"TRADER" SERVICE SHEET

# **COMPONENTS AND VALUES**

	CAPACITORS	Values	Loca- tions
C1 C2 C3	Aerial series L.W. aerial shunt S.W. aerial trim	50pF 800pF 20pF	H4 G4 H4
C4 C5	L.W. aerial trim V1 C.G	60pF 50pF	G4 G4
C6	A.G.C. decoupling	$0.1 \mu F$	G4
C7	1 1st I.F. trans. tun- f	110pF	C2
C8	∫ ing }	110pF	C2
C9	V1 cath. by-pass	$0.05\mu F$	G3
C10		45pF	G4
C11	M.W. osc. tracker	556pF	G3
C12 C13	L.W. osc. tracker	390pF	G3
C14	L.W. osc. trimmer H.T. decoupling	$180 pF \\ 0.05 \mu F$	G3
C15	A.G.C. decoupling	$0.05 \mu F$ $0.05 \mu F$	G4 G4
C16	V2 S.G. decoupling	$0.05 \mu F$	G4
C17	V2 anode decoup.	$0.05 \mu F$	F4
C18	2nd I.F. trans. tun- (	110pF	$\tilde{B}\tilde{2}$
C19	} ing {	110pF	B2
C20	V2 cath. by-pass	$0.05 \mu F$	F4
C21	* V3 cath. by-pass	$50\mu F$	F3
C22	I.F. by-pass	100pF	F4
C23	A.F. coupling	$0.01 \mu F$	F3
C24 C25	A.G.C. coupling	50pF	F4
C26	Tone corrector	0·002μF	F4 F4
C27	A.F. coupling	$0.01 \mu F \\ 0.1 \mu F$	F3
C28	Neg. feed-back }	$0.05 \mu F$	E4
C29	Part tone control	$0.05 \mu F$	E3
C30	) (	$0.001 \mu F$	E4
C31	Tone correctors {	$0.01 \mu F$	
C32		$32\mu F$	C2
€33		$16\mu F$	C2
C34		528 pF	A2
C35		528pF	A1
C36		40pF	H3
C37 C38	t M.W. osc. trimmer L.W. osc. trimmer	40pF	H3 G3
038	i D.W. Osc. trimmer	$40 \mathrm{pF}$	43

\* Electrolytic. † Variable. ‡ Pre-set.

A.C. Transportable Superhet

MPLOYING series-fed heaters and an A.C./D.C. range of valves, the Bush AC34 is a 3-band 4-valve (plus rectifier) operate from A.C. mains of 100-120 V and 200-250 V, 40-100 c/s. The waveband ranges are 16-50 m, 182-560 m and 833-2.068 m.

Release date and original price: August, 1953, £19 12s 9d. Purchase tax extra.

### CIRCUIT DESCRIPTION

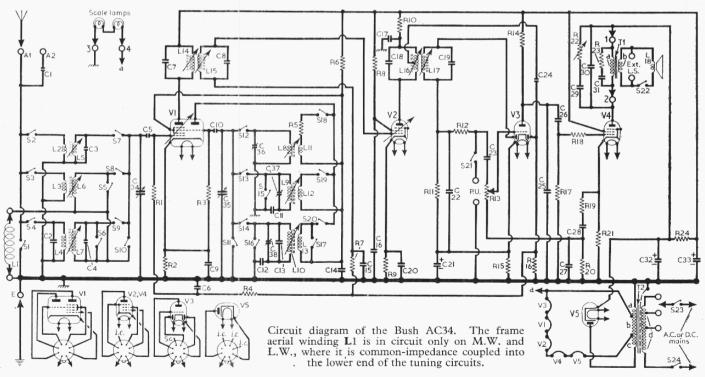
Aerial input via coupling coils L2, L3, L4 to single-tuned circuits L5, C34 (S.W.), L6, C34 (M.W.) and L7, C34 (L.W.), which precede triode hexode valve (V1, Mullard UCH42) operating as frequency changer. Reception from an internal frame aerial L1 is provided on M.W. and L.W., the winding being connected in series

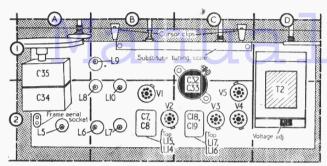
	RESISTORS	Values	Loca- tions
R1	V1 C.G	$470 \mathrm{k}\Omega$	G4
R2	V1 G.B	$220\Omega$	G4
R3	V1 osc. C.G	$47 \mathrm{k}\Omega$	G4
R4	A.G.C. decoupling	$1M\Omega$	F4
R5	S.W. stabilizer	$47\Omega$	H4
R6	H.T. feed	$15k\Omega$	G4
R7	A.G.C. decoupling	$2 \cdot 2M\Omega$	G4
R8	V2 S.G. decoupling	$47 \mathrm{k}\Omega$	F4
R9	V2 G.B	$330\Omega$	F4
R10	V2 anode decoup	$10 \text{k}\Omega$	F4
R11	Signal diode load	$330 \text{k}\Omega$	F4
R12	I.F. stopper	$100 \text{k}\Omega$	F3
R13	Volume control	$2 \cdot 2M\Omega$	F3
R14	V3 triode load	$150 \mathrm{k}\Omega$	F4
R15	V3 G.B	$5.6 \text{k}\Omega$	F4
R16	A.G.C. diode load	$1M\Omega$	F4
R17	V4 C.G	$470 \text{k}\Omega$	F4
R18	V4 C.G. stopper	$47k\Omega$	F4
R19	Neg. feed-back {	$1 \text{k}\Omega$	E4
R20	)	$10k\Omega$	F3
R21	V4 G.B	$220\Omega$	E4
R22	Tone control	$50 \text{k}\Omega$	E3
R23	Tone corrector	$10k\Omega$	-
R24	H.T. smoothing	$10k\Omega$	E4



with the chassis end of the two tuning coils. Oscillator grid coils L8, L9 and L10 are tuned by C35. Parallel trimming by C36 (S.W.), C37 (M.W.) and C13, C38 (L.W.); series tracking (Continued col. 1 overleaf)

ОТІ	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
$_{L1}$	Frame aerial	0.5	
L2	1 4 1		H4
L3	Aerial coupling	0.6	H4
L4	∫ coils	32.0	G4
$L_5$	)		H4
L6	Aerial tuning coils	4.0	H4
L7		16.0	G4 -
L8	Oscillator tuning		H3
$_{\rm L9}$	coils	$3 \cdot 2$	H3
L10	) cons (	4.0	Gr3
L11	Oscillator reaction	-	H3
L12	coils	0.6	H3
L13	)	1.5	G3
L14	lst I.F. trans. Pri.	12.5	C2.
L15	) (Sec.	12.5	C2
L16	2nd I.F. trans. { Pri.	12.5	B2
L17	) (Sec.	12.5	B2
L18	Speech coil	2.5	
T1	O.P. trans $\begin{cases} a & \cdots \\ b & \end{cases}$	500.0	
		0.5	
	( a	3.2	
T2	b	45.2	-
12	Mains trans. { c d,	237-0	102
	tótal	48.0	
S1-S21	Waveband/gram sw.		H4
822	Speaker switch		
S23, S24	Mains sw., g'd R13 {		F3



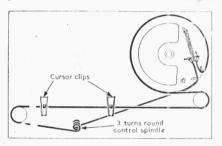


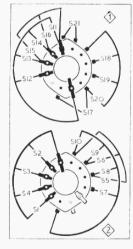
Plan view of chassis showing the posi-tion of the substitute tuning scale referred to in "Circuit Align-ment."

# Circuit Description—continued

by C11 (M.W.) and C12 (L.W.). Reaction coupling from anode by L11, L12 and L13. Second valve (V2, Mullard UF41) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C7, L14, L15, C8 and C18, L16, L17, C19.

Intermediate frequency 470 kc/s
Diode signal detector is part of double diode
triode valve (V3, Mullard UBC41). Audio frequency component in its rectified output is
developed across diode load resistor R1, and
passed via C23 and volume control R13 to grid





Above: Sketch of the tuning drive cord system as seen from the front of an upright chassis.

Left: Diagram of the waveband switch units, which are drawn as seen in the directions indicated by the arrows in the underchassis illustration.

of triode section. I.F. filtering by C22, R12 and the capacitance of the screened leads.

Second diode of V3 is fed from V2 anode via C24, and the resulting D.C. potential developed across load resistor R16 is fed back as bias to V1 and V2, giving A.G.C.

Resistance-capacitance coupling by R14, C26 and R17 between V3 triode anode and pentode output valve (V4, Mullard UL41). Tone correction in anode circuit by C30, C31 and R23. Variable tone control by R22, C29. Negative feed-back tone correction between V4 cathode circuit and V3 grid circuit via R19, C28, R20, C27.

H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Mullard UY41). H.T. smoothing by R24 and electrolytic capacitors C32, C33. Valve heaters are connected in series across section by of the mains transformer secondary winding, which is isolated from the mains.

#### CIRCUIT ALIGNMENT

1.F. Stages .- Switch receiver to medium waves

CIRCUIT ALIGNMENT

1.F. Stages.—Switch receiver to medium waves and tune it to 300 m. Connect output of signal generator, via an 0.1 µF capacitor in one lead, to control grid (pin 6) of V2 and chassis, feed in a 470 kc/s (638.3 m) signal and adjust the cores of L17 (location reference C2) and L16 (C2) for maximum output. Transfer signal generator leads to control grid (pin 6) of V1 and chassis, and, feeding in a 470 kc/s signal adjust the cores of L15 (B2) and L14 (B2) for maximum output. Repeat these adjustments until no further improvement results.

R.F. and Oscillator Stages.—In order that the receiver may be aligned with the chassis in its cabinet, three holes are provided in the cabinet base to give access to C36, C37 and C38. If, however, the chassis is removed from its cabinet for alignment, the frame aerial should be disconnected and a shorting link placed across the frame aerial sockets. As the tuning scale is fixed to the cabinet, reference should be made in this case to the substitute tuning scale fixed in this case to the substitut tuning scale fixed to the tuning drive, and, with the gang at maximum, aligned with the datum line on the substitute tuning scale.

L.W.—Switch receiver to L.W. and connect signal generator output leads to A and E sockets. Tune receiver to 2,000 m, feed in a 2,000 m (150 kc/s) signal and adjust the cores of L10 (B2) and L7 (B2) for maximum output. Tune receiver to 1,000 m, feed in a 1,000 m (300 kc/s) signal and adjust the cores of L9 (B1) and L6 (B2) for maximum output. Repeat these adjustments until no further improvement results.

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the cores of L9 (B1) and L6 (B2) for maximum output. Tune receiver to 2.00 m, feed in a 25 m (24 Mc) signal and adjust the cores of L8 (B2) and L5 (A2) for maximum output. Repeat these adjustments until no further improvement results.

L.W.—Switch receiver to S.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (B2) and L5 (A2) f

the frame aerial re-connected.

GENERAL NOTES

Switches.—S1-S21 are the waveband and radio/gram changeover switches, ganged in two rotary units beneath the chassis. These units are indicated in our underside illustration of the chassis and shown in detail in the switch diagram in column 1, where they are drawn as seen in the direction of the indicating arrows in the chassis view. In the associated switch table, a dash indicates open, and c, closed.

S22 is the internal speaker muting switch and is mounted, together with the external speaker sockets, in the too rear corner of the cabinet.

sockets, in the top rear corner of the cabinet.

Switches	S.W.	M.W.	L.W.	Gram
S1				С
S2	C	\$500 mg		
S3		C		
S4			C	
S5	C			
S6	C	C		
87	С			
S8		C		
89			С	
S10				C
S11				C
S12	С			
S13		С		
S14			С	
S15	С			
S16	C	C		
S17		С		
S18	С			
S19		С		
S20			C	
S21		an read		C

Scale Lamps.—These are 6.2 V, 0.3 A, lamps with large clear spherical bulbs and M.E.S.

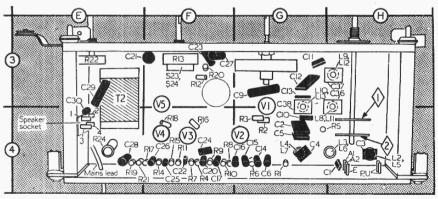
Drive Cord Replacement.-About 4ft 6in of nylon braided glass yarn is required for a new drive cord which should be run as shown in the sketch of the drive cord system, starting with the gang at maximum capacitance and running the cord off clockwise round the drum.

## VALVE ANALYSIS

Valve voltages and currents given in the table below are those derived from the manufacturer's information. They were measured on a receiver which was operated from A.C. mains of 230 V and tuned to the highest wavelength end of M.W. There was no signal input. Voltages were measured on the 10 V and 1,000 V ranges of a Model 7 Avometer, chassis being the negative connection in every case.

Valve	Anode		Screen		Cath.
vaive	V	mA.	V	mA	v
V1 UCH42	{ 120 Osci' 60	$\left. egin{array}{c} 3 \cdot 0 \\ \mathrm{tor} \\ 1 \cdot 5 \end{array} \right\}$	60	1.5	1.2
V2 UF41 V3 UBC41	84 60	3.5	62	1.5	1.5 0.8
V4 UL41 V5 UY41	264 263*	31.0	120	4.0	8·0 282·0

\* A.C. reading. † Cathode current 46 mA.



Underside view of chassis. The speaker socket in E4 also connects up with the scale lamps.