"TRADER" SERVICE SHEET



BATTERY-OPERATED receiver using 2 V valves and an accumulator, the Ferranti 615 is a 4-valve 3-band table superhet employing a Q.P.P. output stage. A strong metal bracket is fixed to the chassis deck to support the H.T. battery, and it provides a useful support on which to invert the chassis for service work

The differences in an early receiver of the same type, model 648, are fully described, but this Service Sheet was prepared from a model

Release dates and original prices: 615, February 1951, £13 18s; 648, February 1948, £13 11s 10d. Batteries and purchase tax extra.

### CIRCUIT DESCRIPTION

Aerial input via coupling coils L2 (S.W.), L3 (M.W.) or L4 (L.W.) to single tuned circuits L5, C28 (S.W.), L6, C28 (M.W.) and L7, C28 (L.W.) which precede triode pentode valve (V1, Mazda TP25) operating as frequency changer with internal coupling. I.F. rejection by L1, C1, Oscillator grid coils L8 (S.W.), L9 (M.W.) and L10 (L.W.) are tuned by C29. Parallel trimming by C30 (S.W.), C31 (M.W.) and C9, G32 (L.W.); series tracking by C10 (S.W.), C11 (M.W.) and C12 (L.W.). Reaction coupling from anode circuit by L11 (S.W.), L12 (M.W.) and L13 (L.W.). Second valve (V2, Mazda VP23) is a variable.

Second valve (V2, Mazda VP23) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C3, L14, L15, C4 and C15, L16, L17, C16. Intermediate frequency 470 kc/s.

Models 615 & 648

Diode signal detector is part of double diode triode valve (V3, Mazda HL23DD). Audio frequency component in rectified output is

triode valve (V3, Mazda HiL23DD). Audio frequency component in rectified output is developed across diode load R10, and is passed via C20 and volume control R11 to grid of triode section which operates as A.F. amplifier. I.F. filtering by C18, R9, C19 and C21.

Second diode of V3 is fed from V2 anode via C17 and the resulting D.C. potential developed across R13 is fed back as bias to V1 and V2 giving automatic gain control. On S.W., V1 control grid circuit is not biased by the A.G.C. voltage, but by the negative voltage developed across R3, which together with R2 forms the oscillator grid leak.

Series-fed transformer coupling by T1 between

Scries-fed transformer coupling by T1 between V3 triode and quiescent push-pull output valve (V4, Mazda QP25). Tone control by R18, C23 and R17. G.B. for V4 is developed across R14, R15 in the H.T. negative lead to chassis. A proportion of this voltage, that across R14, is used as bias for V3 triode section, as delay bias for the A.G.C. diode and as standing bias for V1 and V2.

## **VALVE ANALYSIS**

Valve voltages and currents given in the table below are those derived from the manufacturers' information and were measured with the receiver operating from a new 120 V H.T. battery and a fully charged 2 V L.T. accumulator. The receiver was switched to M.W., with the gang at maximum capacitance, but there was no signal input. signal input.

Voltages were measured with a Model 7 Avometer, chassis being the negative connection in

Valve	Anode		Se	reen
7 41 7 0	V	mA	V	mA
V1 TP25	$\begin{cases} 111 \\ \text{Oscil} \\ 93 \end{cases}$	$\left\{ egin{array}{c} 0.4 \ \mathrm{Hator} \ st \end{array}  ight\}$	48	0.92
V2 VP23 V3 HL23DD V4 QP25	111 110 110	1·4 1·45 4·5†	48 111	0·92 1·0

\* No reading quoted. † Total current measured at T2 primary centre tap.

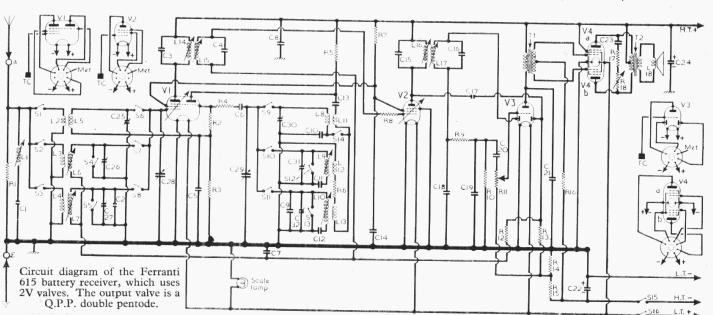
# COMPONENTS AND VALUES !!

	RESISTORS	Values	Locations
R1	Aerial shunt	$33k\Omega$	F4
R2	V1 osc. grid leak {	$33\mathrm{k}\Omega$	F3
R3	)	$15 \mathrm{k}\Omega$	F3
R4	Osc. stabilizer	$47\Omega$	F3
R5	Osc. anode load	$4.7 k\Omega$	F4
R6	Osc. stabilizer	$470\Omega$	G3
R7	S.G. H.T. feed	$47 \mathrm{k}\Omega$	F4
R8	V2 C.G. stopper	$2.2 \mathrm{k}\Omega$	A2
R9	I.F stopper	$47k\Omega$	F4
R10	Signal diode load	$470 \text{k}\Omega$	E4
R11	Volume control	$1M\Omega$	E3
R12	A.G.C. decoupling	$2.2M\Omega$	E4
R13	A.G.C. diode load	$2 \cdot 2 M \Omega$	D4
R14	Transcap (	$100\Omega$	D3
R15	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	$*650\Omega$	D3
R16	V4, C.G	$47 k\Omega$	D4
R17	Part tone control	$15k\Omega$	D3
R18	Tone control	$500 \mathrm{k}\Omega$	D3

\* Two resistors,  $680\Omega$  and  $15k\Omega$ , in parallel.

	CAPACITORS	Values	Loca- tions
C1	Part I.F. rejector	30pF	F4
C2	L.W. aerial trim	80pF	G4
C3	1 1st I.F. trans. tun- 6	105pF	A2
C4	f ing	105pF	A2
C5	S.W. G.B. decoup.	$0.1 \mu F$	$E_3$
C6	V1 osc. C.G	$100 \mathrm{pF}$	F3
C7	A.G.C. decoupling	$0.1 \mu F$	$E_3$
C8	H.T. by-pass	$0.1\mu F$	F4
C9 -	L.W. osc. trim	100pF	G3
C10	S.W. osc. tracker	$0.004 \mu F$	F3
C11	M.W. osc. tracker	470pF	G3
C12	L.W. osc. tracker	130pF	G3
C13	Osc, anode coup	$0.001 \mu F$	F3
C14	S.G. decoupling	$0.1 \mu F$	E3
C15	2nd I.F. trans. tun- (	105pF	B2
C16	} ing {	$180 \mathrm{pF}$	B2
C17	A.G.C. coupling	50 pF	$E_4$
C18		130pF	E4
C19	} I.F. by-passes {	130pF	E4
C20	A.F. coupling	$0.02 \mu F$	E3
C21	A.F. coupling I.F. by-pass	400pF	D4
C22*	G.B. by-pass	$25\mu F$	D4
C23	Part tone control	$0.02 \mu F$	D4
C24*	H.T. reservoir	$8\mu F$	E3
$C25\ddagger$	S.W. aerial trim	$50 \mathrm{pF}$	A2
C26‡	M.W. aerial trim.	$50 \mathrm{pF}$	A2
C27‡	L.W. aerial trim	50pF	A2
C28†	Aerial tuning		B1
C29†	Oscillator tuning	-	B1
C30‡	S.W. osc. trim	50pF	A1
C31‡	M.W. osc trim	50pF	A1
C32‡	L.W. osc. trim	50pF	A1

\* Electrolytic † Variable. ‡ Pre-set.



отн	ER COMI	PONENTS		Approx. Values	Loca
		\/  '		(Ohms)	
L1	I.F. reje	ctor .		18.0	F4
L2	Aerial	coupling		_	G4
L3	coils	coupling	3	29.0	G4
L4	Cons		(	45.0	G4
L5	)				G4
L6	Aerial t	uning coi	ls 〈	3.5	G4
L7	J -		U	17.0	G4
L8	Occillate	or tuning		-	F3
L9	coils	n tuning	3	3.5	G3
L10	Cons		[	12.0	G3
L11	Oscillato	or reaction	. (	Parameter .	F3
L12		or reaction	- {}	1.0	G3
L13	coils		[	3.0	G3
L14	1-47 17 4	[]	Pri.	7.0	A2
L15	} 1st I.F. t	rans. is	ec.	7.0	A2
L16	LOUITE	m	ri.	7.0	B2
L17	} 2nd I.F.	Trans. $\left\{ \begin{array}{l} \mathbf{I} \\ \mathbf{S} \end{array} \right\}$	ec.	7.0	B2
L18	Speech			2.5	-
T1	Intervalve	(Pri.		900.0	D4
	trans.	(Sec., to	tal 10	0.000.0	
T2	O.P. trans.	Pri., to	tal	420.0	C2
		(366			
S1-S14 S15,	Waveba	nd switche	S	Normalia	. G3
S16	Batt sw	., g'd R18		Part and the last of the last	D3

#### GENERAL NOTES

Switches.—\$1-\$14 are the waveband switches, ganged in two rotary units beneath the chassis. These are indicated in our underside view of the chassis, and shown in detail in the diagrams inset beside our plan view illustration, where they are drawn as seen from the rear of an inverted chassis. The table below them gives the switch positions for the three control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed.

\$15, \$16 are the Q.M.B. battery switches, ganged with the tone control R18.

\$cale Lamp.—Any low-consumption 2.5 V lamp with an M.E.S. base can be used. The original lamp was rated at 2.5 V, 0.15 A.

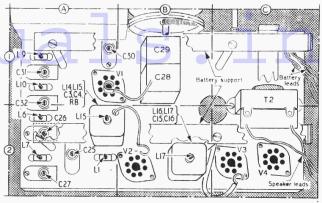
External Speaker.—No provision is made for this, but if one is used its impedance should be about 3-4 Ω. The makers say in their instruction book that an external speaker should not be used.

Batteries.—A 2 V accumulator is required for L.T., and a capacity of 40 AH or more is recommended. Space is available for it in the ashingt.

Batteries.—A 2 V accumulator is required for L.T., and a capacity of 40 AH or more is recommended. Space is available for it in the cabinet. A substantial steel shelf support is mounted on the chassis deck to hold the H.T. battery, which should be of the "super-power" type rated at 120 V. Sizes up to 12in×6in×3\frac{1}{2}in can be accommodated on the shelf.

Model 648.—This was the predecessor of the model 615, and basically both designs were alike. Detailed differences in the 648 as compared with our information here, which was all based on our sample 615, are as follows:—

L1 is fixed, and C1 is 70 pF pre-set. An image rejector of similar design to this is shunted across L4. It should be adjusted by feeding in a strong 247 m (1,214 kc/s) signal, tuning in the



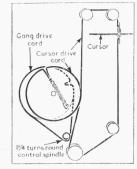
Plan view of the chassis. V1, V2, V3 have top cap connectors.

Waveband switch units, with table (below).

Switches	S.W.	M.W.	L.W.
S1	С		
S2		C	
S1 S2 S3 S4 S5 S6 S7	-		С
84	c		
S5	C	С	
86	C		
87		С	***************************************
\$8 \$9	-		C
89	С		-
S10	-	С	-
S11	Management		C
S12	C		-
S13	C	C	-
S14	С		

image at about 1,056 m, and adjusting the trimmer for minimum output. (It was originally intended for 261 m, with the image at 1,370 m.)

L6 core is not adjustable, and L7, L9, L10 are air-cored. Pre-set trackers of 200 pF (plus 400 pF fixed) and and 70 pF (plus 150 pF fixed) replace C11 and C12. R6 is omitted, and the three



Sketch of the drive tuning system, seen from the front. The gang and cursor have separate drive drums.

reaction coils are switched independently like the tuning coils. L11 and L12 return to chassis via the trackers.

Three scale lamps are provided, one for each waveband, and only the appropriate lamp lights. R9, C18, C19 are housed in the I.F. can, and their values are  $100\,\mathrm{k}\Omega$  and  $150\,\mathrm{pF}$ , C2 is  $50\,\mathrm{pF}$ ; R8 is  $2.7\,\mathrm{k}\Omega$ ; and the intermediate frequency is  $465\,\mathrm{ke}/\mathrm{s}$ . Coil resistances are generally lower.

Drive Cord Replacement.—The gang drive and cursor drive are separate cords with separate frums on the gang spindle. The gang cord requires about  $15\mathrm{in}$  of nylon braided glass yarn, and the cursor drive  $36\mathrm{in}$ . They should be run as shown in the sketch above.

shown in the sketch above.

# CIRCUIT ALIGNMENT

I.F. Stages.—Switch receiver to L.W. and turn gang to maximum capacitance. Connect signal generator output, via an 0.1 µF capacitor in the "live" lead, to control grid (top cap) of V1 and chassis. Feed in a 470 kc/s (638.3 m) signal and adjust the cores of L17 (location reference B2) L16 (E4), L16 (A2) and L14 (F4) for maximum output. Repeat these adjustments until no further improvement results.

R.F. and Oscillator Stages.—Transfer signal generator leads, via a standard dummy aerial, to A and E sockets. Check that with the gang at maximum capacitance, the cursor coincides with the marks at the high wavelength ends of

at maximum capacitance, the cursor coincides with the marks at the high wavelength ends of the tuning scales.

M.W.—Switch receiver to M.W., tune to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust C31 (A1) for maximum output. Feed in a 228 m (1,316 kc/s) signal and tune receiver to it. Adjust C26 (A2) for maximum output. Tune receiver to 500 m, feed in a 500 m (600 kc/s) signal, and adjust the cores of L9 (A1) and L6 (A2) for maximum output, rocking the gang while adjusting L9 for optimum results. Repeat these adjustments until no further improvement results. results

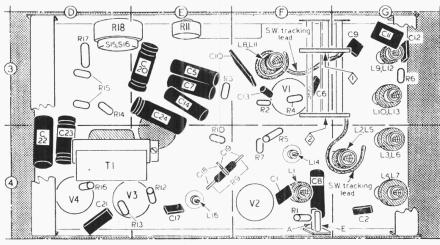
I.F. Rejector.—With the receiver switched to

results.

I.F. Rejector.—With the receiver switched to M.W., turn gang to maximum capacitance. Feed in a 470 kc/s (688.3 m) signal and adjust the core of L1 (A2) for minimum output.

L.W.—Switch receiver to L.W., tune to 1,128 m, feed in an 1,128 m (266 kc/s) signal and adjust C32 (A2) and C27 (A2) for maximum output. Tune receiver to 1,800 m, feed in an 1,800 m (167 kc/s) signal and adjust the cores of L10 (A1) and L7 (A2) for maximum output, rocking the gang while adjusting L10 for optimum results. Repeat these adjustments until no further improvement results.

S.W.—Switch receiver to S.W., tune to 16.7 m, feed in a 16.67 m (18 Me/s) signal and adjust be found when making this adjustment, the correct one being that which involves the lesser capacitance. Tune receiver to 20 m, feed in a 20 m (15 Mc/s) signal, and adjust C25 (A2) for maximum output, rocking the gang for optimum results. Tune receiver to 45 m, feed in a 45 m (6.67 Mc/s) signal and adjust the position of the thick yellow tracking lead, which is looped round L5 (G4) from the waveband switch, for maximum output, while rocking the gang for optimum results. Repeat these adjustments until no further improvement results. Another tracking lead, round L8, is set at the works.



Underside view of the chassis. Tracking lead adjustments are provided for the S.W. band.