"TRADER" SERVICE SHEET

BRISTOL. ACE A.C./D.C. RECEIVERS

Covering Model U51 and Ace A.C./D.C. "Minigram" and "Mayfair" Autoradiograms

ASED on the Ace U51 A.C./D.C. table receiver, with which is associated the 535 range of A.C./D.C. autoradiograms, this service Sheet also covers a number of other models. The model numbers of the receivers and radiograms covered are listed below, and in this list are included all A.C./D.C. models styled "Minigram" and "Mayfair," which differ only in cabinet style. No attempt is made to link a particular arrangement with each model number, but the five different arrangements are explained under "Modifications" overleaf.

The basic table receiver is a 4-valve (plus rectifier) 3-band superhet designed to operate from A.C. or D.C. mains of 200-250 V. The mains frequency range (in radiograms) would be limited by the kind of motor employed. Where a radiogram is fitted with an A.C. motor, an electronic convertor unit supplies the motor with A.C. power. Waveband ranges are 16.5-50 m, 190-550 m and 800-2,100 m.

The models covered in this service Sheet are, in numerical order:—

The models covered in this service Sheet are, in numerical order:—
33U (table), 33UR, 33RG/DC, U51, MGU535, MGU535/C, MGUS535, MGU535/C, RGU535, RGU535/C, RGU535, MRGU635 and MRGUS635 are covered except for the omission of their C.R. tuning indicator. Export versions of all models are covered except for their waveband ranges.

Release dates and original prices: 33U (table), November 1950, £15 15s; 33UR, November 1950, £41 18s 6d; 33RG/DC, November 1950, £43 7s 10d; U51, March 1951, £19 0s 6d, increased later to £19 2s 6d; MGU535 or MGU535/C, November

1951, £60 6s 1d; MGUS535 or MGUS535/C, November 1951, £63 19s 7d; RGU535 or RGU535/C, November 1951, £47 16s 1d; RGUS535 or RGUS535/C, December 1951, £51 9s 7d; MRGU635, November 1951, £60 6s 1d; MRGUS635, November 1951, £63 19s 7d.

CIRCUIT DESCRIPTION

Aerial input is inductively coupled on S.W. by L2 and capacitatively "bottom" coupled on M.W. and L.W. by C5 to single tuned circuits L3, C40 (S.W.), L4, C40 (M.W.) and L5, C40 (L.W.) which precede triode-hexode valve (Y1, Brimar 6K8GT) operating as frequency changer with internal coupling. C1 and C4 isolate the aerial and earth sockets from the chassis while R1 provides a D.C. path between the sockets to prevent the build up of static charges on the aerial. R2 prevents modulation hum.

Oscillator anode coils L8 (S.W.), L9 (M.W.) and L10 (L.W.) are tuned by C44. Parallel trimming by C41 (S.W.), C42 (M.W.) and C11, C43 (L.W.); series tracking by C8 (S.W.), C9 (M.W.) and C10 (L.W.). Reaction coupling from grid circuit across the common impedance of the trackers with additional inductive coupling via L6 (S.W.) and L7 (M.W.). Stabilization by R5, R6 and R7.

Second valve (V2, Brimar 6K7GT) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C6, L11, L12, C7 and C16, L13, L14, C17.

Intermediate frequency 472 kc/s.

Intermediate frequency 472 kc/s.

Diode signal detector is part of double diode triode valve (V3, Brimar 6Q7GT). Audio fre-

quency component in rectified output is developed across R12 and passed via C25 and volume control R14 to control grid of triode section, which operates as A.F. amplifier. I.F.

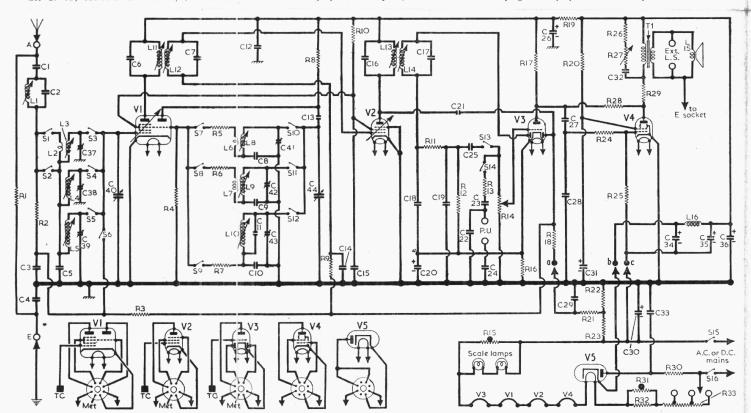
overloped across R12 and passed via C22 and volume control R14 to control grid of triode section, which operates as A.F. amplifier. I.F. filtering by C18, R11 and C19.

Second diode of V3 is fed from V2 anode via C21, and the resulting D.C. potential developed across its load resistor R18 is fed back as bias to V1 and V2 giving automatic gain control. Provision is made for the connection of a gramophone pick-up across R14 via S14 which closes in the gram position of the waveband switch. S6 closes and S13 opens on Gram to prevent radio break-through.

On the table model the P.U. sockets are isolated from chassis by C23 and C24, and shunted by C22. On the radiogram model a transformer isolates the P.U. sockets, one side of its primary being connected to the earth socket, and one side of its secondary to chassis.

Resistance-capacitance coupling via R17, C27 and R25 between V3 triode and beam tetrode output valve (V4, Brimar 25L6GT). Variable tone control by R26, R27 and G32 in V4 anode circuit. Fixed tone correction by negative feedback between the anodes of V4 and V3 via R28. Blas for V4 is obtained from the voltage drop across R22 and R23 in the H.T. negative lead to chassis. A proportion of this voltage, that dropped across R22, is fed via decoupling circuit R21, C29 to the A.G.C. diode and to provide bias for V1 and V2. Provision is made for the connection of a low impedance external speaker across T1 secondary.

H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Brimar 25Z4GT). Smooth-



Circuit diagram of the Ace U51 A.C./D.C. superhet, which is the same as that in all A.C./D.C. "Minigram" and "Mayfair" autoradiograms who motors, an electronic convertor unit, whose diagram is shown on the right of the receiver diagram, is used to drive the motor with A.C. power from D.

ing by R19, choke L16 and electrolytic capacitors C26, C34, C35 and C36.

Valve heaters together with scale lamps, ballast and voltage adjustment resistors R32, R33 and thermistors R15, R31 are connected in series across the mains input. R15 shunts the scale lamps, and R31 protects the valve heaters from current surges.

In the radiogram models a D.C. to A.C. electronic convertor is fitted to supply the gram motor with A.C. from D.C. mains. When the receiver is operated from A.C. mains the convertor switch is set to A.C., opening S17, S18 and closing S19 which connects one side of the motor to the convertor switch S20 connects the mains input across the motor coils via ballast resistor R46.

When the receiver is operated from D.C. mains, the convertor switch is set to D.C., opening S19 and closing S17, S18 which connect the motor coils directly across the output winding of T2. When the motor switch is set to D.C., opening S19 and closing S17, Ils which connect the motor coils directly across the output winding of T2. When the motor switch is sow closed, the electronic convertor is switched on by having its H.T. line connected via S17, motor switch S20 and ballast resistor R46 to the D.C. mains input.

The convertor consists of a two valve 50 c/s

having its H.T. line connected via \$17, motor mains input.

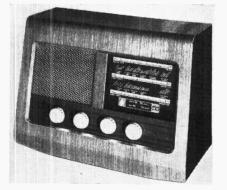
The convertor consists of a two valve 50 c/s multivibrator (V6a, V6b, Brimar 12AU7) whose frequency is governed by the time-constant of \$266, R35 and \$C47, R34. The output from V6a and b is developed across anode load circuit \$17, \$C48, which is tuned to 50 c/s, and passed via \$C49 and \$C50\$ to the control grids of the pushpull connected beam pentode output valves \$(V7, V8, Emitron or Cossor 185BT*s). Output from V7, V8 is coupled via push-pull output transformer T2 and a four-way plug and socket \$5, 6, 7, 8 to the gram motor (pin 7 is blank).

The heater ballast resistor \$852\$ and associated components \$R50, \$R51, \$R53\$ are mounted on the convertor chassis in the radiogram models, and are connected by a four-way plug and socket \$1, 2, 3, 4. The heaters of \$V6\$ are connected in parallel for 0.3 amp operation and together with the heaters of \$V7, \$V8\$ are wired in series with the heaters in the radio chassis. Extra current is passed through \$V7\$, \$V8\$ heaters by ballast and voltage adjustment resistors \$R47\$, \$R48\$ and \$R49\$ to bring their total current, including the H.T. current from the receiver, up to 0.45 amp.

COMPONENTS AND VALUES

	RESISTORS	Values	Loca- tions	
R1)	2·2kΩ	G4	
R2	Aerial shunts {	$10 \mathrm{k}\Omega$	F4	
R3	A.G.C. decoupling	$1M\Omega$	F4	
R4	V1 osc. C.G	$47 \mathrm{k}\Omega$	G4	
R_5	Oscillator stabiliz-	22Ω	F3	
R6		$2 \cdot 2 k\Omega$	F3	
R7	ers	5.6 k Ω	F3	
R8	Osc. anode load	$22 \mathrm{k}\Omega$	G4	
R9	A.G.C. decoupling	$1 M\Omega$	F4	
R10	S.G. feed	$10 \mathrm{k}\Omega$	F4	
R11	I.F. stopper	$47 \mathrm{k}\Omega$	F4	
R12	Diode load	$470 \mathrm{k}\Omega$	F4	
R13	Tone correction	$22\mathrm{k}\Omega$	F4	
R14	Volume control	$1 \text{M}\Omega$	E3	
R15	Thermistor CZ2	2 21 0	D3	
R16	V3 G.B	$2.2k\Omega$	F4	
R17	V3 anode load	$220 \mathrm{k}\Omega$	F4	
R18	A.G.C. diode load	$1M\Omega$	F4	
R19	H.T. smoothing	$1k\Omega$	D3 E4	
R20	V4 S.G. feed	$15k\Omega$	D3	
R21	A.G.C. decoupling	$\frac{1 M \Omega}{68 \Omega}$	D3	
R22	G.B. resistors	$\frac{68\Omega}{22\Omega}$	D3	
R23 R24		$100 \text{k}\Omega$	E4	
R24 R25	V4 grid stopper V4 C.G	470kΩ	E4	
R26	V4 C.G Part tone control	680Ω	D3	
R27	Tone control	50kΩ	D3	
R28	27 / 2 2 3 3	$1M\Omega$	F4	
R29	Neg. teed-back V4 anode stopper	47Ω	E4	
R30	Surge limiter	68Ω	E4	
R31	Thermistor CZ2	0052	C2	
R32)	140Ω	C2	
R33	Heater ballast {	*530Ω	C2	
R34	3 }	47kΩ	K6	
R35	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	47kΩ	K7	
R36	H.T. smoothing	$+20 k\Omega$	K6	
R37	`	$100 \mathrm{k}\Omega$	L6	
R38	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	$100 \mathrm{k}\Omega$	L7	
R39	7 V7, V8 C.G. stop- 3	$1 \mathrm{k} \Omega$	L6	
R40	} pers {	$1 \mathrm{k} \Omega$	L7	
100	Continued next column			

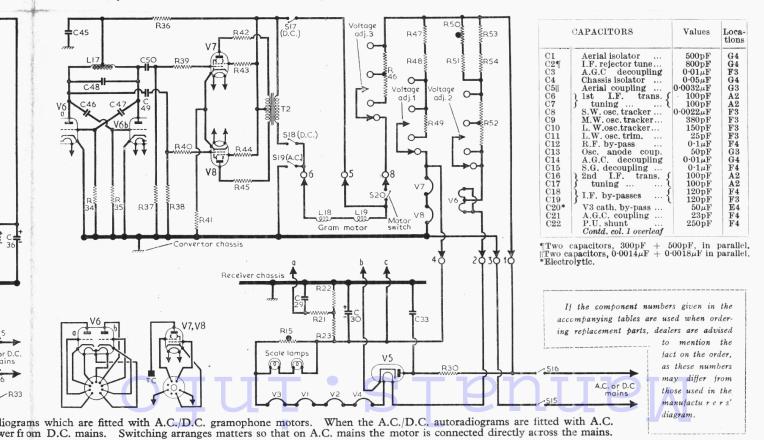
* Tapped at $410\Omega + 60\Omega + 60\Omega$ from R32. † Two $10k\Omega$ resistors in series.



The appearance of the Ace U51 table receiver.

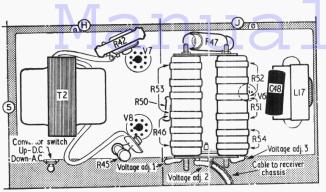
	tions
$\begin{array}{c} {}^{\ddag}34\Omega \\ 68\Omega \\ 1\cdot 1k\Omega \\ 1\cdot 1k\Omega \\ 68\Omega \\ \$120\Omega \\ 1\cdot 49k\Omega \\ 500\Omega \\ 500\Omega \\$	M6 H5 L6 L7 H5 J5 J5 L7 L7 J5 J5 J5
	$\frac{-}{410\Omega}$

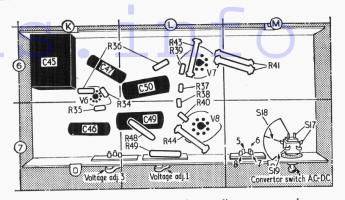
Two 68Ω resistors in parallel. Tapped at $60\Omega + 60\Omega$.



1045 A.C./D.C. RANGE

Supplement to Wireless Electrical Trader, June 7, 1952





Plan view (left) and underside (right) illustrations of the electronic convertor unit. The three voltage adjustment panels are grouped in a triangle at the rear. The A.C./D.C. change-over switch unit \$17-\$19 is replaced by a plug-and-socket device in later models. The 4-pin socket numbered 5, 6, 7, 8 accepts the motor plug.

	CAPACITORS (Continued)	Values	Loca
C23) ($0.1 \mu F$	F4
C24	P.U. isolators {	$0.1 \mu F$	F4
C25	A.F. coupling	$0.1 \mu F$	F3
C26*	H.T. smoothing	$8\mu F$	E3
C27	A.F. coupling	$0.01 \mu F$	F4
C28	I.F. by-pass	$250 \mathrm{pF}$	E4
C29	A.G.C. 1 ecoupling	$0.01 \mu F$	F4
C30*	G.B. by-pass	$50 \mu F$	E3
C31*	V4 S.G. decoup	$8\mu F$	E3
C32	Part tone control	$0.05\mu F$	D3
C33	Mains R.F. filter	$0.05 \mu F$	E4
) Mains Ref. Lines	$16\mu F$	C1
C34* C35*	H.T. smoothing	$16\mu F$	C1
C36*	II.I. smoothing	$12\mu F$	D3
C37†	S.W. aerial trim		G3
C381	M.W. aerial trim		G3
C391	L.W. aerial trim		G3
C40†	Aerial tuning		A1
C41†	S.W. osc. trim		F3
C42†	M.W. osc. trim		F3
C431	L.W. osc. trim.		F3
C44†	Oscillator tuning		A1
C45§	H.T. decoupling	$4\mu F$	K.6
C468) Multi-vibrator re- §	$0.1\mu F$	K7
C47	action coup	$0.1 \mu F$	K6
C48	Osc. anode tune	$0.2\mu F$	J5
C48	\	$0.5\mu F$	L7
C50	Osc. coupling }	$0.5\mu F$	L6

*Electrolytic. †Variable. ‡ §Paper type, not electrolytic ‡Pre-set.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receivers. The figures for V1-V5 were measured in a table model when it was operating from 230 V A.C. mains and tuned to the highest wavelength end of M.W. There was no signal input. The figures for V6-V8 were measured in the convertor unit of a radiogram model when it was switched to D.C., and operating from 230 V D.C. mains with the gram motor running.

Voltage readings were measured with an Avo Clectronic TestMeter, and as this instrument draws no appreciable current, allowance must be made for the current drawn by other types of meter. The A.C. voltage measured across the gram motor input with the converter operating from 230 V D.C. mains was 230 V. The receiver chassis was the negative connection for voltage readings from V1-V5 and the converter chassis for readings from V6-V8.

XX - 1	Anode		Screen		Cath.	
Valve	V	mA	V	mA	V	
V1 6K8GT	192 Osci 105	$\begin{bmatrix} 2 \cdot 6 \\ llator \\ 4 \cdot 0 \end{bmatrix}$	110	5.4		
V2 6K7GT	195	4.7	110	2.4	-	
V3 6Q7GT	95	0.4			1.2	
V4 25L6GT	175	66.0	135	4.5		
V5 25Z4GT	220†			_	230.0	
V6 (a	68	3.0				
12AU7 (b	68	3.0				
V7 185BT	175	115.0	165	16.0	9.5	
V8 185BT	175	115.0	165	16.0	9.5	

† A.C. reading.

DISMANTLING

Removing Chassis .- Remove control knobs (pull-

off) and felt washers; unsolder leads from speech coil tags on speaker; remove four 2BA bolts with washers securing chassis to cabinet and withdraw chassis.

The foregoing applies to the table models only; the fixing is different in the radiograms.

GENERAL NOTES

Switches.—\$1-\$12 are the waveband switches, and \$13, \$14 are the radio-gram change-over switches, ganged in a single rotary unit beneath the chassis. The unit is indicated in our underchassis illustration and shown in detail in the diagram in col. 4, where it is drawn as seen from the rear of an inverted chassis.

The table below it gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and \$\mathbf{C}_c\$, and \$\mathbf{C}_c\$, in a double-pole unit ganged with the volume control \$\mathbf{R14}\$.

Scale Lamps.—These are two M.E.S. lamps, with small clear spherical bulbs rated at 6.5 V, 0.3 A. They are shunted by a Brimistor CZ2,

R15.

External Speaker.—Two sockets are provided at the rear of the chassis for the connection of a low impedance (about 3-4 \Omega) speaker.

Drive Cord Replacement.—About 50 inches of high-grade flax fishing line is required for a new drive cord, which should be run as shown in the sketch in col. 6 where it is drawn as seen from the rear of the chassis, neglecting obstructions, when the gang is at maximum capacitance.

obstructions, when the gang is at maximum capacitance. Capacitor C4.—This is a $4\mu F$ paper type capacitor decoupling the H.T. feed to the convertor oscillator. An electrolytic should not be used as a replacement because if the mains plug is inserted with reversed polarity, this will be applied to the capacitor as soon as the motor is switched on. The motor, of course, will not run under these conditions as the H.T. supply to the anodes of the convertor is reversed.

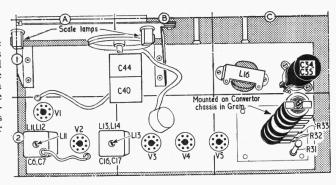
Resistors R30, R42, R45.—These are 68Ω resistors in the anode circuits of heavy-duty valves, and they are rated at 2 W dissipation.

MODIFICATIONS

Export models.—There are two versions of the U51 A.C./D.C. receiver for export, one with S.M.L. wavebands, as in the home version, and one with S.S.M. wavebands. The differences between the circuit of the home model and that of the export versions are that the latter are equipped with a cathode ray tuning indicator (Brimar 6U5G) and that the aerial circuit switching is omitted. ing is omitted.

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	G4 G3 G3 G3
$ \begin{bmatrix} \bar{\textbf{L}}3 \\ \bar{\textbf{L}}5 \\ \bar{\textbf{L}}5 \\ \bar{\textbf{L}}6 \\ \bar{\textbf{L}}7 \\ \bar{\textbf{L}}8 \\ \bar{\textbf{L}}9 \\ \bar{\textbf{L}}9 \\ \bar{\textbf{L}}10 \\ \bar{\textbf{L}}112 \\ \end{bmatrix} $	G3
$ \left. \begin{array}{c} \mathbf{L4} \\ \mathbf{L5} \\ \mathbf{L5} \\ \mathbf{L6} \\ \mathbf{L7} \\ \mathbf{L8} \\ \mathbf{L9} \\ \mathbf{L10} \\ \mathbf{L11} \\ 1 \\ \mathbf$	
$ \begin{array}{c c} L5 \\ L6 \\ L7 \\ L8 \\ L9 \\ L9 \\ L10 \\ L112 \\ \end{array} \begin{array}{c} \text{Reaction coupling } \\ \text{Oscillator tuning} \\ \text{Oscillator tuning} \\ \text{Sec.} \\ \end{array} \begin{array}{c} 40 \cdot 0 \\ 0 \cdot 4 \\ 1 \cdot 0 \\ \hline \\ 1 \cdot 5 \cdot 5 \\ 17 \cdot 5 \\ 9 \cdot 0 \\ \end{array} $	
$ \left\{ \begin{array}{c} 1.6 \\ 1.7 \\ 1.8 \\ 1.9 \\ 1.10 \\ 1.11 \\ 1.12 \\ 1.12 \end{array} \right\} \ \begin{array}{c} 0.4 \\ 1.0 \\ 1.$	
$ \begin{cases} 1.7 \\ 1.8 \\ 1.9 \\ 1.10 \\ 1.11 \\ 1.12 \\ 1 \text{ st I.F. trans. } \begin{cases} -1.0 \\ 5.5 \\ 17.5 \\ 9.0 \\ 9.0 \end{cases} $	G3 F3
$ \begin{array}{c} L7 \\ L8 \\ L9 \\ L10 \\ L11 \\ L12 \\ \end{array} \begin{array}{c} \text{Oscillator tuning} \\ \end{array} \begin{array}{c} -5 \\ 5 \cdot 5 \\ 17 \cdot 5 \\ 17 \cdot 5 \\ 17 \cdot 5 \\ \end{array} $	F3
$egin{array}{ c c c c c c c c c c c c c c c c c c c$	F3
$ \begin{array}{c c} L10 \\ L11 \\ L12 \end{array} $ $ \begin{array}{c c} 17.5 \\ 9.0 \\ 9.0 \end{array} $	F3
$\begin{bmatrix} \mathbf{L}11 \\ \mathbf{L}12 \end{bmatrix}$ 1st I.F. trans. $\begin{cases} \mathbf{Pri.} \\ \mathbf{Sec.} \end{bmatrix} = \begin{bmatrix} 9.0 \\ 9.0 \end{bmatrix}$	F3
$\begin{bmatrix} L11 \\ L12 \end{bmatrix}$ 1st I.F. trans. $\begin{bmatrix} Sec. \\ 9.0 \end{bmatrix}$	A2
112	A 2
L13 Prod I E trops Pri. 6.0	A2
$\left\{\begin{array}{ll} L13 \\ L14 \end{array}\right\}$ 2nd I.F. trans. $\left\{\begin{array}{ll} \operatorname{Pri.} & 6.0 \\ \operatorname{Sec.} & 6.0 \end{array}\right.$	A2
L15 Speech coil 2.5	
L16 Smoothing choke 140.0	C1
L17 Converter osc. coil 650.0	J 5
L18) Gram motor soils 5 230.0	
$\begin{bmatrix} L18 \\ L19 \end{bmatrix}$ Gram. motor coils $\begin{bmatrix} 230.0 \\ 230.0 \end{bmatrix}$	
T1 O.P. trans. $\begin{cases} Pri. \\ Sec. \end{cases} \begin{array}{c} 500 \cdot 0 \\ 0 \cdot 5 \end{array}$	E3
	120
T2 Converter Pri., total 50.0	H 5
U.P. trans (Sec. 050	
S1-S14 Waveband switches —	G3
S15, S16 Mains sw., g'd R14 —	E3
S17- S19 Converter switches —	
S20 Gram, motor sw	M7

Plan view of the receiver chassis as it is in the normal models. In those radiograms which use a convertor, the heater ballast resistor R32, R33 is the convertor in unit.



Where we show \$1 in the home model, there is a short-circuit, and \$2 is omitted, as are \$6 and \$13 also. The switch unit is a simple rotary type with twelve contacts, the tags of two being nipped off, and it has four settings.

Autoradiograms.—There are several series of A.C./D.C. radiograms, with varying type numbers which need not be detailed here, but they divide up electrically into four kinds: (i) uses an unmodified U51 chassis with a single-speed A.C./D.C. record changer; (iii) is like (i) but has a 3-speed A.C./D.C. record changer; (iii) uses a modified U51 chassis with a single-speed A.C. record changer whose motor is run on D.C. mains from an electronic b.C. to A.C. convertor; (iv) is like (iii) but has a 3-speed A.C. record changer whose motor is run from an electronic D.C. to A.C. convertor. The model numbers covered are explained in the introduction and the title of this Service Sheet. Models designed for A.C. mains only are not covered at all.

Universal Motors.—Where the radiogram is fitted with an A.C./D.C. record-changer and the electronic convertor is not needed, a standard U51 chassis is employed, as used in the table receiver, but in some models R13, C22, C23 and C24 are omitted and the pick-up is fed in via a matching transformer. One end of the primary goes to the E socket, and one end of the secondary goes to chassis.

A.C. Motors.—Where the radiogram is fitted with an A.C. record changer, an electronic convertor is used on D.C. mains to supply A.C. to the motor, and the use of this involves physical changes in the chassis as compared with that in the U51 table model, although the circuit is not very different electrically. The same modification with regard to the pick-up input obtains as was described for universal motors.

Convertor Models.—The physical differences involved in the models using the convertor are associated with the power supply components, of which the heater ballast resistor is removed from the radio chassis and is included in the convertor.

the radio chassis and is included in the

convertor.

In order to make this quite clear, the affected part of the receiver circuit is redrawn, in our main diagram overleaf, beneath the convertor circuit as it is in the convertor models, although all the circuit shown below the chassis line of

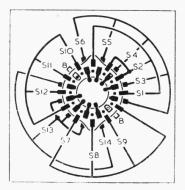
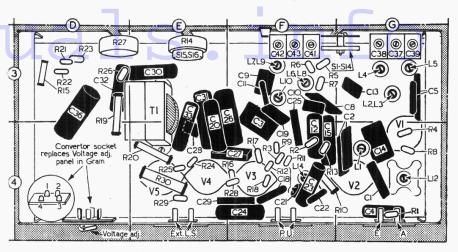


Diagram of the waveband switch unit, drawn as seen from the rear of an inverted chassis. Below is the associated switch table.

Swithces	S.W.	M.W.	L.W.	Gram.
S1	С			
S2		С	C	
83	С		<u>`</u>	
S4	-	С		
S5			С	
86	\			C
S7	С			
S8		С		
S9			С	
S10	С			
S11		С		
S12	-		С	
S13	C	С	С	
S14			-	С

the convertor unit is actually in the receiver chassis. Points **a**, **b** and **c** show where the affected part of the circuit joins the rest of the receiver.

It will be seen that the ballast circuit is a little different from that in the U51, and that



Underside drawing of the radio receiver chassis, with inset at the lower left-hand corner a diagram of the convertor socket which takes the place of the voltage adjustment panel in the convertor-type radiograms.

the heaters of the convertor valves are included in the series heater chain. The two halves of the V6 heater are connected in parallel to match the 0.3 A heater circuit, but the heaters of V7 and V8, which are rated at 0.45 A, are at the "earthy" end of the chain and have a separate ballast resistor R47, R48, R49 which passes 0.15 A, shunting the original heater circuit and bringing the total current for V7, V8 up to the rated value.

Convertor Unit.—The convertor consists of a multi-vibrator type of 50 c/s oscillator driving a push-pull output stage of large-output valves whose output is transformer coupled to the A.C. motor of the gramophone, and it is required, of course, only when the A.C./D.C. receiver is operating from D.C. mains.

Change-over from A.C. to D.C. and vice versa is effected either by a double-pole 2-way switch or a plug-and-socket device. In either case the change-over is represented by switches S17, S18, S19, as explained in "Circuit Description." When a switch is used, its toggle is up for D.C. and down for A.C.; when a plug-and-socket arrangement is used, the plug goes to the upper sockets for D.C., and to the lower ones for A.C.

The gramophone motor is connected to the convertor unit by means of plug and socket for D.C., and to the lower ones for A.C.

The gramophone motor is connected to the convertor unit by means of plug and socket place occupied in normal U51 receivers by the voltage adjustment panel). The mains input to the convertor is via the receiver and then via pins 1 and 3 of the plug, and the heaters are connected in the series via pins 2 and 4. The chassis of the convertor is at a different potential from that of the receiver and then via pins 1 and 3 of the plug, and the heaters are connected in the series via pins 2 and 4. The chassis of the convertor is at a different potential from that of the receiver and the nation of the convertor unit. In our diagram they are numbered 1, 2 and 3. Unfortunately, in our sample at least, all the adjustment panels are not mounted at the

CIRCUIT ALIGNMENT

CIRCUIT ALIGNMENT

It is necessary before carrying out the following alignment procedure to remove the chassis from its cabinet in order to make all the core and trimmer adjustments accessible.

1.F. Stages.—Switch receiver to M.W. and turn gang to maximum capacitance. Connect output of signal generator, via 0.1 µF capacitor in each lead, to control grid (top cap) of V1 and chassis. Feed in a 472 kc/s (685.6 m) signal and adjust the cores of L14 (location reference F4), L13 (A2), L12 (G4) and L11 (A2) for maximum output. Repeat those adjustments.

R.F. and Oscillator Stages.—Transfer signal generator leads, via a suitable dummy aerial, to A and E sockets.

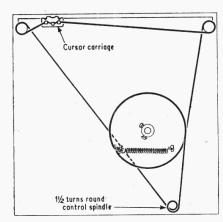
L.W.—Switch receiver to L.W., tune to 2,000 m, feed in a 2,000 m (150 kc/s) signal and adjust the cores of L10 (F3) and L5 (G3) for maximum output. Tune receiver to 1,000 m, feed in a 1,000 m (300 kc/s) signal and adjust C43 (F3) and C39 (G3) for maximum output.

Repeat these adjustments.

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the cores of L9 (F3) and L4 (G3) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust the cores of L9 (F3) and L4 (G3) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust the cores of L9 (F3) and L4 (G3) for maximum output. Repeat these adjustments.

S.W.—Switch receiver to S.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (F3) and L3 (G3) for maximum output.

5.W.—Switch receiver to 8.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (F3) and L3 (G3) for maximum output. Tune receiver to 20m, feed in a 20 m (15 Mc/s) signal and adjust C41 (F3) and C37 (G3) for maximum output. Repeat these (G3) for f adjustments.



Sketch of the drive cord system, drawn as seen from the rear of the chassis, neglecting obstructions.