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# "TRADER" SERVICE SHEET

YE P33TQ 3-band Superhet with R.F. Amplifier

SIGNAL-FREQUENCY amplifier A precedes the frequency changer in the Pye P33TQ, a 5-valve (plus rectifier) 3-band superhet designed to operate from A.C. mains of 200-250 V, 40-100 c/s. Other features include the "Tonemaster" 4-position tone control, using negative feed-back, and a 3-valve amplifier on gram sufficiently sensitive to handle long-playing records.

Release date and original price: April 1951, £23 9s 3d plus purchase tax.

#### CIRCUIT DESCRIPTION

Aerial input via coupling coils L3 (S.W.), L4 (M.W.) and L5 (L.W.) to single tuned circuits L6, C48 (S.W.), L1, L7, C48 (M.W.) and L2, L8, C48 (L.W.), which precede variable-mu pentode valve (V1, Mullard EF41) operating as R.F. amplifier. In areas of good signal strength, use can be made of frame aerial coils L1 (M.W.)

and **L2** (L.W.), which are connected in series with their respective tuning coils **L7**, **L8**.

with their respective tuning coils L7, L8.

Amplified R.F. signals appearing across V1 anode load R2, are coupled via C7 direct to single tuned circuit L12, C51 (S.W.), and via coils L10 (M.W.) and L11 (L.W.) to single tuned circuits L13, C51 (M.W.) and L14, C61 (L.W.), which precede triode-hexode valve (V2, Mullard ECH42) operating as frequency changer. Additional "top" coupling by C11 on M.W. I.F. filtering by C8, L9.

Oscillator anode coils L17 (S.W.), L18 (M.W.) and L19 (L.W.) are tuned by C53. Parallel trimming by C52 (M.W.) and C21 (L.W.); series tracking by C18 (S.W.), C19 (M.W.) and C20 (L.W.) Reaction coupling from grid across the common impedance of the trackers, with additional coupling by L15 (S.W.) and L16 (M.W.).

Third valve (V3, Mullard EBF80) is a double diode R.F. pentode whose pentode section operates as intermediate frequency amplifier with tuned transformer couplings C14, L20, L21, C15 and C95 129 123 29

tuned transformer couplings C14, L20, L21, C15 and C25, L22, L23, C26.

Intermediate Frequency 420 kc/s.

Diode signal detector is part of double diode triode valve (Y4, Mullard EBC41). A.F. component in rectified output is developed across diode load resistor R14 (S43 is closed on radio) and passed via tone control circuit, volume control R22, and G39 to grid of triode section,

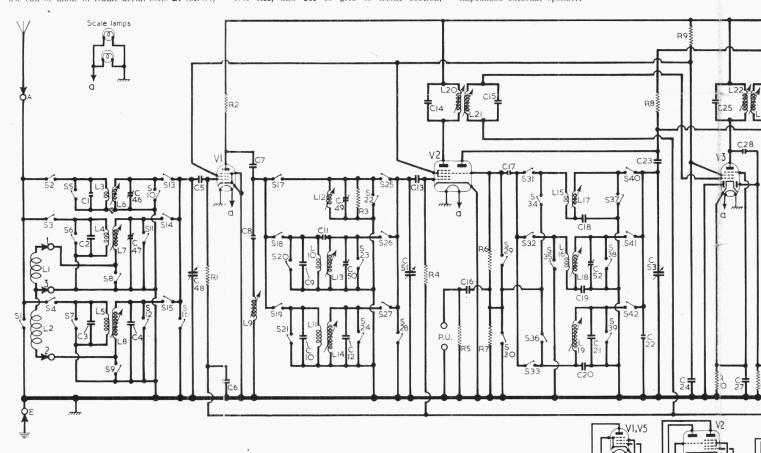
which operates as A.F. amplifier. I.F. filtering by C29, R13 and the capacitance of the screened

One diode of V3 is fed from the pentode anode One diode of **V3** is fed from the pentode anode via **C28**, and the resulting potential developed across **R11** is fed back, via decoupling circuit **R12**, **C6**, as bias for R.F., F.C. and I.F. stages giving automatic gain control. A.G.C. delay is obtained by connecting the A.G.C. line to the second diode of **V4**, and arranging for this diode to conduct while the signal is weak. The delay diode then clamps the A.G.C. line to chassis.

This is achieved by including R11 and R12 in an H.T. potential divider with R26, which has a very high resistance, so that the delay diode anode has a small positive bias and conducts When the potential across R11 rises upon the arrival of a signal, however, its negative polarity tends to offset the positive bias.

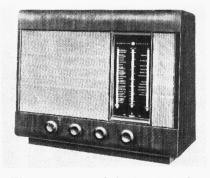
When it becomes large enough, on receipt of a strong enough signal, it neutralizes the bias altogether, and the diode ceases to conduct. The A.G.C. line is then released from chassis and is able to become more and more negative in sympathy with increased signal strength.

Resistance-capacitance coupling by R25, C41 and R27 is employed between V4 triode and pentode output valve (V5, Mullard EL41). Provision is made for the connection of a low impedance external speaker.



Circuit diagram of the Pye P33TQ. L1 and L2 are frame aerial windings, which can be used in many areas where local interference permits, because of the increased gain given by the R.F. amplifier V1. C8, L9 form an I.F. filter. The triode section of the frequency changer V2 is used on gram as a pre-amplifier, and when switched to gram, S43 opens. SX is part of the tone control assembly, on which it consists of two contacts which are always closed. It forms a "through" connection and is not shunted by a wire.

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The appearance of the Pye P33TQ. The two outer knobs are switch controls: left, tone; right, waveband.

Provision is also made for the connection of a gramophone pick-up, using the triode section of the frequency changer \( \mathcal{V} \)2 as a pre-amplifier. When the waveband switch control is turned to gram, \( \mathref{S30} \) opens and \( \mathref{S22} \) closes, connecting the pick-up to the triode grid. The triode output is developed across \( \mathref{R8} \) and passed via tone correcting circuits \( \mathref{R16} \), \( \mathref{C31} \), \( \mathref{R15} \), \( \mathref{C30} \) and \( \mathref{R14} \), \( \mathref{C32} \), \( \mathref{C33} \) to the volume control, \( \mathref{S4} \) being open. Speech voltages in the secondary of the output transformer \( \mathref{T1} \) are tapped off and returned to \( \mathref{V4} \) input circuit, giving negative feed-back affecting the middle and treble frequencies. The overall voltage at \( \mathref{c} \) is returned via \( \mathref{C38} \), \( \mathref{C39} \) directly to the grid of \( \mathre{V4} \), and via switch \( \mathref{Sx} \)

and R18 to the tone control circuit associated with the 5-position switch unit S44-S47, which modifies its effect according to its setting. Sx does not act as a switch, in that it always remains closed, but it forms the connection between S46 and S47.

The path (35, R17, C36, R19 forms a treble filter feed to the tapping on R22, modified by the closing of S46; C34 passing the signal directly to the top of R22. The path C37, R20, R21 provides a bass boost to the tapping, modified by S47. Further tone control is effected by C32 and S45, but not in association with the feed-back circuit.

From the tapping  ${\bf b}$  on  ${\bf T1}$  negative feed-back is applied to the bottom of  ${\bf R22}$ , but this has a fixed frequency characteristic and does not form part of the tone control circuit.

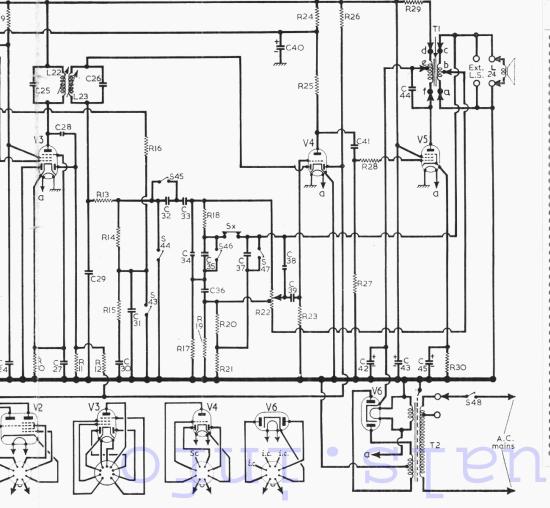
part of the tone control circuit.

H.T. current is supplied by I.H.C. full-wave rectifying valve (V6, Mullard EZ40). Smoothing by R29 and electrolytic capacitors C42, C43, residual hum being neutralized by passing the current through part of the primary winding of the output transformer T1. A single winding on the mains transformer T2 feeds the heaters of all valves, including the rectifier.

Dealers are reminded that the component numbers used in the accompanying tables may be different from those in the makers' circuit diagram. If our component numters are used, therefore, when ordering spares, it is advisable to mention the fact.

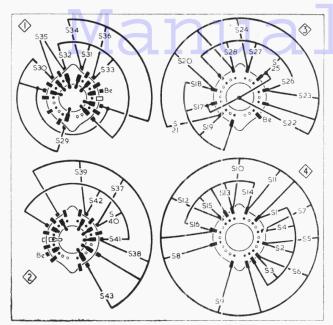
#### **COMPONENTS AND VALUES**

	RESISTORS	Values	Loca- tions
R1	V1 C.G	1ΜΩ	G4
R2	V1 anode load	$4.7 \mathrm{k}\Omega$	G4
R3	S.W. R.F. shunt	$1 \mathrm{k} \Omega$	G4
R4	V2 hex. C.G	$1 \mathrm{M}\Omega$	G4
35	P.U. shunt	$22\mathrm{k}\Omega$	G4
R6	V2 osc. C.G	$47 \mathrm{k}\Omega$	H3
R7	V2 P.U. C.G	$10 \mathbf{M} \Omega$	H3
8	V2 osc. anode feed	$10 \mathrm{k}\Omega$	G3
.9	S.G. H.T. feed	$22 \mathrm{k}\Omega$	G4
110	V3 G.B	$100\Omega$	F4
R11	A.G.C. diode load	$1 \mathrm{M}\Omega$	F4
12	A.G.C. decoupling	$2 \cdot 2 \mathbf{M} \Omega$	F4
13	} Signal diode load {	$470 \mathrm{k}\Omega$	F4
14	Signal diode load	$100 \mathrm{k}\Omega$	E4
15	} Tone correctors {	$10 \text{k}\Omega$	$\mathbf{E4}$
6	folie correctors }	$100 \mathrm{k}\Omega$	G3
17	1	$2.7 \mathrm{k}\Omega$	D3
18	Part of tone control	$2 \cdot 2M\Omega$	D3
19	network	$10 \text{k}\Omega$	D3
20	network	$100 \mathrm{k}\Omega$	-D3
R21	J	$100 \mathrm{k}\Omega$	$D_3$
322	Volume control	$1 M\Omega$	E3
323	V4 C.G	$22 \mathrm{M}\Omega$	E4
24	H.T. decoupling	$4.7 \mathrm{k}\Omega$	F4
25	V4 anode load	$220 \mathrm{k}\Omega$	E4
26	A.G.C. delay	$47 \mathrm{M}\Omega$	E4
R27	V5 C.G	$470 \mathrm{k}\Omega$	E3
228	V5 C.G. stopper	$470 \text{k}\Omega$	E4
329	H.T. smoothing	$1k\Omega$	E4
R30	V5 G.B	$180\Omega$	E4



	CAPACITORS	Values	Location
C1	S.W. aerial shunt	22pF	H4
$\tilde{c}\hat{z}$	S.W. aerial shunt M.W. aerial shunt	100pF	H4
Č3	L.W. aerial shunt	220pF	H4
Č4	L.W. aerial shunt L.W. aerial trim	120pF	H4
ŬŜ.	V1 C.G	100pF	G4
Č6	A.G.C. decoupling	$0.05 \mu F$	G4
07	R. F. counling	100pF	G4
28	Part I.F. filter M.W. R.F. shunt L.W. R.F. shunt M.W. R.F. coupling L.W. R.F. trimmer V2 hex. C.G.	56pF	H4
C9	M.W. R.F. shunt	470 pF	H4
C10	L.W. R.F. shunt	470 pF	H4
C11	M.W. R.F. coupling	$15 \mathrm{pF}$	H4
C12	L.W. R.F. trimmer	$110 \mathrm{pF}$	H4
C13	V2 hex. C.G	$100 \mathrm{pF}$	G4
C14	1 1st 1.F. trans. tun- j	$100 \mathrm{pF}$	B1
C15	} ing }	$100 \mathrm{pF}$	B1
216	P.U. coupling	$0.01 \mu F$	F4
217	V2 osc. C.G	$47 \mathrm{pF}$	H3
218	S.W. osc. tracker	$0.0047 \mu F$	G3
219	M.W. osc. tracker	$620 \mathrm{pF}$	G3
220	L.W. osc. tracker	240pF	H3
221	L.W. osc. trimmer	$150 \mathrm{pF}$	H3
$\frac{022}{023}$	Fixed trimmer	15pF	G3
023	Osc. anode coup	100pF	G3
024	S.G. decoupling 2nd I.F. trans. tun- §	$0.1 \mu F$	F4
	and i.r. trans, tun-	100pF	B2 B2
026	∫ ing \	100pF	F4
027 028	V3 cath. by-pass	$\frac{0.1 \mu \mathrm{F}}{47 \mathrm{pF}}$	F4
028	A.G.C. diode coup.	100pF	F4
C30	I.F. by-pass	$0.05 \mu F$	E4
031	? P.U. tone correctors ?	$0.005 \mu F$	E4
031	?	$0.002 \mu F$	E3
U33	A.F. coupling {	$0.02\mu F$	D3
C34	,	$47 \mathrm{pF}$	D3
U35	1	$0.001 \mu F$	D3
U36	. Part tone control	$0.002 \mu F$	D3
037	Tare conceconcrois	$0.01 \mu F$	E3
038	1.	4.7pF	E3
C39	A.F. coupling	$0.05 \mu F$	<b>E</b> 3
C40*	H.T. decoup	$32\mu F$	Bi
041	A.F. coupling	$0.01 \mu F$	E4
C42*	` '	$60 \mu F$	C1
C43*	H.T. smoothing {	$60 \mu F$	C1
244	Tone corrector	$0.01 \mu F$	D4
C45*	V5 cath. by-pass	$50\mu F$	$\mathbf{E4}$
C461	S.W. aerial trim M.W. aerial trim	50pF	G4
C47‡	M.W. aerial trim	$50\mathrm{pF}$	H4
C48†	Aerial filning	\$532 pF	A1
C49‡	S.W. R.F. trimmer	$50 \mathrm{pF}$	G3
C50‡	M.W. R.F. trimmer	$50 \mathrm{pF}$	H3
$C51\dagger$	R.F. tuning	\$532pF	A1
052‡	S.W. R.F. trimmer M.W. R.F. trimmer R.F. tuning M.W. osc. trimmer	$50 \mathrm{pF}$	H3
$353\dagger$	Oscillator tuning	§532pF	A1
	ectrolytic. † Variable § "Swing" value, min	. ‡ Pre	

#### V/aveband Switch Unit Diagrams and Table



Four diagrams of the three waveband switch units, drawn as seen when viewed in the directions of the arrows our underside drawing of the chassis opposite. Diagrams 1 and 2 are the two sides of the front unit. The associated switch table is on the right of this caption, in col. 3.

Switch	M.W.	s.w.	L.W.	Gram.
S1 S2		С	E	C
\$3 \$4 \$5 \$6 \$7 \$8 \$9 \$10 \$11 \$12 \$13 \$14 \$15 \$16 \$17 \$18 \$19 \$20 \$21 \$22 \$23 \$24 \$25 \$26 \$27 \$28 \$30 \$31 \$31 \$31 \$31 \$31 \$31 \$31 \$31			000000000000000000000000000000000000000	

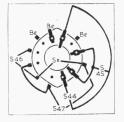
#### Approx. Values OTHER COMPONENTS Loca-(ohms) M.W. frame aerial... L.W. frame aerial... L1 L2 L3 L4 L5 L6 L7 L8 15.0H43.0 Aerial coupling coils 80.0 260.0 G4Very low H4 H4 Aerial tuning coils $10.0 \\ 32.0$ G4 H4 I.F. filter coil L10 L11 L12 L13 L14 L15 L16 L17 L18 L19 G4 H4 H4 G4 H4 40.0 R.F. coupling coils 270.0 Very low 3.0 24.0 R.F. tuning coils... Oscillator reaction Very low $\overline{G3}$ coils Very low 1.9 G3Oscillator tuning G3 H3 1st I.F. trans { Pri. Sec. Pri. 4.2 L20 L2113.9 13.9 Βi L22 2nd I.F. trans { Sec. 13.9 **B**2 13.9 Speech coil L24 2.4 9·0 500·0 T1 $0.2 \\ 0.2$ **B**1 a---b H.T. sec. (total) ... Heater sec. ... Primary (total) ... 600.0 Very low 38.0 T2C2S1-S43 Waveband switches $H_3$ S44-S47 S48 Tone switches Mains switch

#### **GENERAL NOTES**

Switches.—S1-S43 are the waveband and radio/gram change-over switches, ganged in three rotary units beneath the chassis. These are indicated in our under-chassis view by the num-

Switches	Off	- F	В	M	s
S44 S45	С	С		С	_
S46 S47	c		С	С	C

Diagram of the tone control switch unit, as seen from the rear of an inverted chassis.



bers 1-4 in diamond surrounds, 1 and 2 being the two sides of the front unit. These units are shown in detail in the diagrams above, where they are drawn as seen in the directions of the arrows in the under-chassis drawing. The table in column 3 gives

the switch positions for the four control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and **c**, closed.

S44-S47 are the tone control switches, ganged in a single rotary unit beneath the chassis. This unit forms part of an assembly on which is mounted the mains switch S48, and although the tone control has only four positions, a fifth is required for the off position.

The unit is shown in detail in the diagram in col. 2, where it is viewed from the rear of an inverted chassis. The table above it gives the switch positions for the five settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed. One of the switches, S44, plays no part in the action of the tone control. It closes only in the "off" position.

Switch Sx forms part of this group, but it

switch Sx forms part of this group, but it does not function as a switch. It merely provides continuity between the wiring associated with S46 and that associated with S47, and could be replaced by a piece of wire, as it never opens. We show it because our diagram is intended for service work, and if the switch contacts were not shown some confusion might arise from the absence of the connecting wire. Scale lamps.—In our chassis these were two Mazda M.E.S. types, with large spherical bulbs sprayed white. They were rated at 6.5 V, 0.3 A. External Speaker.—Two vertical pairs of sockets are provided on the right-hand panel at the rear of the chassis for the connection of the internal speaker and an external speaker if desired. Either can be muted by withdrawing a plug. The impedance is about 2-4 Ω.

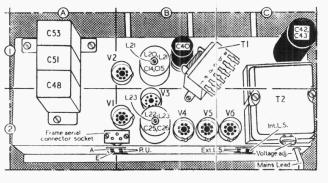
#### CIRCUIT ALIGNMENT

Remove chassis from cabinet and stand it, on its mains transformer end, on the bench. Place cabinet near chassis and re-connect frame aerial plug.

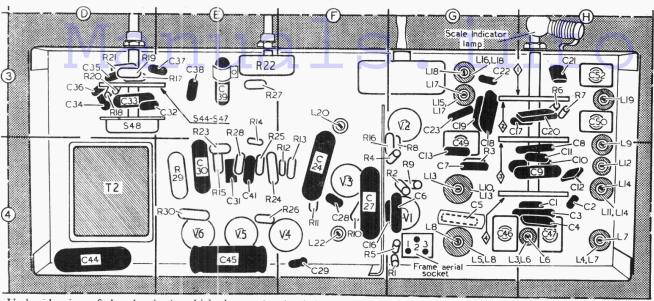
aerial plug.

1.F. Stages.—Connect signal generator output, via a 0.1 µF capacitor in the "live" lead, to control grid (pin 6) of V2 and chassis. Switch set to M.W. and turn gang to maximum. Feed in a 420 kc/s (714.3 m) signal and adjust the cores of L23 (location reference B2), L22 (F4), L21 (B1) and L20 (F3) for maximum output.

I.F. Filter.—Transfer signal generator leads via a dummy aerial to A and E sockets.



Plan view of the chassis. The connecting tags of the output transformer T1 are coded to agree with the circuit diagram overleaf.



Underside view of the chassis, in which the waveband switch units are indicated by the numbers 1-4 in diamond surrounds. The front unit is viewed from both sides, arrows showing the direction of view in the diagrams in col. 1 opposite. A diagram of the tone control switch unit appears in col. 2.

With set switched to M.W., feed in a 420 kc/s signal and adjust the core of L9 (H4) for minimum output.

R.F. and Oscillator Stages.—As the tuning scale remains fixed in the cabinet when the chassis is withdrawn, reference must be made to the substitute tuning scale printed on the rear of the scale backing plate. This scale is numbered 0 to 50, and readings on it are taken

numbered 0 to 50, and readings on it are taken against the top edge of the cursor carriage. Check that with the gang at maximum capacitance the substitute scale reading is 50. When the chassis is in the cabinet the cursor should also coincide with the upper ends of the M.W. and L.W. scales at maximum gang setting. M.W.—With the set switched to M.W., tune to 41 on substitute scale, feed in a 500 m (600 kc/s) signal and adjust the cores of L13 (G4) and L7 (H4) for maximum output. Tune set to 4.2 on scale, feed in a 200 m (1.500 kc/s) signal and adjust 652, 650 (H3) and C47 (H4) for maximum output. Repeat these adjustments until calibration holds at both ends of the scale.

S.W.—Switch set to S.W., tune to 47 on scale,

S.W.—Switch set to S.W., tune to 47 on scale, feed in a 49.3 m (6.1 Mc/s) signal and adjust the cores of L17 (G3), L12 (H4) and L6 (H4) for maximum output. Repeat these adjust-ments until no further improvement results. Feed in a 19.6 m (15.3 Mc/s) signal, tune it in, and adjust **C49** (G3) and **C46** (G4) for maximum

output. Repeat these adjustments until no further improvement results.

L.W.—Switch set to L.W., tune to 24 on scale, feed in a 1,400 m (214 kc/s) signal and adjust the cores of L19 (H3), L14 (H4) and L8 (G4) for maximum output.

#### **VALVE ANALYSIS**

Valve voltages and currents given in the table below are those derived from the manufac-

Valves	Anode		Screen		Cath
vaives	v	mA	V	mA	V
V1 EF41	190 ( 215	4.9	66	1.7	
V2 ECH42		llator 6.3*	66	3.1	
V3 EBF80	215	6.0	66	2.5	0.9
V4 EBC41	65	0.5	en en en	-	
V5 EL41	230	29•0	215	4.5	5.8
V6 EZ40	480†				250.0

<sup>\*</sup> Including 1.3mA passing through R16.

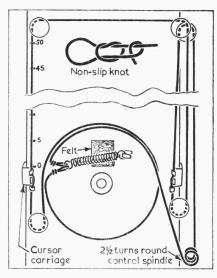
† A.C. volts, each anode

turers' service information and were taken on a receiver while it was operating from A.C. mains of 210 V, the voltage adjustment being set to the 200-220 V tapping. The set was tuned to the high wavelength end of M.W., but there was

o signal input.
Voltage readings were measured with a Model 7 Avometer, chassis being the negative

### DRIVE CORD REPLACEMENT

About six feet of nylon braided glass yarn is required for a new drive cord, and it should be run as shown in the sketch below, where the system is drawn as seen from the rear, with the gang at minimum capacitance. It is helpful to make up the cord before fitting, by tying a



Sketch showing the cord-driven tuning. drive system. It is drawn as seen from the rear of the chassis, neglecting obstructions. The gang minimum.

non-slip loop at each end, the overall length then being 70 inches, as recommended by the makers.

Actually, in our sample the length was one inch shorter than this, so there is some latitude in that direction, although our tension spring was stretched to its utmost, and it was difficult to hook to its anchor. A suggested method of tying a non-slip knot is shown inset in the sketch in the sketch.

Fitting is simplified if the cord is run with the gang at minimum, pulling against the gang stop to hold the cord in position. The cursor can be slipped on afterwards, and should be adjusted so that with the gang at maximum the upper edge of the cursor carriage is level with the top calibration mark (No. 50). At minimum it is roughly level with the zero mark.

#### DISMANTLING THE SET

Removing Chassis.—Remove four control knobs

(pull off); unplug frame aerial leads from top, and speaker leads from rear of chassis; remove two 2BA cheese-head bolts securing rear chassis flange to cabinet, and withdraw

## Service Sheet Correction

An unfortunate error crept into our circuit diagram of the Bush TV22 receiver in Service Sheet 1003/T15, owing to a slip in the drawing office which was not noticed in subsequent checking.

The upper end of the deflector coil secondary d on the line output transformer T2 is shown connected to C31 and Vioa anode, whereas in fact it should go to C<sub>31</sub> and HT positive, where it completes the circuit to the deflector coils via socket **B** and C<sub>34</sub>.

Thanks are due to one of our subscribers for pointing out the error, and dealers are requested to transpose the connection in their diagrams to avoid the possibility of confusion at some later