"TRADER" SERVICE SHEET

CAPACITORS	Values	Loca- tions
C1	68pF 0-002µF 0-001µF 0-001µF 56pF 100pF 0-1µF 100pF 100pF 100pF 0-1µF 0-047µF 230pF 110pF 0-1µF 0-1µF 0-04µF 100pF 100pF 100pF 100pF 100pF 100pF 100pF 100pF 0-05µF 4-70pF 0-002µF 4-70pF 0-002µF 15pF 0-001µF 0-002µF 15pF 0-002µF 0-002µF 15pF 0-002µF	H4 A22 A22 A23 B2 B2 B2 B2 B3 G3 G3 G3 G3 G3 G4 G4 G4 G2 C2 C2 F4 F4 F4 F4 F4 F4 F4 F4 F4 F4 F4 F4 F4

* Electrolytic. † Variable. ‡ Pre-set.

3-Band A.C. Superhet

CIRCUIT DESCRIPTION

AERIAL input via coupling coils L2, L3 and L4 to single-tuned circuits, which precede triode hexode valve (V1, Mullard UCH42) operating as frequency changer with internal coupling. I.F. rejection by L1, C1.

Second valve (V2, Mullard UF41) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C3, L14, L15, C9 and C18, L16, L17, C19.

L17, C19.

Intermediate Frequency 460 k/os.
Diode signal detector is part of double diode triode valve (V3, Mullard UBC41). Audio frequency component in its rectified output is developed across diode load resistor R11, and

	RESISTORS	Values	Loca- tions
R1	Aerial shunt	1ΜΩ	H4
R2	V1 C.G	$680 \text{k}\Omega$	H4
R3	V1 screen grid	$18k\Omega$	H4
R4	potential divider ($27k\Omega$	H4
R5	Osc. C.G. stopper	220Ω	H4
R6	V1 osc. C.G.	$47 \mathrm{k}\Omega$	H4
R7) Oss speds foods	$22k\Omega$	H4
R8	Osc. anode feeds {	$68k\Omega$	H4
R9	V2 S.G. feed	$47k\Omega$	F4
R10	V2 anode decoup	$2 \cdot 2k\Omega$	F4
R11	Signal diode load	$680 \mathrm{k}\Omega$	F4
R12	I.F. stopper	$47 \mathrm{k}\Omega$	F4
R13	Tone control	$1M\Omega$	D1
R14	Part tone control	$220 k\Omega$	D1
R15	Volume control	$1 M\Omega$	E3
R16	V3 C.G	$10M\Omega$	F4
R17	V3 anode load	$220 \text{k}\Omega$	F4
R18	A.G.C. decoupling	$1 \text{M}\Omega$	F4
R19	A.G.C. diode load	$1 \text{M}\Omega$	F4
R20	V4 C.G	$680 \text{k}\Omega$	F3
R21	H.T. smoothing	$10 \text{k}\Omega$	F4
R22	Part tone corrector	$4.7M\Omega$	F3
R23	Nog food book	220Ω	F4
R24	Neg. feed-back {	10Ω	E4
R25	Part tone corrector	$3.3 \text{k}\Omega$	E3
R26	H.T. smoothing	680Ω	F3
R27	G.B. potential	33Ω	E3
R28*	} divider \	-84Ω	E3
R29	V5 surge limiter	-100Ω	E4

 $^{\circ}$ Two resistors, 190 Ω and 150 Ω , in parallel.

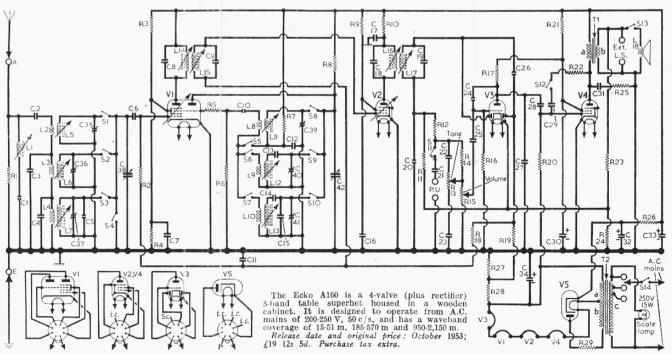


is passed via volume control R15 and C25 to grid of triode section.

Resistance-capacitance coupling by R17, C28 and R20 between V3 and pentode output valve (V4, Mullard UL41). Provision is made for the connection of a iow impedance external speaker across T1 secondary winding.

(Continued col. 1 overleaf)

ОТН	ER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13 L14 L15 L16 L17 L18	I.F. filter coil Aerial coupling coils Aerial tuning coils Oscillator reaction coils Oscillator tuning coils Ist I.F. trans. { Pri. Sec. } 2nd I.F. trans. { Sec. Speech coil } 0.P. trans. { a } Mains \$ \frac{a}{a} \	15 	H4 A2 A1 A2 A1 A2 H3 G3 H3 G3 B2 E2 C2 C2 F3
T2 S1-S12 S13 S14	Mains trans. trans. c, total Waveband switches Speaker switch Mains sw., g'd R15	85·0 40·0 — —	H3 G4 E3



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Circuit Description-continued.

Variable tone control by C22, R13, C23 and R14 in V3 grid circuit. Fixed tone correction by C31, R25 in V4 anode circuit and negative feed-back capacitor C29 in V3 anode circuit. A proportion of the speech coil voltage, that developed across R24 in potential divider R25, R24, is fed to V3 cathode circuit giving a further degree of negative feed-back.

GENERAL NOTES

Switches.—S1-S12 are the waveband switches, ganged in two rotary units beneath the chassis. These units are indicated in our under chassis illustration and shown in detail below col. 3 where they are drawn as seen from the con-

Switch	S.W.	M.W.	L.W.	Gran
S1	С		-	
S2		С		
S3	_		С	271
84				С
S5	С		-	
S6		С		
S7		P. Consult	С	
S8	С			
S9		С		10000
S10		Prima.	С	
S11	\$100 mm			С
S12				С

trol knob end of an inverted chassis. In the associated switch table above, a dash indicates open and C closed.

Modification.—In earlier receivers the valves were biased individually by means of cathode bias resistors as follows: V1 cathode was returned to chassis via a 330Ω resistor shunted with an 0.1 µF capacitor; V4 cathode was returned to chassis via a 150Ω resistor shunted with a 50 µF electrolytic capacitor; R27, R28 and C34 were not fitted, and the top end of winding a on T2 was returned to classis together with the low potential end of the heater chain.

Drive Cord Replacement.—About 24 index of

heater chain.

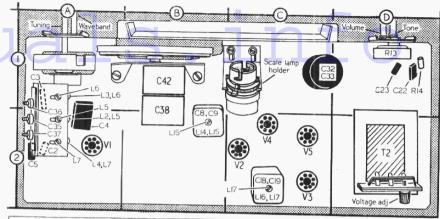
Drive Cord Replacement.—About 24 inches of fine-gauge Bowden cable and 34 inches of high-grade flax fishing line, plaited and waxed, are required for a new drive cord. Soldered end loops should be made on the Bowden cable so that it measures 21½ inches overall. One end of the length of drive cord should be tied to one of these soldered loops, and the complete drive then run as shown in the sketch beneath the plan view on this page.

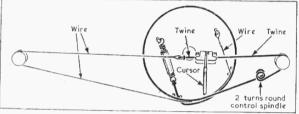
VALVE ANALYSIS

Valve analysis

Valve voltages and currents in the table (next col.) are those measured in our receiver when it was operating from A.C. mains of 235 V, the voltage adjustment being set to the 240-250 V tapping. The receiver was switched to M.W. and the gang turned to maximum capacitance, but there was no signal input.

Voltages were measured on an Avo Electronic TestMeter, and as this instrument has a





Above: Plan view of The tuning chassis. scale must be detached and placed over the scale backing plate for alignment.

Left: Sketch of the drive cord system with gang at maximum.

high internal resistance, allowance should be high internal resistance, allowance should be made for the current drawn by other types of meter. Chassis was the negative connection in every case. The negative voltage measured across R27 was 1.8 V. and across C34, 10 V.

Valve	Anode		Screen		Cath.	
	V	mA	V	mA	V	
V1UCH42	$\begin{cases} 174 \\ \text{Osci} \\ 62 \end{cases}$	$\left\{\begin{array}{c} 2\cdot 9 \\ \text{llator} \\ 1\cdot 7 \end{array}\right\}$	88	2.4		
$\begin{array}{c} V2UF41 \\ V3UBC41 \end{array}$	162 62	5·5 0·23	88	1.7	_	
$\begin{array}{c} { m V4UL41} \\ { m V5UY41} \end{array}$	160 200*	34.0	110	6.0	206†	

CIRCUIT ALIGNMENT

I.F. Stages.—Switch receiver to M.W. 1.r. stages.—Swhich receiver to M.W. and turn gang to maximum capacitance. Connect output of signal generator, via an 0.1 µF capacitor in each lead, to control grid (pin 6) of V1 and chassis. Feed in a 460ke/s (652.1 m) signal and adjust the cores of L17 (location reference C2), L16 (F4), L15 (B2) and L14 (G4) for maximum output.

R.F. and Oscillator Stages.—Check that with

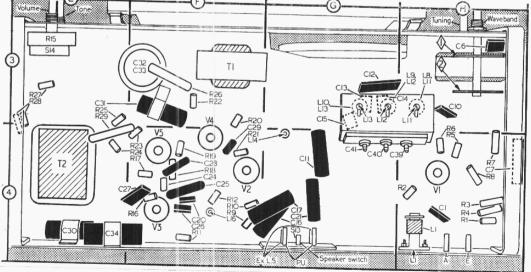
R.F. and Oscillator Stages.—Check that with the gang at maximum capacitance, the cursor coincides with the vertical lines at the high wavelength ends of the S.W. and L.W. tuning scales. Transfer signal generator to A and E. I.F. Filter.—Feed in a 460 kc/s signal and adjust the core of L1 for minimum output.

S.W.—Switch receiver to S.W., tune to 16.67 m, feed in a 16.67 m (18 Mc/s) signal and adjust C39 (H4) and C35 (A2) for maximum output. Tune receiver to 33.34 m (9 Mc/s) signal and adjust cores of L11 (H3) and L5 (A2) for maximum output.

M.W.—Switch receiver to M.W. tune to

M.W.—Switch receiver to M.W., tune to 214.3 m, feed in a 214.3 m (1,400 ke/s) signal and adjust C40 (G4) and C36 (A1) for maximum output. Tune receiver to 333.4 m, feed in a 333.4 m (800 ke/s) signal and adjust the cores of L12 (G3) and L6 (A1) for maximum output.

L.W.—Switch receiver to L.W., tune to 1.000 m, feed in a 1.000 m (300 ke/s) signal and adjust C41 (G4) and C37 (A2) for maximum output. Tune receiver to 1.429 m, feed in a 1.420 m (210 ke/s) signal and adjust the cores of L13 (G3) and L7 (A2) for maximum output.



Above: Waveband switches. Left: Underside view of chassis.

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