"TRADER" SERVICE SHEET

895

A PLATE aerial is provided in the Mullard MAS221 receiver for use in temporary locations, a jack-type switch associated with the aerial socket converting it to a screen when an external aerial is connected.

The receiver is a 4-valve (plus rectifier) 3-band superhet designed to operate from A.C. mains of 100-260 V, 50-100 c/s. The S.W. range is 16.3-51 m, the aerial circuit operating aperiodically on this band. The other ranges are 192-560 m and 900-2,000 m.

Release date and original price: July 1948; £20 7s. 11d. plus purchase tax.

#### CIRCUIT DESCRIPTION

External aerial input is coupled, via the I.F. rejector L1, C1 and capacitative potential divider C2, L2, C3, R2, to single-tuned circuits L3, C34 (M.W.) and L4, C34 (L.W.). A resistor R1 shunts the input circuit to prevent modulation hum. For S.W. operation the M.W. aerial coil L3 is shunted by a S.W. R.F. choke L2,

# MULLARD MAS221

# 3-Band A.C. Superhet

via **S2**, and the tuning capacitor **C34** is disconnected due to the opening of **S5**, so that the input circuit is aperiodic.

An internal plate aerial, operative on all bands, is provided and coupled to the aerial circuits via the low potential ends of the trimmers C32, C33, but when an external aerial is employed S14, a jacktype switch associated with the A socket, closes to connect these trimmers across their tuned circuits and earth the plate aerial, which then acts as a screen.

First valve (V1, Mullard metallized

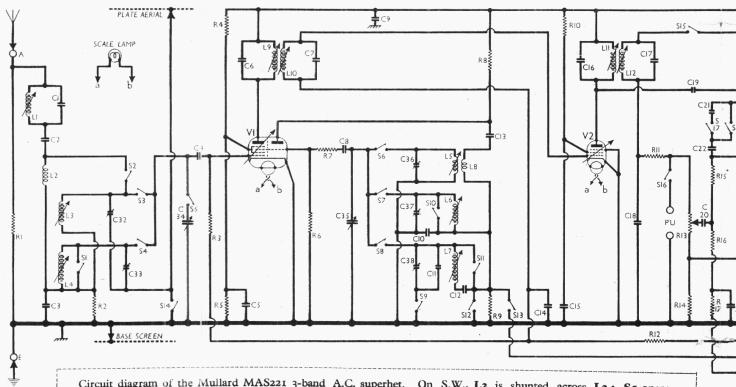
First valve (V1, Mullard metallized ECH35) is a triode-hexode operating as frequency changer with internal coupling. Triode oscillator grid coils L5 (S.W.), L6 (M.W.), L7 (L.W.) are tuned by C35, with parallel trimming by C36 (S.W.), C37 (M.W.) and C11, C38 (L.W.). Tracking by C10 (M.W.) and C10, C12 in series (L.W.); reaction coupling from anode, via C13, is inductive, due to L8, on S.W., and capacitative, due to the common impedance of C10 in grid and anode circuits, on M.W. and L.W., S12 and S13 then being open.

Second valve (V2, Mullard metallized

EF39) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned-transformer couplings C6, L9, L10, C7 and C16, L11, L12, C17. Intermediate frequency 470 kc/s.

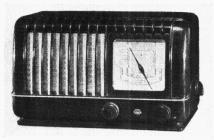
Diode second detector is part of double diode triode valve (V3, Mullard metallized EBC33). Audio frequency component in rectified output is developed across manual volume control R13, which is also the diode load resistor, and passed via C20 and R15 to grid of triode section, which operates as A.F. amplifier. I.F. filtering by C18, R11 in diode circuit, and provision for the connection of a gramophone pick-up across R13 via S16, with which is associated the radio muting switch S15. Three-position negative feed-back tone control is provided by C21, S17, S18, C22 which enable V3 anode output voltages to be fed back to its control grid circuit.

Second diode of V3, fed from V2 anode via C19, provides D.C. potential which is developed across load resistor R19 and fed back through a decoupling circuit R12, C14 as G.B. to F.C. and I.F. valves, giving automatic gain control.



Circuit diagram of the Mullard MAS221 3-band A.C. superhet. On S.W., L2 is shunted across L3; S5 opens, and the aerial circuit is aperiodic. The insertion of the external aerial plug automatically closes S14, connecting the trimmers C32, C33 and the plate aerial to chassis.

3-position tone control is provided by feedback coupling between the control grids of V4 and V3. Another feedback circuit R26, R27, R28, C29 provides tone correction, while hum neutralising voltages are applied by R25, C27. The feedback coupling is modified on S.W. by the closing of S12, S13.



The Mullard MAS221 A.C. superhet.

Resistance-capacitance coupling by R18, R22, C24, R23, via grid stopper R24, be-H22, C24, H23, via grid stopper H22, between V3 triode and pentode output valve (V4, Mullard EL33). Fixed tone correction by C26 in anode circuit.

A.F. voltages developed across T1 secondary winding are applied to a potential divider network R27, R28, C29, Lapped off and fed heat through R26, C28, R44.

tial divider network R27, R28, C29, tapped off, and fed back through R26, C28, R14, to V3 grid circuit to improve the A.F. response on M.W. and L.W., and a small proportion of the ripple voltage present on the H.T. + line is also fed to this point via R25, C27 to neutralize residual hum. The response of the circuit is modified on the S.W. band, when S12, S13 close and short-circuit C29.

H.T. current is supplied by full wave rectifying valve (V5, Mullard AZ31). Smoothing by resistor R29 and electrolytic capacitors C30, C31, but the H.T.

supply for V4 anode is obtained direct from the rectifier filament. Fixed G.B. for V1-V4 and A.G.C. delay voltage is provided by the drop across R20, R21 in the H.T. negative lead to chassis. H.T. circuit R.F. filtering by C9.

# **COMPONENTS AND VALUES**

	RESISTORS	Values (ohms)	Loca- tions
R1	Aerial shunt	5,600	M 5
R2	Aerial coupling	10,000	L4
R3	V1 hex. C.G	1,000,000	B2
R4	V1 S.G. H.T. feed	22,000	L6
$R_5$	f potential divider	27,000	L6
R6	V1 osc. C.G	47,000	M6
R7	Osc. stabilizer	180	M5
R8	Osc. H.T. feed	22,000	L6
R9	Osc. coupling	5,600	L6
R10	V2 S.G. feed	100,000	L5
R11	I.F. stopper	47,000	J6
R12	A.G.C. decoupling	680,000	J5
R13	Volume control	500,000	K4
R14	) FB. couplings	1,000	K4
R15	resistors	100,000	$H_5$
R16	V3 C.G. resistor	1,000,000	H4
R17	V3 C.G. decoup,	470,000	J5
R18	V3 triode load	220,000	J5
R19	A.G C. diode load	680,000	J5
R20	) V1-V4 G.B. ; A.G. C.	47	J5
R21	delay resistors	82	J5
R22	A.F. stabilizer	47	J5
R23	V4 C.G. resistor }	470,000	$H_5$
R24	V4 C.G. stopper	100,000	H5
R25	) FB. series resist-{	150,000	K4
R26	Cors	2,700	H4
R27	FB. potential	2,700 4,700	H4
R28	divider resistors	220	J4
R29	H.T. smoothing	1,500	K5
2000	zarzi oznottinig	1,000	11.0

	CAPACITORS	$_{(\mu F)}^{ m Values}$	Loca- tions
C1.	I.F. rejector tune	0.00056	M5
C2	Aerial coupling (	0.0015	M4
Č3	capacitors	0.0033	L4
C4-	V1 hex C.G.	0.0001	B2
Cb	V1. SG. decoup	0.047	M6
Č6	1st I.F. trans.	0.00015	B3
Ci	tuning	0.00015	B3
Č8	tuning \\ V1 osc. C.G	0.00015	L5
C9	H.T. R.F. by-pass	0.00019	H4
CLO	Occ. M.W. treeless	0.00036	L5
CLI	Osc. M.W. tracker Osc. L.W. trimmer	0.00001	L <sub>3</sub>
CL2	Osc. L.W. tracker		
		0.00015	M5
C1.3	Osc. anode coup.	0.0001	M5
C1.4 C1.5	A.G.C. decoupling	0.1	J5
	V2 S.G. decoupling	0.047	K5
C16	\2nd I.F. trans.	0.00015	$D_3$
C17	\_ tuning \\	0.00015	$\overline{D3}$
C18	I.F. by-pass	0.0001	K6
C1.9	A.G.C. coupling	0.000047	J6
C20	A.F. coupling	0.01	J4
C21 ·	FB. coupling	0.000033	H4
C22	capacitors (	0.00015	H5
C23	V3 G.B. decoupling	0.1	$H_5$
C24	A.F. coupling	0.0047	J5
C25*	G.B. by-pass	25.0	$_{\rm H6}$
C26	Tone corrector	0.001	D1
C27	FB. coupling	0.1	J4
C28	FB. coupling	0.12	J4
C29	capacitors	0.047	J4
C30*	H.T. smoothing	32.0	C2
C31*	capacitors }	32.0	C2
C321	Aerial M.W. trim	0.000012	M4
C33‡	Aerial L.W. trim	0.000032	M4
C34†	Aerial tuning		B1
C35†	Oscillator tuning		$^{\mathrm{B2}}$
C361	Osc. S.W. trim	0.00003	L5
C371	Osc. M.W. trim	0.00003	L5
C38‡	Osc. L.W. trim	0.00003	L4

\* Electrolytic. † Variable. ‡ Pre-set.

RIB R/22		EXT. LI3		VI V	TC MET
SIB V3	R23	C27		V3	V5 V5
R C R19		C28 R28	. K29	C3i	
Raim	<b>‡</b> -c25			VS T	O AC MAINS

ОТЕ	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1 L2 L3 L4 L5 L6 L7 L8	I.F. rejector coil S.W. R.F. choke  Aerial tuning coils  Oscillator tuning coils Osc. S.W. react	4·0 Very low 7·5 24·0 Very low 8·0 12·0 0·1	M5 L4 A1 A1 L5 A2 A2 L5
L9 L10 L11 L12 L13 T1	} lst I.F. trans. { Pri. Sec. } Speech coil Output { Pri. Sec Trans. } Sec { Pri. trans. } Sec { Pri. total Heat. sec. Rec. heat. sec H.T. sec H.T. sec	8.0 8.0 8.0 2.75 380.0 0.5 51.0 0.1	B3 B3 D3 D3 
\$13 \$14 \$15, \$16 \$17, \$18 \$19- \$20	W/band switches Plate aerial switch Radio/Gram Switches Tone control switches Mains sw., g'd R13	1,100·0 ——————————————————————————————————	F1 L5 M6 J6 H4 K4

### **VALVE ANALYSIS**

Valve voltages and currents given in the table below are those measured in our receiver when it was operating on mains

Valve	Anode	Anode	Screen	Screen
	Voltage	Current	Voltage	Current
	(V)	(mA)	(V)	(mA)
V1 ECH35 V2 EF39 V3 EBC33 V4 EL33 V5 AZ31	$\left\{\begin{array}{c} 237\\ \text{Oscil}\\ 102\\ 237\\ 75\\ 257\\ 292 \dagger \end{array}\right.$	2·5 lator 5·4 4·3 0·6 35·0	94 84 237	2·0 1·4 3·6

† Each anode, A.C.

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of 224 V, using the 220 V tapping on the mains transformer.

The receiver was tuned to the lowest wavelength on the M.W. band, and the volume control was at maximum, but there was no signal input. Voltages were measured on the 400 V scale of a model 7 Avometer, chassis being the negative connection.

#### DISMANTLING THE SET

Almost unimpeded access to the top and underside of the chassis may be gained upon removal of the back cover (two round-head wood screws and two cheese-head screws, with washers) and bottom cover (four cheese-head screws, with washers).

Removing Chassis.—Remove back cover as previously described;

remove the two front control knobs (recessed grub screws), and from the rear of the cabinet remove the two side control knobs (one cheese-head screw each, accessible through cut-away sections of the rear chassis member);

from the underside of the cabinet remove the bottom fixing screw (with washer) to which a flexible earthing lead is attached;

if the two large chassis fixing screws (with lock-washers), located to the left of the gang and adjacent to the mains transformer, are now removed, the chassis may be slid from the cabinet to the extent of the speaker leads, which is sufficient for most purposes.

To free the chassis entirely unsolder the speaker leads at tags on the output transformer.

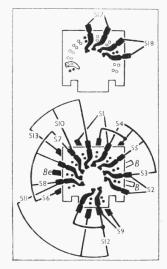
When replacing, the waveband and tone control switches should be turned fully anti-clockwise before inserting the chassis in the cabinet.

Do not omit to replace the yellow plate aerial connecting lead beneath the head of the left-hand chassis fixing screw, and the black base screen lead beneath the appropriate bottom cover fixing screw.

Removing Speaker.—Remove the three nuts (with washers) securing the speaker to the sub-baffle, and lift it out.

#### Switch Tables and Diagram

Switch	s.w.	M.W.	L.W.
S1 S2 S3	CCC	С	
S2	С		
S3	C	С	
S4	Management		С
\$4 \$5 \$6 \$7 \$8 \$9		С	С
86	С		
S7		С	
<b>S</b> 8			С
89			С
S10	C		CCC
S11		С	
S12	С		
S13	С		



Diagrams of the tone control (top) and waveband (bottom) switch units, viewed in the direction of the arrows in our under-chassis view. The table above the diagrams gives the switch positions for the three settings of the lower (waveband) unit.

When replacing, the connecting panel should point to the left-hand side of the cabinet, and the leads should be resoldered to the rear tags (e, f) on the output transformer.

#### **GENERAL NOTES**

S1-S13 are the waveband switches, ganged in a single rotary unit beneath the chassis. The unit is indicated in our under-chassis view, and shown in detail in the diagram in col. 2, where it is viewed as seen from the control knob with the chassis inverted, as indicated by the arrow in our photograph.

The table (col. 2) gives the switch positions for the three control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and **C**, closed.

\$14 is the plate aerial shorting switch. It is operated by insertion or removal of the external aerial plug, and connects the plate aerial to chassis when an external aerial is in use.

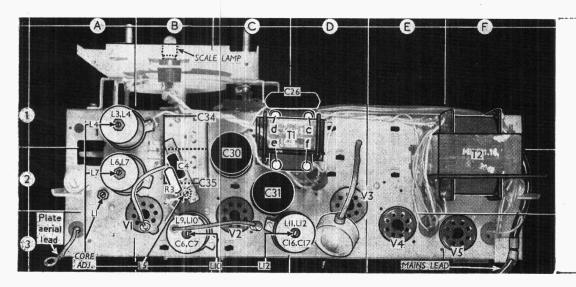
\$15, \$16 are the radio/gram changeover switches, in a two-position unit mounted on the rear chassis member. The tags are clearly identified in our underchassis illustration. On radio (control lever down) \$15 is closed, and \$16 open. On gram (control lever up) the position is reversed.

\$17, \$18 are the tone control switches, in a three-position rotary unit beneath the chassis. Its position is indicated in our under-chassis view, where an arrow shows the direction in which it is viewed in the diagram in col. 2. In the normal position (knob fully clockwise) both switches are open; in the middle position (reduced high-note response) \$17 closes; in the anti-clockwise position ("deep" tone) \$17 is open, and \$18 closed.

S19, S20 are the QMB mains switches in a circular unit mounted concentrically round the volume control spindle, and operated by a lever mounted on the spindle.

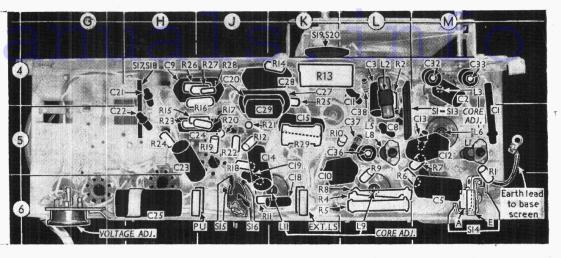
spindle.

Coils.—The I.F. rejector coil L1 and the aperiodic S.W. aerial coil L2 are in two unscreened units beneath the chassis. The M.W. and L.W. aerial tuning coils L6, L7 are in two screened units on the chassis deck. In each case the L.W. coil core is adjusted from the upper end of the unit, and the M.W. core from beneath the chassis. Diagrams in col. 4 show the base connections of these two units. The S.W.



Plan view of the chassis, showing the aerial, oscillator and I.F. secondary core adjustments. The connections of the output transformer Trare lettered c, d, e, f to a gree with those in the circuit diagram.

Under-chassis view. The tags of the radio/gram switch unit S15, S16, are identified here. Diagrams of the waveband switch unit SI-SI3 and the tone control unit S17, S18 appear in col. 2. S14 is associated with the aerial socket.

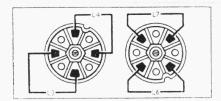


oscillator coils L5, L8 form a third unscreened unit beneath the chassis.

Scale Lamp.—This is mounted in a plastic bayonet-fitting holder on the scale assembly. The lamp is a Philips type 8045/D00, rated at 6 V, 0.32 A. It has a tubular bulb and an M.E.S. base.

External Speaker.—Two sockets are provided at the rear of the chassis for the connection of a low-impedance (5-7  $\Omega$ ) external speaker.

Chassis Divergencies.-In a few early versions, L2 may not be fitted, and the



Diagrams showing the base connections of the two M.W. and L.W. coil

waveband switch unit may be arranged to short-circuit R2, C3 on the S.W. band. In some chassis, too, the positions of C32 and C37 may be transposed.

## CIRCUIT ALIGNMENT

These operations may be carried out with the chassis in the cabinet, after removal of the bottom cover.

I.F. Stages.—Switch set to M.W., tune to 375 m on scale, turn volume control to maximum, and connect signal generator, via an 0.047  $\mu$ F capacitor in the "live" lead, to control grid (top cap) of V1 and chassis. Shunt L11 (location reference K6) with an 0.0001 µF capacitor, feed in a 470 kc/s (638.3 m) signal, and adjust the core of L12 (D3) for maximum output. Transfer shunting capacitor to L10 (L6) and adjust the cores of L11 (K6) and L9 (L6) for maximum output. Finally, transfer shunting capacitor to L9 (L6) and adjust the core of L10 (B3) for maximum output, and then disconnect "live" signal generator lead and shunting capacitor.

I.F. Rejector.—With set still switched to M.W., tune to 560 m on scale, transfer "live" signal generator lead to A socket, via a suitable dummy aerial, feed in a strong 470 kc/s signal, and adjust the core of L1 (A2) for minimum output.

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R.F. and Oscillator Stages .- With the gang at minimum capacitance the pointer should be horizontal. It may be adjusted in position by rotating it on its spindle. Note that the local oscillator frequency in this receiver is higher than the signal frequency on all bands.

When adjusting a wire-wound trimmer, wire should be unwound until output, having reached a maximum, begins to decrease. The winding should then be sealed with wax and any surplus cut off. Do not attempt to increase capacitance by adding wire, as the turns would not remain in place, but replace capacitor with a new one.

M.W.—With set still switched to M.W.

tune to  $500\,\mathrm{m}$  on scale, feed in a  $500\,\mathrm{m}$ (600 kc/s) signal, and adjust the core of L6 (M5) for maximum output. Tune to 200 m (line on scale), feed in a 200 m (1,500 kc/s) signal, and adjust **C37** (L5) for maximum output. Retune to 500 m on scale, feed in a 500 m signal, and adjust core of L3 (M4) for maximum output. Retune to the 200 m calibration line, feed in a 200 m signal, and adjust **C32** (M4) for maximum output. Repeat these operations until no improvement results.

L.W.—Switch set to L.W., tune to 1,720 m (line on scale), feed in a 1,720 m (174.4 kc/s) signal, and adjust the core of L7 (A2) for maximum output. Tune to 790 m (line on scale), feed in a 790 m (379.8 kc/s) signal, and adjust **C38** (L4) for maximum output. Retune to 1,720 m on scale, feed in a 1,720 m signal, and adjust the core of **L4** (A1) for maximum output. Retune to 790 m on scale, feed in a 790 m signal, and adjust C33 (M4) for maximum output. Repeat these operations until no improvement results.

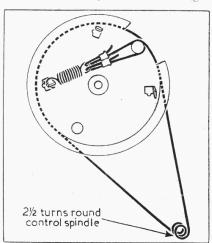
S.W.—Switch set to S.W., tune to 50 m on scale, feed in a 50 m (6 Mc/s) signal, and adjust the core of L5 (B2) for maximum output. Turn gang to minimum capacitance, feed in a 16.22 m (18.5 Mc/s) signal, and adjust C36 (L5) for maximum output.

#### DRIVE CORD REPLACEMENT

For replacement of the tuning drive cord, the scale assembly must be removed. This entails simply removing the scale lamp holder, withdrawing the scale pointer (push-on fit) and removing the two fixing screws (with flat washers and lock-washers) holding the assembly to the chassis.

Make up the cord, with a loop at each end, so that the overall length is 446 mm (ours measured 173 inches). Turn the gang to maximum, when the drum should be in the position shown in our sketch below, hook one end of the cord to one end of the tension spring, which in turn is hooked to its anchor, and run the cord over the guide pin and down to the control spindle.

Make  $2\frac{1}{2}$  turns clockwise round the spindle and complete the run as shown in the sketch. Keep the cord well to the front of the waisted portion of the control spindle, as if it gets close to the chassis it tends to run off the flat rim of the drum. When refitting the pointer, hold it near the middle, where it is strong.



Sketch of the tuning drive cord, drawn as seen from the front of the chassis, after removing the scale assembly, with the gang at maximum.