of V2 and chassis, feed in a 470 kc/s (638.3 m) signal and adjust the cores of L17 (location reference C2) and L16 (C2) for maximum output. Transfer signal generator leads to control grid (pin 6) of V1 and chassis, and, feeding in a 470 kc/s signal adjust the cores of L15 (B2) and L14 (B2) for maximum output. Repeat these adjustments until no further improvement results.

R.F. and Oscillator Stages.—In order that the receiver may be aligned with the chassis in its cabinet, three holes are provided in the cabinet base to give access to C41, C42 and C43. If, however, the chassis is removed from its cabinet, three holes are provided in the cabinet for alignment, the frame aerial should be disconnected and a shorting link placed across the frame aerial sockets. As the tuning scale is fixed to the cabinet, reference should be made in this case to the substitute tuning scale fixed along the front of the chassis deck. A temporary cursor, such as a paper clip, should be fixed to the tuning drive, and, with the gang at maximum, aligned with the datum line on the substitute tuning scale.

L.W.—Switch receiver to L.W. and connect signal generator output leads to A and F

the substitute tuning scale.

L.W.—Switch receiver to L.W. and connect signal generator output leads to A and E sockets. Tune receiver to 2.000 m, feed in a 2.000 m (150 kc/s) signal and adjust the cores of L10 (B2) and L7 (B2) for maximum output. Tune receiver to 1.000 m, feed in a 1.000 m (300 kc/s) signal and adjust C43 (G4) for maximum output. Repeat these adjustments until no further improvement results.

M.W.—Switch receiver to M.W. tune to

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the cores of L9 (B1) and L6 (B2) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust C42 (H3) for maximum output. Repeat these adjustments until no further improvement results.

S.W.—Switch receiver to S.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (B2) and L5 (A2) for maximum output. Tune receiver to 25 m, feed in a 25 m (12 Mc/s) signal and adjust C41 (H4) for maximum output. Repeat these adjustments until no further improvement results.

L.W. Check.—If alignment has been carried out with the chassis out of its cabinet, the cores of L7 and L10 should be re-adjusted for maximum output at 2.000 m (150 kc/s) after the chassis has been replaced in its cabinet and the frame aerial re-connected,

#### GENERAL NOTES

Switches.—\$1-\$21 are the waveband and radio/gram change-over switches, ganged in two rotary units beneath the chassis. These units are indicated in our underside illustration of the chassis and shown in detail in the switch diagram in column 1, where they are drawn as seen in the direction of the indicating arrows in the chassis view. In the associated switch table, a dash indicates open, and c, closed.

\$22 is the internal speaker muting switch and is mounted, together with the external speaker Switches.-S1-S21 are the waveband and radio/

Switches	S.W.	M.W.	L.W.	Gram.
S1				С
S2	С			
S3	-	С	-	
S4			С	
S5	C			
86	Ċ	С		
S7	C			
88		С	_	
89			С	_
S10	******			C
S11 S12	C	***************************************		С
S12 S13	C	-		
S13 S14	-	С	С	
S14 S15	_		C	
S16	C	0	_	
S17	č	C		
S18	C	U	-	
S19	_	C		
S20		-	С	
S21			Ü	С

sockets, in the top rear corner of the cabinet. Scale Lamps.—These are 3.5 V, 0.15 A lamps with large clear spherical bulbs and M.E.S.

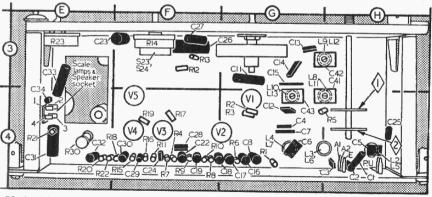
Drive Cord Replacemnt.—About 4ft 6in of nylon braided glass yarn is required for a new drive cord which should be run as shown in the sketch of the drive cord system, starting with the gang at maximum capacitance and running the cord off clockwise round the drum.

## VALVE ANALYSIS

Valve voltages and currents given in the table below are those derived from the manufacturer's information. They were measured on a receiver which was operated from A.C. mains of 230 V and tuned to the highest wavelength end of M.W. There was no signal input. Voltages were measured on the 10 V and 1,000 V ranges of a Model 7 Avometer, chassisbeing the negative connection in every case.

Valve	Anode		Screen		Cath
***************************************	V	mA	V	mA	V
V1 UCH42 V2 UF41 V3 UBC41	48 68 48	$\left\{ egin{array}{l} 2 \cdot 4 \\ 1 \cdot 2 \\ 1 \cdot 2 \\ 2 \cdot 8 \\ 0 \cdot 16 \end{array} \right\}$	48 50	1·2 1·2	1·0 1·2 0·6
V4 UL41 V5 UY41	212 211*	25.0	96	3.2	6·4 226·0

\* A.C. reading † Cathode current 37 mA.



Underside view of chassis. Switch units, indicated here, are shown in detail in col. 1.

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