Wirel

"TRADER" SERVICE SHEET

OTH the A.C. and A.C./D.C. versions of the Ferguson 353 series are covered here, together with a full description of the differences between them and two earlier versions of the same

The basic A.C. receiver, model 353A, is a 3-valve (plus rectifier) 3-band superhet table model, with a frame aerial for M.W. and L.W., designed to operate from A.C. mains of 200-250V, 40-60 c/s using a

# FERCUSON 353 Series

Covering Early and Late Versions of 353A and 353U Receivers

double-wound transformer. The A.C./D.C. version, model 353U, is designed to operate from mains of the same range ratings. Differences between our samples and the early versions are fully explained under "Modifications" overleaf.

Release date and original price, all models: November, 1952, £16 3s 1d.

#### CIRCUIT DESCRIPTION

Tuned frame aerial input by L1, C33 (M.W.) and L1, loading coil L3 and C33 (L.W.). On S.W. the tuned circuit L4, C33 is coupled via L2 to the frame aerial, which then acts as an untuned internal aerial, provision also being made for the connection of an external aerial via C1. R1 is shunted across L3 to give an increased margin of stability on L.W. In the A.C./ D.C. model **C39** isolates the **E** socket from chassis which is "live" to the mains.

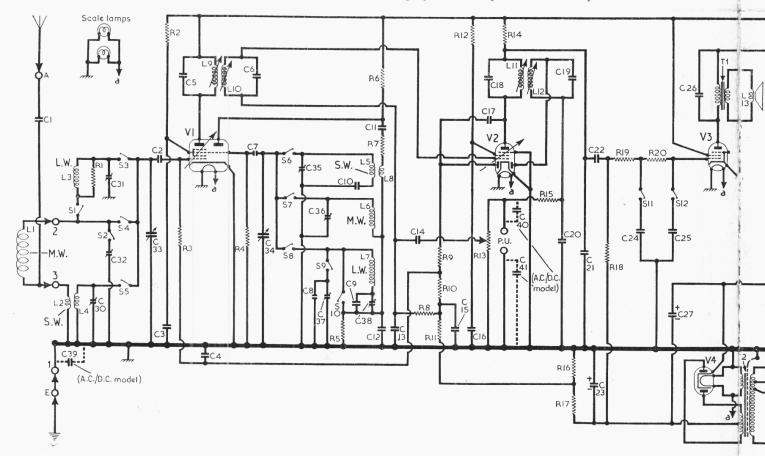
V1 (Mullard ECH42 (A.C. model) or UCH42 (A.C./D.C. model)) is a triode hexode valve operating as frequency changer with internal coupling. Oscillator grid coils L5 (S.W.), L6 (M.W.) and L7 (L.W.) are tuned by C34. Parallel trimming by C35 (S.W.), C36 (M.W.) and C8, C37 (L.W.); series tracking by C10 (S.W.), C12 (M.W.) and C9, C12, C38 (L.W.). Reaction coupling across the common impedance of tracker C12 (M.W. and L.W.) and via L8 (S.W.). R5 limits the reaction coupling on M.W. and L.W. Oscillator stabilization by R7.

Second valve (V2 Mullard EBF80 (A.C. model) or UBF80 (A.C./D.C. model)) is a double diode pentode valve, its pentode section operating as a reflex I.F./A.F. amplifier with tuned transformer I.F. couplings C5, L9, L10, C6 and C18, L11, L12, C19.

# Intermediate frequency 470 kc/s.

First diode section of V2 operates as signal detector, the A.F. component in its rectified output being developed across volume control R13, which acts as diode load, and passed via C14 and L10 to control grid of V2 pentode section, which then operates as A.F. amplifier. I.F. filtering by C13, R15, C20 and C21. Provision is made for the connection of a gramophone pick-up across R13, the pick-up sockets in the A.C./D.C. model being isolated from chassis by C40 and C41.

Second diode of V2 is fed via C17 from V2 pentode anode, and the resulting D.C. component is developed across



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resistors R9, R10, R11, which act as a potential divider, bias for V1 and V2 being tapped off from it to give automatic gain control.

Amplified A.F. output from V2 is developed across audio load resistor R14 and passed via C22, R19 and R20 to pentode output valve (V3, Mullard EL41 (A.C. model) or UL41 (A.C./D.C. model). Tone correction in anode circuit by C26. Three-position tone control is provided by C24, C25 and switches S11, S12.

In the A.C. model H.T. current is supplied by full-wave I.H.C. rectifying valve (V4, Mullard EZ40). Smoothing by R21, R22 and electrolytic capacitors C27, C28 and C29. A double-wound mains transformer T2 feeds the valve heaters from a common secondary winding. Grid bias for V3 is developed across R16, R17 in the H.T. negative lead to chassis. A proportion of this voltage, that across R16, is used as delay bias for the A.G.C. diode and standing bias for V1 and V2 pentode

In the A.C./D.C. model H.T. current is supplied by half-wave I.H.C. rectifying valve (V4, Mullard UY41). Smoothing by R21, R25 and electrolytic capacitors C27, C42 and C43. The valve heaters, together with ballast resistor R27, scale lamps with shunts R28 and R29, and mains R.F. filter chokes L14, L15, are connected in series across the mains input. R26 protects V4, and R28 the scale lamps, from current surges. Thermistor R29 (Brimistor, CZ2) maintains the heater circuit should the scale lamps fail, and prevents R28 from being overloaded by the heater current.

#### **COMPONENTS AND VALUES**

	CAPACITORS	Values	Loca- tions
C1	Aerial coupling	0·001μF	
C2	V1 C.G	200pF	G3 -
C3	V1 S.G. decoupling	$0.05\mu F$	G3
C4	A.G.C. decoupling	$0.02 \mu F$	G3
C5	1st I.F. trans.	100pF	B1
C6	f tuning \	$100 \mathrm{pF}$	B1
C7	V1 osc. C.G	50pF	G3
C8	L.W. osc. trim	50 pF	G3
C9	L.W. osc. tracker	$250 \mathrm{pF}$	G3
C10	S.W. osc. tracker	¶4,550pF	F3
C11	Osc. anode coup.	100pF	F3
C12	M.W. osc. tracker	520pF	F3
C13	A.G.C. decoupling	500pF	E3
C14	A.F. coupling	$0.01 \mu F$	D3
C15	A.G.C. decoupling	$0.05 \mu F$	E4
C16	V2 S.G. decoupling	$0.1 \mu F$	E4
C17	A.G.C. coupling	100pF	E3
C18	2nd I.F. trans.	100pF	C1
C19	tuning	100pF	C1
C20	1	200pF	D3
C21	I.F. by-passes	$0.002 \mu F$	$\overline{\mathrm{D}3}$
022	A.F. coupling	$0.01 \mu F$	E4
C23*	G.B. by-pass	$100\mu F$	E4
224	)	$0.002\mu F$	$\widetilde{\mathrm{D3}}$
225	Parts tone control	$0.002 \mu F$	D3
326	Tone corrector	$  0.002\mu F  $	B2
227*	)	$32\mu F$	G4
028*	H.T. Smoothing	$24\mu F$	G4
C29*		$24\mu F$	G4
C30‡	S.W. aerial trim.	70pF	A1
C31İ	L.W. aerial trim.	70pF	A1
C32İ	M.W. aerial trim.	· 30pF	A2
C33‡	Aerial tuning	§528pF	AI
C34†	Oscillator tuning	§528pF	Aî
C35‡	S.W. osc. trim	70pF	A1
C36‡	M.W. osc. trim	70pF	A1
C37‡	L.W. osc. trim	70pF	AI
C38‡	L.W. osc. tracker	70pF	A2
C39	Earth isolator	$0.005 \mu F$	112
C40	<b>\</b>	$0.005 \mu F$ $0.005 \mu F$	
C41	P.U. isolators }	$0.05 \mu F$	-
C42*	) (	$32\mu F$	
C43*	H.T. smoothing }	$16\mu F$	
C44	Mains R.F. by-pass	$0.01 \mu F$	
CII	Dienis It.I. Dy-pass	συτμι	-

*	Electrolytic.
†	Variable.
İ	Pre-set.
- 8	" Swing "

ordev

T1					§ "Swing" value, minimum to maximum. ¶ Two capacitors, 1,000pF and 3,550pF, in parallel. $\parallel 0.005\mu F$ in A.C./D.C. model.
		i.c. i.c.	i.c.	i.c	Circuit diagram of the Ferguson Model 353A. The A.C./D.C. version, Model 353U, is covered by the additional power supply circuit inset below, the only
R2:	8 <sup>+</sup> C+ 29	C27	R21 1 R25	+C43	below, the only other differences between these two models in the main diagram being the addition of isolating capacitors drawn in broken line.
	A.C. mains	R23 to RII + C R24 TORIB	V4 V3		LI4 SI3  c lomps  A.C. or D.C.  mains  LI5 SI4

	RESISTORS	Values	Loca- tions
R1 R2 R3 R4	L.W. stabilizer V1 S.G. feed V1 C.G V1 osc, C.G	$\begin{array}{c} 220 k\Omega \\ *47 k\Omega \\ 1 M\Omega \\ 47 k\Omega \end{array}$	G3 E3 G3 F3
R5 R6 R7 R8	Osc. reaction limiter Osc. anode feed Osc. stabilizer V2 C.G	$egin{array}{l} 3 \cdot 9 & \Omega \ + 27 & \Omega \ 220 & \Omega \ 1 & \Omega \end{array}$	F3 F4 F3 E3
R9 R10 R11 R12 R13	$ \begin{cases} A.G.C. \ potential \\ divider \\ V2 S.G. \ feed \\ Volume \ control \\ \dots \end{cases} $	‡270kΩ §1·2MΩ **47kΩ   100kΩ 500kΩ	E3 E4 E3 D3
R14 R15 R16 R17	Volume control V2 A.F. load I.F. stopper G.B. potential { divider}	$10 \text{k}\Omega$ $100 \text{k}\Omega$ $100 \text{k}\Omega$ $39\Omega$ $82\Omega$	E3 E3 E4 E4
R18 R19 R20 R21	V3 C.G Parts tone control { H.T. smoothing {	$470 \mathrm{k}\Omega$ $47 \mathrm{k}\Omega$ $47 \mathrm{k}\Omega$ $47 \mathrm{k}\Omega$ $470 \Omega$	E4 E3 E4 G4
R22 R23 R24 R25	G.B. potential { divider { H.T. smoothing	$820\Omega \\ 33\Omega \\ 150\Omega \\ 820\Omega$	G4 
R26 R27 R28 R29	V4 surge limiter Heater ballast Scale lamp shunt Brimistor CZ2	$140\Omega$ $1,220\Omega$ $1.2k\Omega$	

* 33kΩ ‡ 330kΩ ** 150kΩ	$\left. egin{array}{l} { m A.C./D.C.} \ { m model} \end{array}  ight.$	
¶ Tapped	at $820\Omega + 200\Omega + 200\Omega$ from L	14.
† 22kΩ § 680 kΩ    27kΩ	A.C./D.C model	

ОТЕ	HER COMPONENTS	Approx. Value (ohms)	Loca- tions
L1 L2 L3 L4 L5	Frame aerial S.W. aerial coup L.W. loading coil S.W. aerial tuning	1·5 15·0	G3 G3 G3 F3
L6 L7 L8 L9	S.W. osc. reaction	$\frac{2.7}{12.0}$ $\frac{8.0}{12.0}$	G4 G4 F3 B1
L10 L11 L12 L13	$\left. \begin{array}{l} \text{1st I.F. trans.} \left\{ \begin{array}{l} \text{Pri.} \\ \text{Sec.} \end{array} \right. \\ \text{2nd I.F. trans.} \left\{ \begin{array}{l} \text{Pri.} \\ \text{Sec.} \end{array} \right. \\ \text{Speech coil} \end{array} \right.$	8·0 8·0 6·0 2·5	B1 C1 C1
L14 L15 T1	$\left.\begin{array}{ll} \text{R.F. filter chokes} & \left\{\\ \text{O.P. trans.} & \left\{\begin{array}{ll} \text{Pri.} & \dots \\ \text{Sec.} & \dots \end{array}\right. \end{array}\right.$	3·5 3·5 480·0	 B1
T2	Mains Pri., total H.T. sec., total	41·0 550·0	C2
S1-S10 S11, S12	Waveband switches		G3
S13, S14	Tone control sw:  Mains sw., g'd R13		D3 D3

# **GENERAL NOTES**

GENERAL NOTES

Switches.—\$1-\$10 are the waveband switches, ganged in a single 3-position rotary unit beneath the chassis. The unit is indicated in our underside view of the chassis, and is shown in detail in the diagram in col. 1 overleaf, where it is drawn as seen when viewed from the rear of an inverted chassis.

The table beside it gives the switch positions for the three control settings, starting from the fully anti-clockwise position of the control spindle. A dash indicates open, and C, closed.

\$11, \$12 are the tone control switches, in a 3-position unit beneath the chassis. This is indicated in our underside view of the chassis, and shown again in the diagram in col. 3 overleaf, where it is viewed in the same direction as seen in the chassis drawing.

Scale Lamps.—These are two M.E.S. type lamps, with small clear spherical bubs. In the A.C. /D.C. version they are rated at 6.3 V, 0.3 A, and the A.C./D.C. version they are rated at 8 V, 0.15 A. They are in plastic holders which can be withdrawn from their flat mounting lugs without removing the chassis.

# Waveband Switch Diagram and Table

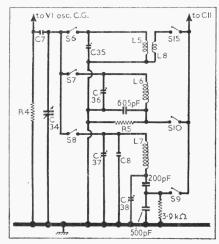


Waveband switches, drawn as seen from the rear of an inverted chassis. On the right is the associated table.

Switches	s.w.	M.W.	L.W.
S1 S2		C	С
\$3 \$4 \$5	0	C	C
S6 S7 S8 S9	C	С	
\$9 \$10		C	C

# **MODIFICATIONS**

There are two versions of the 353 series, an early production version and a late production version. This Service Sheet was prepared from two samples of the late version, and our information is presented as it was in those samples, one A.C., and the other A.C./D.C. Our circuit diagram is based on the A.C. version, but differences in the A.C./D.C. version are shown in the diagram by additional items connected by broken lines, and outside it by a separate section diagram of the A.C./D.C. power supply circuit. Where component values

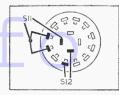


Oscillator circuit of the early version receiver, showing the differences between this and the late version described under "Modifications."

differ between the A.C. and A.C./D.C. models, these are indicated in the component tables. One difference that may be found in all versions is the omission of R1.

Early Version.—Differences between our sample and the earlier production version are numerous, and the oscillator circuit is quite different. A diagram of the earlier oscillator circuit is shown above, where the component

Tone control switches, drawn as indicated in the under-chassis view.



values that are different from ours are shown. C10 was omitted, and so was R7, and R6 was 22 kΩ. The control grid and anode sections were physically transposed on the waveband switch wafer as compared with our switch diagram.

switch wafer as compared with our switch diagram.

There were a few differences in the aerial circuit. C1, which is now 0.001 μF, was 15 pF, and it went to the top of L1 instead of the bottom, so that the external aerial could be used on M.W. and L.W. R1 was omitted, and C32 was permanently connected to the top of L1. C31 was then a fixed 47 pF capacitor, and its position in our plan view was then occupied by C32, which in our sample was a single unit, not part of an assembly. C32 was 70 pF. L2, L3, L4 were mounted on the chassis deck.

In the A.F. circuits, C40 was included in both A.C. and A.C./D.C. versions, and C26 was 0.005 μF. The tone control circuit was omitted from V3 control grid circuit and was connected across C26, but the switch then became a single-pole 3-position unit, and it shunted a 0.01 μF er Chassis of the early production can be recognized by the presence of the aerial coils L2, L3, L4 in the chassis deck, a 2-pin frame aerial plug and an E socket lead soldered to a chassis tag. The late production chassis can be recognized by the absence of tuning coils on the chassis deck, the presence of the lone trimmer C32 mounted vertically on the deck, and the use of a 3-pin frame aerial plug.

CIRCUIT ALIGNMENT

# CIRCUIT ALIGNMENT

LIF. Stages.—Remove chassis from cabinet and stand it on the bench with the frame aerial connected. Switch set to M.W. and turn gang and volume control to maximum. Connect output of signal generator, via an 0.1 µF capacitor in each lead, to the junction of 633 and 62, and to chassis. Feed in a 470 ke/s (638.3 m) signal and adjust the cores of L12 (location reference Cl), L11 (E3), L10 (B1) and L9 (F3) for maximum output, reducing the input as the circuits come into line to avoid A.G.C. action. Repeat these adjustments until no further improvement results.

#### Late Production Models

Late Production Models

R.F. and Oscillator Stages.—Replace chassis in cabinet, leaving the back open to give access to the trimmers but keeping the frame aerial connected. Disconnect signal generator leads and lay them near the frame aerial. The alignment points given in the following instructions are indicated by calibration marks above the clear sections of the tuning scale. Check that with the gang at maximum capacitance the cursor coincides with the vertical marks at the high wavelength ends of the tuning scales.

S.W.—Switch receiver to S.W., tune to 17 Mc/s, feed in a 17 Mc/s (17.65 m) signal and adjust G35 (A1) and G30 (A1) for maximum output, "rocking" the gang while adjusting

voltages were measured on the 10 v and
400 V ranges of a Model 7 Avometer, chassis
being the negative connection in every case.
In the A.C. model, the voltage across 627 was
243 V, across C28 it was 234 V and across R16,
R17 it was 5.7 V. In the A.C./D.C. model the
voltage across C27 was 190 V, across C42 was
166 V and across R23, R24 it was 9.5 V.

VALVE ANALYSIS

Valve voltages and currents given in the tables below are those derived from the manufacturers' information and were measured with the receivers operating from 230 V A.C. mains, the voltage adjustments being set to the 220-230 V tappings. The receivers were tuned to a point at the high wavelength end of the M.W. scale where there was no signal pick-up. Measurements made on early production models were slightly higher than those quoted in our tables.

#### A.C. Model

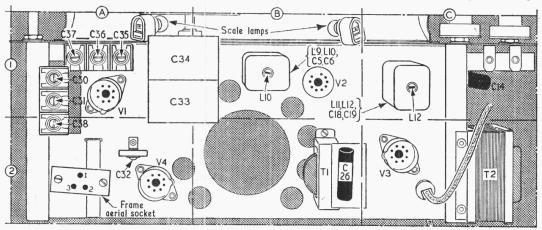
Valve	Anode		Screen	
vaive	V	mA	V	mA
V1 ECH42	{ 220 Oscill	$\left\{egin{array}{c} 2\cdot 4 \ \mathrm{ator} \ 5\cdot 5 \end{array}\right\}$	70	2.9
V2 EBF80	175	4.2	60	1.6
V3 EL41 V4 EZ40	228 240*	26.5	220	3.8

\* A.C. reading, each anode.

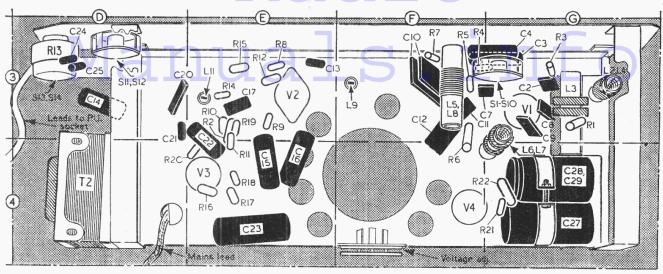
#### A.C./D.C. Model

Valve	And	ode	Ser	een
vaive	v	mA	V	mA
V1 UCH42 V2 UBF80	$\begin{cases} 150 \\ \text{Oscill} \\ 70 \\ 83 \end{cases}$	3.1	60	2.8
V2 UBF80 V3 UL41 V4 UY41	155 222*	6·0 29·0	85 150	2·5 6·0

\* A.C. reading.



Plan view of chassis, showing the vertically mounted trimmer C32 which in the early version models takes the where place we show C31, this trimmer being replaced by a fixed capacitor. The frame aerial socket is a 2-pin type in the early versions.



Under-chassis view of receiver. The arrows pointing to the tone control and waveband switches indicate the directions in which they are viewed in the diagrams in cols. 1 and 3.

the latter for optimum results. Repeat these adjustments until no further improvement

adjustments until no further improvement results.

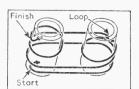
M.W. Oscillator.—Switch receiver to M.W., tune to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust C36 (A1) for maximum output.

L.W.—Switch receiver to L.W., tune to 857 m, feed in an 857 m (350 kc/s) signal and adjust C37 (A1) and C31 (A1) for maximum output. Tune receiver to 1,875 m, feed in a 1,875 m (160 kc/s) signal and adjust C38 (A2) for maximum output, while "rocking" the gang for optimum results. Repeat these adjustments until no further improvement results.

M.W. Aerial.—Replace cabinet back cover and lay the signal generator leads near the frame aerial. Switch receiver to M.W., tune to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust C32 (A2), through the hole provided in the back cover, for maximum output.

# Early Production Models

R.F. and Oscillator Stages.—As calibration marks are not printed on the tuning scale in these models, it will be found difficult to set the cursor accurately for the L.W. trimming and tracking points (on S.W. and M.W. these points coincide with scale divisions), and to facilitate this operation, a substitute tuning scale should be made up in the following way. Measure off on a strip of paper two calibration marks, the first at 1% in, and the second at



Sketch of volume control drive cord system, as seen from front of chassis.

78in from the right-hand edge of the paper. These points represent the cursor settings for L.W. tracking and trimming respectively, and the paper should be held up to the tuning scale with its right-hand edge lined up with the high wavelength ends of the tuning scales.

After completing the LF. stage alignment, replace chassis in cabinet. Disconnect signal generator leads and lay them near the frame aerial. Check that with the gang at maximum capacitance the cursor coincides with the high wavelength ends of the tuning scales.

S.W. and M.W.—Alignment on these bands should be carried out as described for the late production models, but when adjusting the aerial circuit on M.W., the cabinet back must be unfastened at the top to give access to trimmer C32 which is part of the trimmer bank in location A1, and takes the place of C31.

L.W.—Switch receiver to L.W., tune to tracking point on substitute scale, feed in a 1,875 m

mum output. Tune receiver to trimming point on substitute scale, feed in an 857 m (350 kc/s) signal and adjust **637** (A1) for maximum output, while rocking the gang for optimum results.

#### DRIVE CORD REPLACEMENT

DRIVE CORD REPLACEMENT

Tuning Drive.—This is unusual, in that there is a two-to-one step-up drive on the cursor section of the cord, devised by means of an anchored loop to which the cursor is attached. Altogether, about five feet of high-grade flax fishing line, plaited and waxed, is required, and it is divided into three lengths.

First make the cursor loop. This consists of a cord with a small loop at each end, measuring 134in overall. The two loops are slipped over the anchor stud and preferably pulled uptight so that they won't slip off. The large loop so formed is identified as the cursor loop in the accompanying sketch, which shows the complete system as seen from the front with the gang at maximum.

Next make up the cord L. For this take about 20in of cord and tie the left-hand eyelet L to one end of it, but doing so while the anchored loop lies in the eyelet groove, so that not only the eyelet but the loop also is included. At the remote end of cord L make a small loop for anchoring, so that the overall length of cord L is 184in. Then hook the end loop to the tension spring and run the cord as shown in the sketch.

Now take about 26in of cord for cord R, and tie one end to eyelet R, again including the cursor loop. Make a small loop at the far end big enough to take a 4BA screw, so that the overall length is 234in. The cord system is now completely made up, and cord R is run as shown in the sketch, pulling against the gang stop all the way, until the end loop is anchored to the boss screw in the gang drum, as shown. The tension can be eased while fixing this end by slipping the spring off its anchor temporarily.

The cursor should be fitted afterwards, and is adjusted as described under "Circuit Alignment."

adjusted as described under "Circuit Alignment."

Volume Control Drive.—The volume control is offset from its control knob by about an inch and a half, and the drive is transferred to it by cord of the same type as is used for the tuning drive. Two feet of cord is ample.

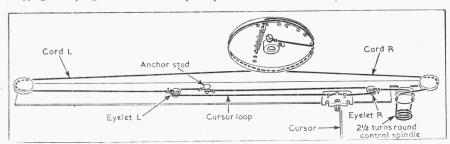
The cord is run as shown in the accompanying sketch (col. 4) where it is drawn as seen from the front with the mains switch in the "off" position, starting and froishing as indicated by tying knots in the cord, but the full procedure is complicated by the necessity of moving the volume control to obtain tension.

First slacken the volume control fixing nut under the left-hand drum, using a thin spanner of %in between flats, and slide the volume control along towards the right-hand drum as tar as it will go, and tighten up nut lightly.

Run the cord as shown, anchoring it to the drums by means of the slots, and make it as tight as possible. Then slacken the fixing nut again and pull the volume control advance to a stight as possible away from the right-hand drum, working the control backwards and forwards to allow the slack to be taken up, and tighten up the nut again with the cord in firm tension. A touch of Durofix on the knots will prevent them from slipping.

# DISMANTLING

Removing Chassis.—Remove back cover and unplug frame aerial lead (on Early Versions unsolder chassis lead from E socket); unsolder leads from speech coil tags on speaker; remove two wood screws securing P.U. socket panel to side of cabinet; remove four self-tapping screws and large washers securing chassis to cabinet (in the A.C./D.C. model the screw heads are covered by agreement of the screw heads are covered by agreement the screw heads are covered by agreement the screw heads are self-tapping to the screw heads are covered by agreement the screw heads are self-tapping to the screw heads are covered by agreement the screw heads are self-tapping to the screw heads are self-tapping to the screw heads are covered by a screw heads are self-tapping to the screw heads are self-tapping to the screw heads are self-tapping to the screw heads are covered by the screw heads are self-tapping to the screw heads are self-tappin by cardboard insulating caps which must first be prised off); withdraw chassis complete with knobs.



Sketch of tuning drive system, drawn as seen from front of chassis with the gang at maximum capacitance. There are three cords in the system, one of which, the cursor loop, is tied to an anchor stud to effect a two-to-one step-up in cursor movement.

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