"TRADER" SERVICE SHEET



THREE wavebands are covered in the Champion "Meteor," a 4-valve (plus rectifier) superhet of compact design. The waveband ranges are 16-49 m, 200-500 m and 800-2,000 m. The receiver operates from A.C. or D.C. mains of 200-250 V.

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The "Comet" is also covered in this Service Sheet, the differences being explained overleaf, but our information was prepared from a "Meteor."

Release dates and original prices:
Meteor, February 1949, £9 198. 6d.;
Comet, October 1947, £14 14s. P.T. extra.

CIRCUIT DESCRIPTION

Tuned frame aerial input, on M.W. only, by L1, C24 which precedes a triode-hexode valve (V1, Brimar 12K8GT) operating as frequency changer with electron coupling. For S.W. and L.W. operation L1 acts as an aperiodic frame aerial, and is inductively coupled by L2 (S.W.) L3 (L.W.) to single-tuned circuits L4, C24

and "COMET" Superhets

(S.W.) or **L5, C24** (L.W.). Provision is made for the connection of an external aerial, via series capacitor C1.

Triode oscillator anode coils L9 (S.W.); L10 (M.W.), L11 (L.W.) are tuned by C28, with parallel trimming by C27 (S.W.), C25 (M.W.), C7, C26 (L.W.), and series tracking by C5 (M.W.), C6 (L.W.). Inductive reaction coupling to C.G. is employed on all bands, with additional capacitative coupling on M.W. and L.W. due to the common impedance of trackers in grid and anode circuits.

Second valve (V2, Brimar metal 12SK7) is a variable-mu R.F. pentode operating

COMPONENTS AND VALUES

	RESISTORS	Values (ohms)	Loca- tions
R1	V1 fixed G.B	220	Н5
R2	V1 osc. C.G	47,000	G_5
R3	Osc. anode load	22,000	G3
R4	V2 fixed G.B	470	F4
R.5	Diode load	470,000	D_5
R.6	Volume control	500,000	D_3
R.7	V3 G.B., A.G.C.		
	delay	6,800	C4
R.8	V3 triode load	220,000	D4
R9	A.G.C. decoup	2,200,000	C4
R.10	A.G.C. diode load	1,000,000	D4
R11	V4 C.G. resistor	470,000	C5
R.12	V4 G.B. resistor	470	C4
R13	H.T. smoothing	3,000	E4
R14	Pilot lamp shunt	40 §	$\mathbf{F}3$
R15	Heater ballast	620†	E4

 $\$ 100 Ω + 68 Ω in parallel.

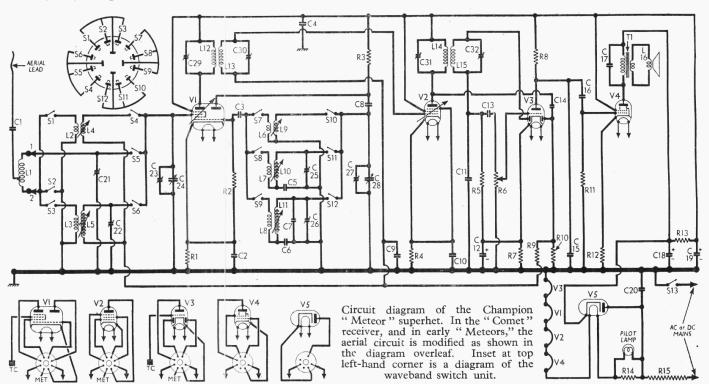
† Line cord.

as intermediate frequency amplifier with tuned transformer couplings C29, L12, L13, C30 and C31, L14, L15, C32.

Intermediate frequency 465 kc/s. Diode second detector is part of double diode triode valve (V3, Brimar 12Q7GT). Audio frequency component in rectified (Continued col. 1 overleaf)

	CAPACITORS	$_{(\mu F)}^{ m Values}$	Loca tions
C1 C2	Aerial series V1 cath. by-pass	0·0003 0·1	B2 F5
C3	V1 cath. by-pass V1 osc. C.G	0.0001	G4
C4	H.T. R.F. by-pass	0.1	E5
C5	Osc. M.W. tracker	0.000576	H5
C6	Osc. L.W. tracker	0.000168	H5
C7	Osc. L.W. tracker	0.00005	G4
Č8	Osc. anode coup	0.00003	H4
C9	A.G.C. decoup	0.1	G5
C10	V2 cath, by-pass	0.1	E5
C11	I.F. by-pass	0.0003	D5
C12*	V3 cath. by-pass	25.0	C4
C13	A.F. coupling	0.01	D4
C14	A.G.C. coupling	0.00005	D4
C15	I.F. by-pass	0.0003	C3
C16	A.F. coupling	0.01	C4
C17	Tone corrector	0.02	E4
C18*		32.0	$\mathbf{E4}$
C19*	H.T. smoothing	32.0	D4
C20	Mains R.F. by-pass	0.002	F4
C21‡	Aerial M.W. trim	_	H_5
C221	Aerial L.W. trim		H4
$C23\dot{1}$	Aerial S.W. trim		A2
C24†	Aerial tuning		A2
C25‡	Osc. M.W. trim		H4
C26‡	Osc. L.W. trim		H_5
C27‡	Osc. S.W. trim	manufile.	A1
C28†	Oscillator tuning	-	A1
C29‡	lst I.F. trans-		$\mathbf{F5}$
C30‡	former tuning (F5
C31‡	2nd I.F. trans-		D5
C32‡	former tuning \	_	E5

* Electrolytic. † Variable. ‡ Pre-set.



ОТ	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13 L14 L15 L16 T1	Frame aerial, total Aerial coupling coils Aerial tuning coils Oscillator reaction coils Oscillator tuning coils 1st I.F. trans. {Pri. Sec. Pri. Speech coil Speaker trans. {Pri. Sec. Speech coil Speaker trans. {Pri. Sec. Speech coil Speaker trans. {Pri. Sec.	1·0 8·0 53·0 Very low 16·5 7·0 1·1 2·0 Very low 3·0 8·5 3·5 3·5 3·5 3·5 2·4 550·0 0·4	A2 G3 G4 G3 G4 H4 H4 H5 H4 H5 A2 A2 B2 B2
S1- S12 S13	W/band switches Mains sw., g'd R6		H3 D3

Circuit Description—continued

output is developed across load resistor R5 and

output is developed across load resistor R5 and passed, via C13 and volume control R6, to grid of triode section, which operates as A.F. amplifier. I.F. filtering by C11 in diode circuit, and C15 in triode anode circuit.

Second diode of V3, fed from V2 anode via C14, provides D.C. potential which is developed across load resistor R10 and fed back, through a decoupling circuit R9, C9, as G.B. to F.C. (except on M.W.) and I.F. valves, giving A.G.C.
Resistance-capacitance coupling by R8, C16, R11 between V3 triode and beam tetrode output valve (V4, Brimar 35L6CT). Fixed tone correction by C17 in tetrode anode circuit.

When the receiver is operated from A.C. main H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Brimar 35Z4CT) which, with D.C. mains, behaves as a low resistance. Smoothing by resistor R13 and electrolytic capacitors

D.C. mains, behaves as a low resistance. Smoothing by resistor R13 and electrolytic capacitors C18, C19.

Valve heaters, together with pilot lamp (shunted by R14) and line cord ballast resistor R15, are connected in series across mains input. Mains R.F. filtering by C20.

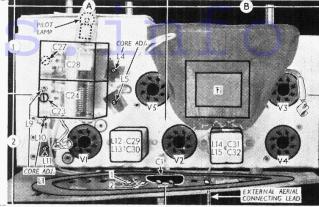
DISMANTLING THE SET

Removing Chassis.—Remove the three control knobs (recessed grub screws) and the three self-threading screws (with washers) located inside rubber feet on the base of the cabinet. The chassis and speaker may now be slid from the cabinet as a single unit.

GENERAL NOTES

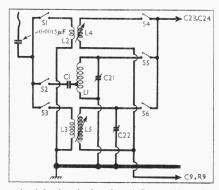
Switches.—S1-S12 are the waveband switches, ganged in a single rotary unit beneath the chassis. This is indicated in our under-chassis view, and shown in detail in the diagram inset in the top left-hand corner of the circuit diagram, where it is drawn as seen from the rear of an inverted chassis. S1, S4, S7, S10, close on S.W., S2, S5, S8, S11 close on M.W. and S3, S6, S9, \$12 close on L.W. (knob fully clockwise).

Plan view of the chassis, with the back cover, carrying the frame winding Li and external aerial isolating capacitor C1. The frame connecting tags I and 2 are indicated. The external aerial connection is a short piece of flexible wire.



Pilot Lamp.—This is rated at 2.5 V, 0.15 A. It has a small clear spherical bulb and an M.E.S. base.

Drive Cord Replacement.—The cord is very simple, and a sketch to describe is unnecessary. A single loop of good quality fine gauge twine twelve inches in circumfer-ence makes about three-quarters of a turn round the drum and 1½ turns in the same direction round the V-shaped groove on the



Aerial circuit in the "Comet" and early "Meteor."

control spindle. The join the cord is hooked on to the tension spring. Access is gained to the drive by removing the pointer and scale. Chassis Divergencies.—Some early Meteor receivers had large I.F. transformer units with the trimmers on top and R14 may not consist of a 10002 and a 68 Ω resistor connected in parallel. In some early cases the aerial circuit was different from that in our diagram, the frame aerial operating only on M.W. The early circuit is shown in the diagram above.

Comet Model.—The Comet is in general very much like the early Meteor, but the aerial isolating capacitor is 0.002xF, and a 0.005xF tracking capacitor is inserted between the junction of L6 and L9 and chassis. The line cord is different, too, having four leads at the receiver end, two coming from tappings on the resistance element which forms R14, R15 and a surge limiter. The arrangement is as follows: Two scale lamps are used, connected in series across R14 which becomes 2002. The next tapping is 60002 further on, to supply V5 anode. A third section of 20002 completes the line cord.

CIRCUIT ALIGNMENT

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1.F. Stages.—Switch set to M.W., turn gang and volume control to maximum, connect signal generator (via an 0.1 µF isolating capacitor in each lead) to control grid (top cap) of V1 and chassis, feed in a 465 kc/s (645.16 m) signal, and adjust C32, C31, C30, C29 (location references E5, D5, E5) for maximum output.

R.F. and Oscillator Stages.—With the gang at maximum capacitance the pointer should be horizontal. Transfer "live" signal generators lead and series capacitor to aerial connecting lead, via a suitable dummy aerial.

S.W.—Switch set to S.W., tune to 16 m on scale, feed in a 16 m (18.75 Mc/s) signal, and adjust C27 (A1) and C23 (A2) for maximum output. Tune to 49 m on scale, feed in a 49 m on the control of the cores of L9 (A1) and L4 (A1) for maximum output. Repeat these operations until no improvement results. results.

results.

M.W.—Switch set to M.W., tune to 200 m on scale, feed in a 200 m (1,500 kc/s) signal, and adjust C25 (H4) and C21 (H5) for maximum output. Tune to 500 m on scale, feed in a 500 m (600 kc/s) signal, and adjust the core of L10 (A2) for maximum output. Repeat these operations until no improvement results.

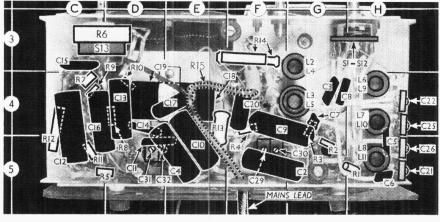
L.W.—Switch set to L.W., tune to 1,000 m on scale, feed in a 1,000 m (300 kc/s) signal, and adjust C26 (H5) and C22 (H4) for maximum output. Tune to 2,000 m on scale, feed in a 2,000 m (150 kc/s) signal, and adjust the cores of L11 (A2) and L5 (A2) for maximum output. Repeat these adjustments until no improvement results. results.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receiver when it was operating from A.C. mains of 233 V. The receiver was tuned to the lowest wavelength on the M.W. band, and the volume

control was at maximum, but there was no signal input.
Voltages were measured on the 400 V range of a model 7 Avometer, except cathode voltages, which were measured on the most convenient range, and chassis was the negative connection.

X - 1	Anode		Screen		Cath.	
Valve	V	mA	v	mA	\mathbf{V}^{-}	
V1 12K8GT	$\begin{cases} 73 \\ \text{Oscil} \\ 42 \end{cases}$	$\left\{ \begin{array}{c} 1 \cdot 3 \\ \text{lator} \\ 1 \cdot 1 \end{array} \right\}$	73	2.5	1.0	
V2 12SK7	73	4.3	- 73	1.2	2.5	
V3 12Q7GT	22	0.1			0.5	
V4 35 L6GT	103	13.0	73	0.6	6.3	
V5 35Z4GT	110†		-		110	



Under-chassis view. A diagram of the S1-S12 switch diagram is given overleaf.