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# ADER" SERVICE SHEET BRIST C.E.C. BC5246

and BC6245, A.C. and A.C. D.C. Transportables

"TRADER" SERVICE SHEET

1122

HE G.E.C. BC5246 is a compact 4-valve (plus rectifier) 3-band transportable table receiver, designed to operate from A.C. mains of 190-250 V, 40-100 c/s. The waveband ranges are 1,000-2,000 m, 187-572 m, 13.5-50 m.

Model BC6245 is an A.C./D.C. version of model BC5246, differences between them being covered in the circuit diagram below, where the aerial input, power output and mains supply circuits for the BC6245 are re-drawn on either side of the main circuit. Other differences between the models are covered in the component and valve voltage tables.

Release date and original price, both models: August 1953, £12 148 5d. Purchase tax extra.

#### CIRCUIT DESCRIPTION

Tuned frame aerial input on M.W. by L1, C27 and on L.W. by L1, L2, C27.

For S.W. reception an external aerial is necessary and is coupled via L3 to single-tuned circuit L4, C27. Provision is also made for the connection of an external aerial on M.W. and L.W., and when in use it is coupled to the tuned grid circuits by the common impedance of C1. R1 shunts the aerial circuit to prevent modulation hum. In the A.C./D.C. model C30 and C31 isolate the A and E sockets from chassis and L14 shunts the aerial circuit to by-pass modulation hum voltages. R17 prevents the build-up of static charges on the aerial.

First valve (V1, Osram X79 (A.C. model) or X109 (A.C./D.C. model) is a triode hexode operating as frequency changer with internal coupling. Oscillator grid coils L5 (S.W.), L6 (M.W.) and L7 (L.W.) are tuned by C28. Parallel trimming by C29 (M.W.) and C9 (L.W.); series tracking by C11 (M.W.) and C10, C11 (L.W.). Reaction coupling from oscillator anode by L8 (S.W.) and across

the common impedance of tracker C11 (M.W. and L.W.).

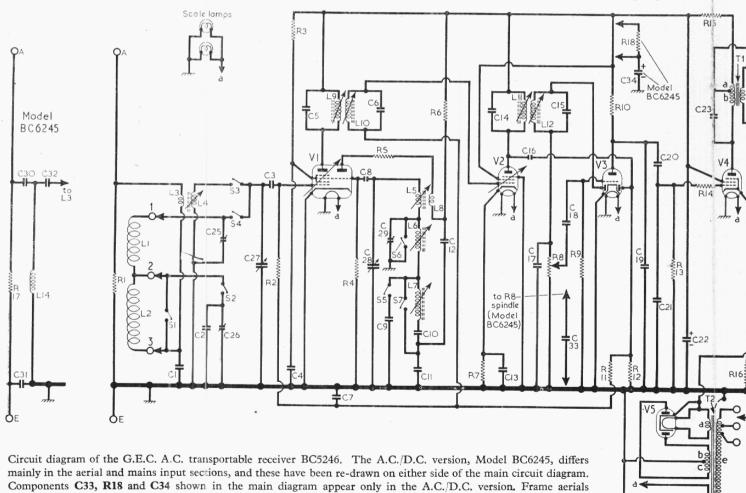
Second valve (V2, Osram W77 (A.C. model) or W107 (A.C./D.C. model)) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C5, L9, L10, C6 and C14, L11, L12, C15.

#### Intermediate frequency 470 kc/s.

Diode signal detector is part of double diode triode valve (V3, Osram DH77 (A.C. model) or DH107 (A.C./D.C. model)). A.F. component in rectified output is developed across volume control R8, which operates as diode load, and is passed via C18 to triode section. I.F. filtering by C17 and C19.

Second diode of V3 is fed from V2 anode via C16, and the resulting D.C. potential developed across load resistor R12 is fed back as bias to V1 and V2, giving automatic gain control.

Resistance - capacitance coupling by



L1 and L2 are for M.W. and L.W. operation only, an external aerial being necessary for S.W. operation.

### COMPONENT VALUES AND LOCATIONS



Appearance of BC5246 and BC6245.

R10, C20 and R13 between V3 and pentode output valve (V4, Osram N78 (A.C. model) or N108 (A.C./D.C. model)). Tone correction in grid circuit by **C21**, in anode circuit by **C23**, and in cathode circuit (A.C. model only) by the negative feed-back voltage developed across R16.

In the A.C. model, H.T. current is supplied by I.H.C. full-wave rectifying valve (V5, Osram U78). Smoothing by R15 and electrolytic capacitors C22 and C24, residual hum being neutralized by passing the current through section a of the primary winding on the output transformer.

(Continued in column 6)

	RESISTORS	Values	Loca- tions
R1	Mod. hum shunt	10kΩ	G4
R2	V1 C.G	$1 \text{M}\Omega$	G4
R3	V1 S.G. feed	$47k\Omega\dagger$	G4
R4	V1 osc, C.G	$100 \mathrm{k}\Omega$	G4
R5	Osc. stabilizer	680Ω	G4
R6	Osc. anode feed	33kه	G4
R7	V2 G.B	470Ω§	F4
R8	Volume control	$1 \text{M}\Omega$	D3
R9	V3 C.G	10ΜΩ	E4
R10	V3 anode load	$150 k\Omega$	E4
R11	A.G.C. decoupling	$1M\Omega$	E4
R12	A.G.C. diode load	$470 \text{k}\Omega$	E4
R13	V4 C.G	$270 \text{k}\Omega$	E4
R14	V4 C.G. stopper	10kΩ	E3
R15	H.T. smoothing	4·7kΩ	B2
R16	V4 G.B	150Ω	E3
R17	Aerial shunt	$1M\Omega$	210
R18	H.T. decoupling	8·2kΩ	
R19	V5 surge limiter	$270\Omega$	
R20	Brimistor CZ1	21032	-
R21	Heater ballast	$1.040 \Omega^*$	

\* Tapped at  $420\Omega+310\Omega+310\Omega$  from R20. †  $100 k\Omega$  )

A.C./D.C. model  $10k\Omega$ 

If the component numbers given in the accompanying tables are used when ordering replacements, dealers are advised to mention the fact on the order, as these numbers may differ from those used in the manufacturers' circuit diagram.

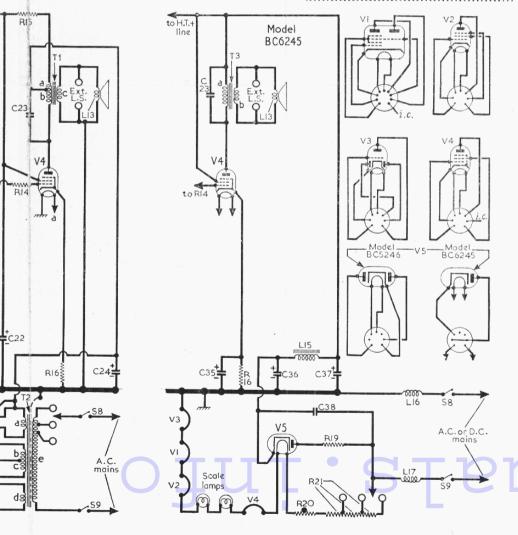
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		CAPACITORS	Values	Loca- tions
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C1	Ext. aerial coupling	3.950pF	F3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	C2			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	33			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	14	V1 S.G. decoupling		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	16			A2
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	17	A.G.C. decoupling		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	18			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	79	L.W. osc. trim	166pF	G3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		L.W. osc, tracker	180 pF	G3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				G3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	C12			G3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			$120 \mathrm{pF}$	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1.F. by-pass		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		A.F. coupling		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		1.F. by-pass		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		A.F. coupling		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	21			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Tone corrector		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		H.T. smoothing	$16\mu F$	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		M.W. aerial trim		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
$ \begin{array}{c} (29)^{+} \\ (33)^{+} \\ (31)^{-} \\ (32)^{-} \\ (33)^{-} \\ (33)^{-} \\ (34)^{-} \\ (35)^{-} \\ (35)^{-} \\ (37$				
	1004			
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		M. W. osc. trim	0.001 1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		Chassis isolators }		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		) lavial coupling		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				
$\begin{pmatrix} 035* \\ 036* \\ 037* \end{pmatrix}$ H.T. smoothing $\begin{pmatrix} 100\mu F \\ 32\mu F \\ 32\mu F \end{pmatrix}$		H T descupling		-
$\begin{pmatrix} \text{C36*} \\ \text{C37*} \end{pmatrix}$ H.T. smoothing $\begin{pmatrix} 32\mu\text{F} \\ 32\mu\text{F} \end{pmatrix}$ =		V4 cath by-pace		
$(37*)$ H.T. smootning $\{32\mu F\}$		) (		
(57)		} H.T. smoothing }		
C38 Mains R.F. by-pass 0.01µF —	C38	Mains R.F. by-pass		

\* Electrolytic. † Variable. ‡ Pre-set.

OTE	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13 L14 L15 L14 L15 L16 L16 L16 L16 L16 L16 L16 L17	M.W. frame aerial L.W. frame aerial S.W. coupling coil S.W. aerial tuning Oscillator tuning coils S.W. reaction coil  Ist I.F. trans. {Pri. Sec. 2nd I.F. trans. {Pri. Sec. Speech coil I.F. choke Smoothing choke Mains R.F. filter chokes	1·0 1·1·0	F3 F3 G4 G3 G3 G4 A2 A2 B2 B2 B2
Т1	O.P. trans. $ \begin{pmatrix} a & \cdots \\ b & \cdots \\ c & \cdots \end{pmatrix} $ Mains $ \begin{pmatrix} a & \cdots \\ c & \cdots \\ a & \cdots \\ b & \cdots \end{pmatrix} $	24·0 460·0 — 270·0	В1
T2 T3 S1-S7	Trans. (BC 5246) $\begin{pmatrix} c & \cdots \\ d & \cdots \\ e, total \end{pmatrix}$ (BC 6245) $\begin{pmatrix} b & \cdots \\ b & \cdots \\ b & \cdots \end{pmatrix}$ (BC 6245) $\begin{pmatrix} b & \cdots \\ b & \cdots \\ b & \cdots \end{pmatrix}$	270·0 270·0 34·0 430·0	C2 — G3
S8, S9	Mains sw., g'd R8	-	D3

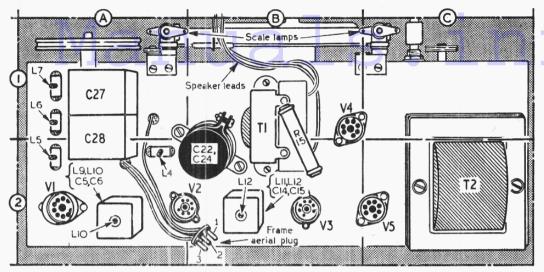
#### Circuit Description—continued.

In the A.C./D.C. model H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Osram U107). Smoothing by choke L15 and electrolytic capacitors C36 and C37. Valve heaters, together with scale lamps, thermistor R20 and ballast resistor R21 are connected in series across the mains input. R20 protects the valve heaters and scale lamps from current surges, and R19 protects V5 from current surges. Mains R.F. filtering by C38 and chokes L16, L17.









Plan view of the chassis showing the 3-pin frame aerial connector. The pins are numbered and refer to similarly numbered connections in the circuit diagram overleaf. In the A.C. / D.C. model, the heater ballast resistor R21 is mounted horizontal on the chassis in place of T2.

#### **GENERAL NOTES**

Switches.-S1-S7 are the waveband switches ganged in a single rotary unit beneath the chassis. The unit is indicated in our under chassis illustration and shown in detail in the diagram below.

The associated switch table gives the switch operations for the three control settings, starting with the slide-type switch control in the extreme left-hand position (viewed from front). indicates open and c closed.

S8, S9 are the Q.M.B. mains on/off switches ganged to the volume control R8.

Scale Lamps, A.C. Model.-Two 6.5 V. 0.3 A lamps with small clear spherical bulbs and M.E.S. bases.

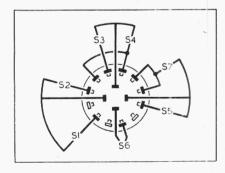
Scale Lamps, A.C./D.C. Model.—Two 6.5 V, 0.115 A lamps with small clear spherical bulbs and M.E.S. bases. A spare lamp is mounted inside the receiver

on the back cover.

Model BC6245.—This is an A.C./D.C. version of the BC5246 on which this Service Sheet is based. The main differences are in the aerial and mains input circuits,

Switch	M.W.	S.W.	L.W.
S1	С		
S2			С
S2 S3	-	С	Name of Street
84	С		С
85			С
S4 S5 S6		С	
S7	C	C	

Above: Table showing switch operations. Below: Waveband switch diagram drawn as seen from rear of inverted chassis.



and these sections are redrawn on either side of the main circuit diagram overleaf.

Differences in values are indicated in the component tables and a separate valve voltage table is given for each model. The heater ballast resistor R21 is mounted horizontally on the deck of the chassis in place of the mains transformer T2. Apart from these changes, however, the remaining information applies to both models.

Modifications.—In early A.C. models C13 and C21 were omitted, and the screen grids of V1 and V2 were fed from a com-

mon H.T. resistor.

#### CIRCUIT ALIGNMENT

All the core and trimmer adjustments can be made accessible by removing the cabinet back and base cover.

I.F. Stages.—Switch receiver to M.W. and tune receiver to a point at the high wavelength end of the band where there is no signal pick-up. Connect output of signal generator, via an 0.1 µF capacitor in each lead, to control grid (pin 1) of V2 and chassis. Feed in a 470 kc/s (638.3 m) signal and adjust the cores of L12 (location reference B2) and L11 (F4) for maximum output. Transfer signal generator "live" lead to V1 control grid (pin 2). Feeding in a 470 kc/s signal, adjust the cores of L10 (A2) and L9 (G4) for maximum output. Repeat these adjustments, transfering signal generator "live" lead to V2 control grid when readjusting the cores of L11 and L12.

R.F. and Oscillator Stages .- The following adjustments are accessible with the chassis in its cabinet, but if the chassis is withdrawn, then the adjustments can be carried out with the aid of the substitute tuning scale which is printed on the front edge of the cursor rail. Readings on this scale are made against the right-hand edge of the cursor carriage (viewed from front of receiver) and are quoted in brackets after each calibration wavelength in the following instructions. Check that with the gang at maximum capacitance, the cursor coincides with the high wavelength end of the S.W. tuning scale, or that the right-hand edge of the cursor carriage coincides with 90 on the substitute tuning scale. Transfer signal generator leads, via a dummy aerial, to A and E sockets.

**S.W.**—Switch receiver to S.W. and tune to 50 m (85). Feed in a 50 m (6 Mc/s) signal and adjust the cores of L5 (A2) and L4 (A2) for maximum out-Repeat these adjustments.

M.W.—Switch receiver to M.W. and tune to 500 m (71.5). Feed in a 500 m (600 kc/s) signal and adjust the core of L6 (A1) for maximum output. Tune receiver to 200 m (6), feed in a 200 m (1,500 kc/s) signal and adjust **C29** (G3) and **C25** (G3) for maximum output. Repeat these adjustments until no further improvement results.

L.W.—Switch receiver to L.W. and tune to 1,304 m (26). Feed in a 1,304 m (230 kc/s) signal and adjust the core of L7 (A1) and C26 (G3) for maximum output. Repeat these adjustments. If adjustments are subsequently made to the S.W. or L.W. cores or trimmers the complete R.F. and oscillator alignment should be repeated.

#### Sensitivity Figures

Connect output of signal generator directly to the  $\boldsymbol{A}$  and  $\boldsymbol{E}$  sockets, and connect a 0-100 V A.C. voltmeter across the output transformer primary winding (section b of T1 or section a of T3). sensitivity figures quoted below indicate the signal generator output required to produce a 13.5 V reading (50 milliwatts) on the A.C. voltmeter. As these figures were measured on new receivers at the factory, sensitivities within the range of -50% to +100% are acceptable. signal generator output should be modulated by 400 c/s to a depth of 30%.

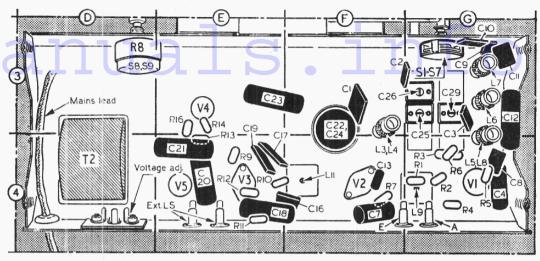
S.W.—Switch receiver to S.W., feed in

a 50 m (6 Mc/s) signal and tune it in on receiver. Check that to obtain a 13.5 V meter reading, the signal generator output is about  $36 \,\mu V$ .

M.W.—Switch receiver to M.W., feed in a 500 m (600 kc/s) signal and tune it in on receiver. Check that for a 13.5 V meter reading, the signal generator output is about 20 µV. Check that the same sensitivity is obtained at 200 m (1,500

L.W.—Switch receiver to L.W., feed in a 1,304 m (230 kc/s) signal and tune it in on receiver. Check that for a 13.5 V meter reading, the signal generator output is about 30  $\mu V_{\rm \cdot}$ 

Under-chassis view showing the three trimmers (location G3) adjusted in the R.F. and oscillator alignment. The core adjustments of L4, L5, L6 and L7 are accessible from the top of the chassis deck and are indicated in our plan view of the chassis



#### DRIVE CORD REPLACEMENT

For both A.C. and A.C./D.C. models, approximately two feet of high-grade fishing line, plaited and waxed, and about a foot of stranded steel flexible wire are required for the complete tuning drive, which consists of two parts. Suitable lengths can be obtained from the makers' service department, Greycoat Street, Westminster, London, S.W.1.

Our sketch shows the complete system as seen when viewed from the front with the gang at minimum capacitance. The wire is made up into a length measuring 10 in overall, with a soldered loop about in diameter each end. The cord should be tied to one of the loops and the remaining loop anchored round the plastic lug in the drive drum. The wire should then be led out through the top gap in

#### VALVE ANALYSIS

Valve voltages and currents given in the table below are those derived from the manufacturers' information, and were measured with the receiver operating from A.C. mains of 230 V. The receivers were switched to M.W. and tuned to 200 m, but there was no signal input.

Voltages were measured on the 15 V and 750 V ranges of a 1,000 ohms-per-volt meter,

chassis being the negative connection in each case.

#### A.C. Model

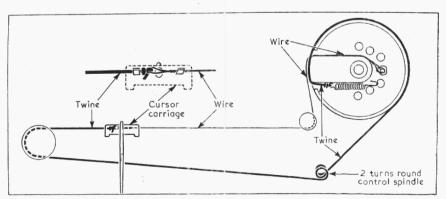
Valve		Anode		Screen		Cath.	
varve		V	mA	v	mA	V	
VI X79		200 Oscill 85	$\left\{ egin{array}{c} 2 \cdot 0 \\ ator \\ 3 \cdot 2 \end{array} \right\}$	64	2.9	_	
V2 W77		200	5.0	200	1.4	3.0	
V3 DH77 V4 N78 V5 U78		80 275 250*	0·8 23·0	200	3.5	4·0 290·0†	

A.C. reading, each anode. Cathode current 42 mA.

#### A.C./D.C. Model

Voles	Valve		Anode		een	Cath.	
vaive			mA	·V	mA	V	
V1 X109		$\begin{cases} 156 \\ \text{Oscil} \\ 115 \end{cases}$	$\begin{pmatrix} 0.6 \\ lator \\ 3.7 \end{pmatrix}$	40	1.2	_	
V2 W107		156	4.5	140	1.2	1.5	
V3 DH107 V4 N108		$\frac{60}{142}$	0·5 42·5	156	7.5	7.5	
V5 U107	• • • •	215*				200.0†	

\* A.C. reading. † Cathode current 62mA.



Sketch of the tuning and cursor drive system as seen from the front of the chassis with the gang at minimum capacitance. Both drive cord and wire are used in this system.

the drum, and run anti-clockwise down to and under the first pulley. Continue on as shown in the sketch at the foot of columns 4 and 5, finally tying off the cord to one end of the tension spring and anchoring the other end of the spring in one of the holes in the lower half of the drive drum. The tension on the drive cord can be varied by anchoring the spring in any one of the three holes provided.

Turn the gang to maximum capacitance and slide the cursor carriage along the scale backing plate until its right-hand edge (viewed from front) coincides with 90 on the substitute tuning scale. Finally, clamp the drive cord and drive wire under the clips on the cursor carriage.

## Service Sheet Correction

Owing to an oversight when writing up the circuit description of the Pye P65MBQ in Service Sheet 1114, it was stated that for mains operation filament current was supplied via R13, whereas from a study of this rather complex circuit diagram it is obvious that the output valve V5 is connected in series with the rest of the receiver, and all the current, H.T. and L.T., must be drawn from V5 cathode.

At the same time, attention is drawn to the omission of an asterisk in the valve equivalents table in Service Sheet 1105, where N37 is shown as an equivalent of PL82. It will be appreciated as a favour if users will insert an asterisk against the N37 entries opposite PL82, to indicate that the base connections are different.

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