"TRADER" SERVICE SHEET

ACE A.C.

COMPONENTS AND VALUES

	CAPACITORS	Values	Loca- tions
C1	Aerial coupling	500pF	G4
C2§	I.F. filter tune	$820 \mathrm{pF}$	G4
$\overline{\text{C3}}$	A.G.C. decoupling	$0.01\mu F$	F4
C4	Aerial coupling	$0.0033\mu F$	G3
$\tilde{\text{C5}}$	1 1st I.F. trans.	100pF	A2
Č6	tuning	100pF	A2
Č7	H.T. by-pass	$0.01 \mu F$	F4
Č8	L.W. osc. trim	25pF	F3
C98	S.W. osc. tracker	$0.0022 \mu F$	F3
C10	M.W. osc. tracker	380pF	F3
C11	L.W. osc. tracker	150pF	F3
C12	Osc. anode coup	50pF	G3
C13	A.G.C. decoupling	$0.01 \mu F$	G4
C14	S.G. decoupling	$0.01 \mu F$	F4
C15	2nd I.F. trans.	100pF	B2
C16	tuning	100pF	B2
C17	5	120pF	F4
C18	I.F. by-passes }	120pF	F3
C19*	V3 cath, by-pass	$25\mu F$	E4
C20	A.G.C. coupling	23pF	F4
C21	A.F. coupling	$0.05 \mu F$	F3
C22	P.U. tone corrector	250pF	F4
C23	V3 anode decoup	$0.1 \mu F$	E4
C24	A.F. coupling	$0.01 \mu F$	F4
C25	I.F. by pass	250pF	E4
C26	A.G.C. decoupling	$0.01 \mu F$	F4
C27*	G.B. by-pass	$25\mu F$	E3
C28	Part tone control	$0.05 \mu F$	E3
C29*		$16\mu F$	C1
C30*	H.T. smoothing {	$8\mu F$	C1
C31*		$16\mu F$	C1
C22†	G.W. aerial trim		G3
C33‡	M.W. aerial trim		G3
C34‡	L.W. aerial trim		G3
C35†	Aerial tuning	P. Williams	B1
C36‡	S.W. osc. trim		F3
C37‡ C38‡	M.W. osc. trim L.W. osc. trim		F3 F3

* Electrolytic. † Variable. ‡ Pre-set. § Two in parallel.

Covering A51, and "Minigram" and "Mayfair" Autoradiograms

FIVE Ace receivers are covered in this Service
Sheet, which was prepared from an A51
table receiver. The other models are the "Mayfair" MRG535 (single speed) and MRG5335 (3speed) autoradiograms; and the "Minigram"
RGA535 (single speed) and RGAS35 (3-speed)
autoradiograms.

An identical chassis is employed in all five

autoradiograms.

An identical chassis is employed in all five models. It is a 4-valve (plus rectifier) 3-band superhet designed to operate from A.C. mains only of 190-250 V.

Release date (approximate, all ARG models, November 1951) and original prices: A51, March 1951, f19 2s 64; MRGS35, f55 3s 1d; MRGS535, f58 16s 8d; RGA535, f42 13s 1d; RGAS535, f46 6s 7d. Purchase tax extra.

	RESISTORS	Values	Loca
R1 R2 R3 R4	Aerial shunts { V1 osc. C.G V1 osc. stopper	2·2kΩ 10kΩ 47kΩ 120Ω	G4 F4 G4 G3
R5 R6 R7	A.G.C. decoupling Osc. anode feed A.G.C. decoupling	1ΜΩ 22kΩ 1ΜΩ	F4 G4 F4
R8 R9 R10	S.G. H.T. feed I.F. stopper Diode load	$\begin{array}{c} 15 \mathrm{k}\Omega \\ 47 \mathrm{k}\Omega \\ 470 \mathrm{k}\Omega \end{array}$	F4 F4 F4
R11 R12 R13 R14	Volume control V3 G.B V3 H.T. decoupling V3 anode load	1MΩ 2·4kΩ 68kΩ 220kΩ	E3 F4 E4 F4
R15 R16 R17	A.G.C. diode load A.G.C. decoupling G.B. resistors {	$1M\Omega$ $1M\Omega$ 47Ω	F4 D3 D3
R18 R19 R20 R21	} v4 c.g {	150Ω 68kΩ 470kΩ	E4 E4
R22 R23 R24	Part tone control Tone control H.T. smoothing	1·5kΩ 680Ω 50kΩ 500Ω	D3 E3 D3 D3
R25	V4 anode stopper	47Ω	E4

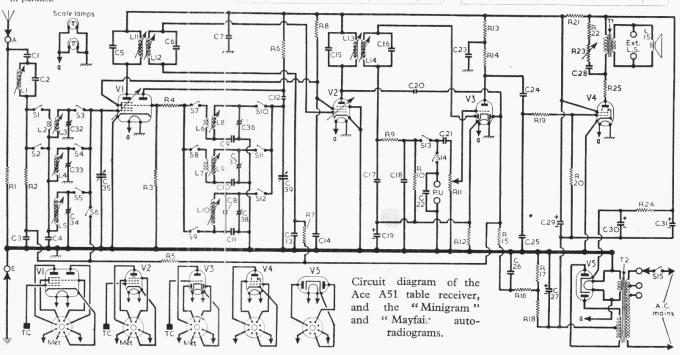


The appearance of the Ace A51.

CIRCUIT DESCRIPTION

Aerial input is inductively coupled on S.W. by L2, and capacitatively "bottom" coupled on M.W. and L.W. by C4 to single tuned circuits L3, C35 (S.W.), L4, C35 (M.W.) and L5, C35 (L.W.) which precede triode hexode valve (V1, Brimar 6K8GT), operating as frequency changer (Continued col. 1 overleaf)

OT	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1 L2	I.F. rejector S.W. aerial coup	1.8	G4 G3
L3 L4 L5	Aerial tuning coils {	$\frac{-}{1\cdot7}$	G3 G3 G3
L6 L7	Osc. reaction coils	$0.4 \\ 1.0$	F3 F3
L8 L9 L10	Oscillator tuning coils	5·5 17·5	F3 F3 F3
L11 L12 L13	} 1st I.F. trans. { Pri. Sec.	8·0 8·0	A2 A2
L14 L15	$\begin{cases} 2 \text{nd I.F. trans.} \begin{cases} \text{Pri.} \\ \text{Sec.} \end{cases} \\ \text{Speech coil} \\ \dots \end{cases}$	5·5 5·5 2·5	B2 B2
T1	O.P. trans. { Pri Sec	$400.0 \\ 0.5$	E3 E3
T2	$\begin{cases} \text{Pri., total } \dots \\ \text{H.T. sec., total } \dots \\ \text{Heater sec.} \dots \end{cases}$	$ \begin{array}{r} 34.0 \\ 450.0 \\ 0.2 \end{array} $	C2
S1-S14 S15	Waveband switches Mains sw., g'd R11		G3 E3



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Circuit Description—continued

with internal coupling. I.F. rejection by L1, C2.
Oscillator anode coils L8 (S.W.), L9 (M.W.) and L10 (L.W.) are tuned by C39. Parallel trimming by C36 (S.W.), C37 (M.W.) and C8, C38 (L.W.); series tracking by G9 (S.W.) C10 (M.W.) and C11 (L.W.).
Second valve (V2, Brimar 6K7CT) is a variable mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C5, L11, L12, C6 and C15, L13, L14, C16. Intermediate frequency 472 kc/s.
Diode signal detector is part of double-diode triode valve (V3, Brimar 6Q7CT). Audio-frequency component in rectified output is developed across load resistor R10 and passed via C21 and volume control R11 to control grid of triode section, which operates as A.F. amplifier. I.F. filtering by C17, R9, C18 and C25.
Second diode of V3 is fed from V2 anode via C20, and the resulting D.C. potential developed across its load resistor R15 is fed back as bias to V1 and V2, giving automatic gain control. Provision is made for the connection of a gramophone pick-up across R11 via S14, which closes in the gram position of the waveband switch control. S6 closes and S13 opens on gram to prevent radio break-through.

Resistance-capacitance coupling via R14, C24 and R20 between V3 triode anode and beem

prevent radio break-through.

Resistance-capacitance coupling via R14, C24
and R20 between V3 triode anode and beam
tetrode output valve (V4, Brimar 6V6GT).
Variable tone control in anode circuit by R22,
R23 and C28. Provision is made for the connection of a low-impedance external speaker
across T1 secondary. Bias for V4 is obtained
from the voltage dropped across R17 and R18
in the H.T. negative lead to chassis.
H.T. current is supplied by I.H.C. full-wave
rectifying valve (V5, Brimar 6X5GT). Smoothing by R21, R24 and electrolytic capacitors C29,
G30, G31.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receiver when it was operating from A.C. mains of 230 V. The receiver was tuned to the highest wavelength end of M.W., but there was no signal input. Voltage readings were measured with an Avo Electronic Test Meter which has a very high internal impedance, and allowance should be made for the extra current drawn by meters of lower impedance. Chassis was the negative connection. connection.

77 - 1	Anode		Screen		Cath.
Valve	V	mA	v	mA	v
V1 6K8GT V2 6K7GT V3 6Q7GT V4 6V6GT V5 6X5GT	$\begin{cases} 230 & \text{Oscil} \\ 115 & \text{230} \\ 70 & \text{260} \\ 280 \dagger \end{cases}$	$ \begin{bmatrix} 2.0 \\ 1ator \\ 4.5 \\ 9.0 \\ 0.45 \\ 38.0 \\ - \end{bmatrix} $	130 130 230	5·8 2·0 2·0 2·0	1·0 310·0

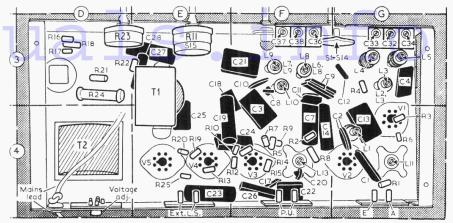
† A.C. reading.

CIRCUIT ALIGNMENT

I.F. Stages.—Switch receiver to M.W. and turn gang to maximum capacitance. Connect output of signal generator, via an 0.1 µF capacitor in the "live" lead, to control grid (top cap) of V1 and chassis. Feed in a 472 kc/s (635.6 m) signal and adjust the cores of L14, L13, L12 and L11 (location references B2, F4, A2, G4) for maximum output. Repeat these adjustments.

R.F. and Oscillator Stages.—Transfer signal generator leads via a suitable dummy aerial, to

generator leads, via a suitable dummy aerial, to A and E sockets.



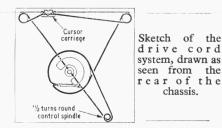
Underside view of the chassis, showing all the R.F. and oscillator adjustments.

L.W.—Switch receiver to L.W., tune to 2,000 m, feed in a 2,000 m (150 kc/s) signal and adjust the cores of L10 (F3) and L5 (G3) for maximum output. Tune receiver to 1,000 m, feed in a 1,000 m (300 kc/s) signal and adjust C38 (F3) and C34 (G3) for maximum output. Repeat these adjustments,

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the cores of L9 (F3) and L4 (G3) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust C37 (F3) and C33 (G3) for maximum output. Repeat these adjustments.

ments.

S.W.—Switch receiver to S.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (F3) and L3 (G3) for maximum output. Tune receiver to 20 m, feed in a 20 m (15 Mc/s) signal and adjust G36 (F3) and G32 (G3) for maximum output. Repeat these adjust-



GENERAL NOTES

Switches.—S1-S12 are the waveband switches, and S13, S14 are the radio/gram change-over switches ganged in a single rotary unit beneath the chassis. This is indicated in our underside view of the chassis and shown in detail in the diagram in col. 3, where it is drawn as seen from the rear of an inverted chassis.

The table below it gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed.

S15 is the Q.M.B. mains switch, ganged with the volume control R11.

the volume control R11.

Scale lamps Speaker leads 0 0 C39 0 0 0 C35 0 (0) •

Plan view of chassis, showing two of the I.F. core adjustments. The remaining I.F. adjustments, together with all the R.F. and oscillator cores and trimmers, are shown in the underside view of the chassis.

Scale Lamps.—These are two Osram lamps, with small clear spherical bulbs and M.E.S. bases. rated at 6.5 V, 0.3 A.

External speaker.—Two sockets are provided at the rear of the chassis for the connection of a low impedance (3-42) external speaker.

Chasis Divergencies.—C25 is shown in the maker's diagram as being connected between V3 triode anode and chassis, whereas in our chassis

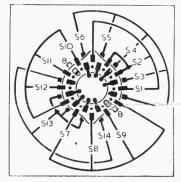


Diagram of the waveband switch unit, drawn as seen from the rear of an inverted chassis. Below is the associated switch table.

Switches	s.w.	M.W.	L.W.	Gram.
S1	С			
S2		С	С	
S3	С			
S4		С		
S5			С	
S6				С
87	С			
88		C		
S9			C	
S10	С	-		
S11	-	C		
S12			С	
S13	С	C	C	
S14				С

it was connected as shown in our diagram, so it may be connected either way. Similarly, we give the value of C19 and that of C27 as $25\,\mu\text{F}$, as they were in our chassis. In other chassis they may be $50\,\mu\text{F}$ each. Our H.T. smoothing electrolytic was as shown in our table, but it is shown in the makers' diagram as being $25\,\mu\text{F}+25\,\mu\text{F}$ for C29 and C31, and a separate $8\,\mu\text{F}$ reservoir for C30. Drive Cord Replacement.—About 50 inches of high grade flax fishing line, plaited and waxed, is required for a new tuning drive cord, which should be run as shown in the accompanying sketch, which is drawn as seen from the rear of the chassis, neglecting obstructions, when the gang is at maximum capacitance.