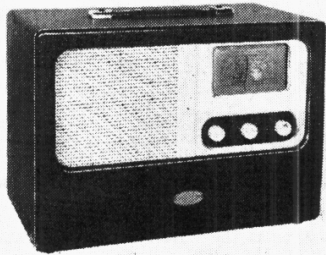


"TRADER" SERVICE SHEET
883

AMPLION ADP2

Covering also Model ADP1



The Amplion ADP2 portable.

AN all-dry battery portable with two wavebands, the Amplion ADP2 is a superhet employing four valves and using the Ever Ready No. 3 combined H.T. and L.T. battery.

The ADP1 was an earlier model using a chassis almost identical with that in the ADP2, but housed in a different case. The differences are explained under "Divergencies" overleaf.

Release dates and original prices: ADP1 February, 1946, £13 13s (with battery); increased September, 1946, to £13 15s. ADP2, December, 1946, £13 15s (less battery), increased November, 1947, to £14 14s; reduced February, 1948, to £12 14s (with battery); then June, 1948, to £12 12s (less battery); and October, 1948, to £11 2s 6d (with battery). Purchase tax extra.

CIRCUIT DESCRIPTION

Tuned frame aerial input by **L1**, **C16** (M.W.), with the addition of loading coil **L2** on L.W., precedes a heptode valve (**V1**, **1A7GT**) operating as frequency changer with electron coupling.

Triode oscillator grid coils **L3** (M.W.) and **L4** (L.W.) are tuned by **C17**, with

parallel trimming by **C18** (M.W.) and **C4**, **C19** (L.W.), and series tracking by **C5** (M.W.) and **C6** (L.W.). Reaction coupling from anode via **C7**, by **L5** (M.W.) and **L6** (L.W.), with additional coupling due to the inclusion of the trackers in the common grid and anode circuit.

Second valve (**V2**, **1N5GT**) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings **C20**, **L7**, **L8**, **C21** and **C22**, **L9**, **L10**, **C23**.

Intermediate frequency 465 kc/s.

Diode second detector is part of single diode triode valve (**V3**, **1H5GT**). Audio frequency component in rectified output is developed across manual volume control **R6**, which is also the diode load resistor, and passed via A.F. coupling capacitor **C10** and C.G. resistor **R7** to grid of triode section, which operates as A.F. amplifier. I.F. filtering by **C8**, **R5**, **C9** in diode circuit and **C11** in **V3** triode anode circuit.

D.C. potential developed across **R5**, **R6** in series is tapped off and fed back, (Continued col. 1 overleaf)

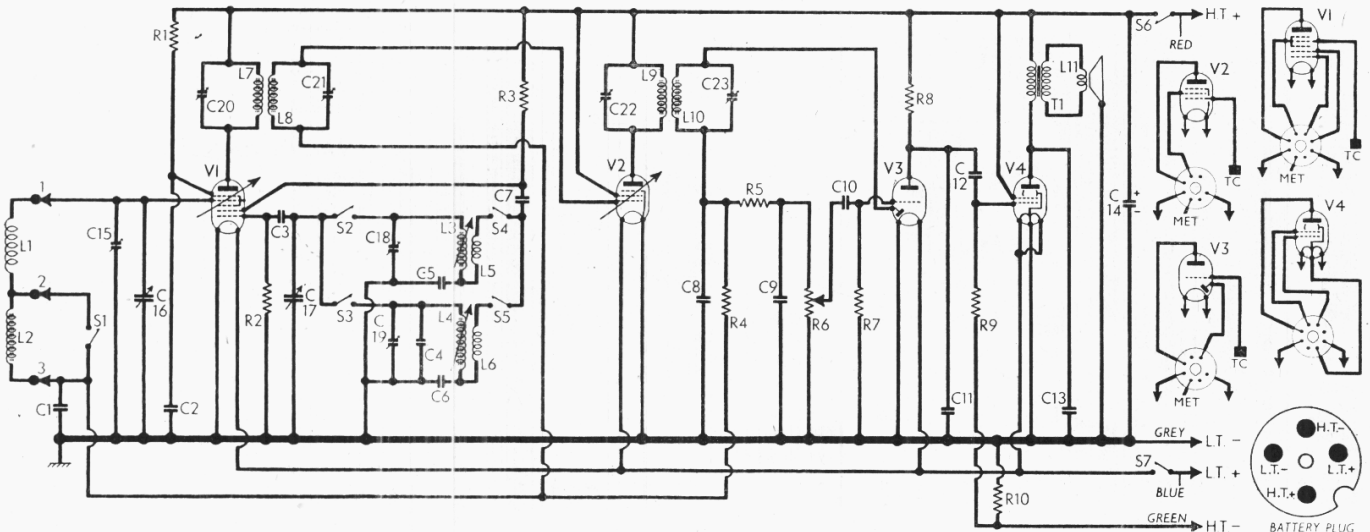
COMPONENTS AND VALUES

RESISTORS		Values (ohms)	Locations
R1	V1 S.G. feed ...	47,000	J5
R2	V1 osc. C.G. ...	220,000	K6
R3	Osc. anode load ...	22,000	J5
R4	A.G.C. decoupling ...	2,500,000	H5
R5	I.F. stopper ...	47,000	F4
R6	Volume control ...	500,000	H3
R7	V3 triode C.G. ...	2,500,000	H5
R8	V3 triode load ...	1,000,000	G5
R9	V4 C.G. resistor ...	2,500,000	F5
R10	V4 G.B. resistor ...	560	E6

CAPACITORS		Values (μF)	Locations
C1	A.G.C. decoupling ...	0.1	J6
C2	V1 S.G. decoup. ...	0.1	J5
C3	V1 osc. C.G. ...	0.0001	K4
C4	Osc. L.W. trimmer ...	0.0001	J4
C5	Osc. M.W. tracker ...	0.00035	J4
C6	Osc. L.W. tracker ...	0.00015	J4
C7	Osc. anode coup. ...	0.002	K5
C8	I.F. by-pass capacitors ...	0.0001	G4
C9		0.0001	F6
C10	A.F. coupling ...	0.01	G4
C11	I.F. by-pass ...	0.0001	G4
C12	A.F. coupling ...	0.02	E5
C13	Tone corrector ...	0.001	E6
C14*	H.T. reservoir ...	8.0	F4
C15†	Aerial M.W. trim ...	—	A1
C16†	Aerial tuning ...	—	B1
C17†	Oscillator tuning ...	—	B1
C18†	Osc. M.W. trim. ...	—	K4
C19†	Osc. L.W. trim. ...	—	K5
C20†	1st I.F. transformer ...	—	B2
C21†		tuning ...	—
C22†	2nd I.F. transformer ...	—	C2
C23†		tuning ...	—

* Electrolytic. † Variable. ‡ Pre-set.

OTHER COMPONENTS		Approx. Values (ohms)	Locations
L1	Frame aerial ...	2.1	A2
L2	L.W. loading coil ...	12.5	B2
L3	Oscillator tuning coils ...	2.6	B1, B2
L4		6.3	
L5	Oscillator reaction coils ...	0.5	K5
L6		0.6	
L7	1st I.F. trans. ...	5.0	B2
L8		5.0	
L9	2nd I.F. trans. ...	9.5	C2
L10		9.5	
L11	Speech coil ...	2.75	—
T1	Speaker trans. ...	470.0	—
S1-S5	W/band switches ...	—	K3
S6	H.T. circuit switch ...	—	K3
S7	L.T. circuit switch ...	—	K3



Circuit diagram of the Amplion ADP2. Small differences that occur in some of these models, and the differences in the ADP1 are explained under "General Notes" overleaf.

Circuit Description—continued

through a decoupling circuit **R4**, **C1**, as G.B. to F.C. and I.F. valves, giving automatic gain control.

Resistance-capacitance coupling by **R8**, **C12**, **R9** between **V3** triode and beam tetrode output valve (**V4**, **3Q5GT**), whose twin filament sections are wired in parallel. Fixed tone correction in anode circuit by **C13**. G.B. potential for **V4** is obtained from the drop across **R10** in the H.T. negative lead to chassis.

CIRCUIT ALIGNMENT

It is necessary to remove the chassis from the carrying case before commencing these operations.

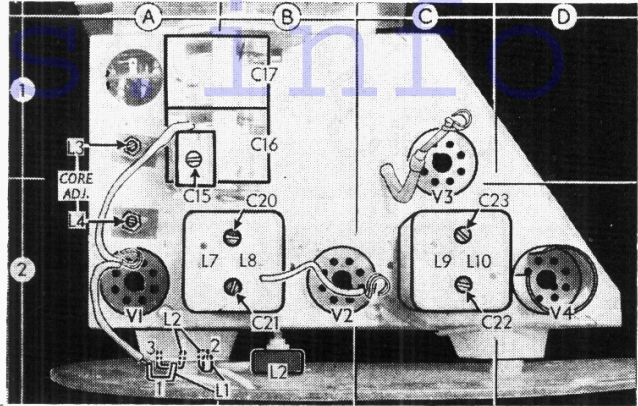
I.F. Stages.—Switch set to M.W., tune to 200 m on scale, turn volume control to maximum, and connect signal generator (via an $0.1\mu\text{F}$ capacitor in the "live" lead) to control grid (top cap) of **V1** and chassis. Feed in a 465 kc/s (645.16 m) signal, and adjust **C20**, **C21**, **C22** and **C23** (location references B2, C2) for maximum output, progressively attenuating the signal generator output as the circuits are aligned, to avoid A.G.C. action.

R.F. and Oscillator Stages.—With the gang at maximum capacitance the pointer should be horizontal and coincident with the high-wavelength end of the M.W. scale. It may be adjusted in position by rotating it on the gang capacitor spindle. Loosely couple the signal generator by means of a 6 in piece of wire laid close to the frame aerial winding.

M.W.—Switch set to M.W., tune to 500 m on scale, feed in a 500 m (600 kc/s) signal, and adjust the core of **L3** (A1) for maximum output. Tune to 200 m on scale, feed in a 200 m (1,500 kc/s) signal, and adjust **C18** (K4) and then **C15** (A1) for maximum output. Repeat these operations until no improvement results.

L.W.—Switch set to L.W., tune to 2,000 m on scale, feed in a 2,000 m (150 kc/s) signal, and adjust the core of **L4** (A2) for maximum output. Tune to 1,000 m on scale, feed in a 1,000 m (300 kc/s) signal, and adjust **C19** (K5) for maximum output. Repeat these operations until no improvement results.

Plan view of the chassis. The L.W. coil **L2** is mounted on the M.W. frame aerial panel. **V4** is fitted with a close-fitting shield.



GENERAL NOTES

Switches.—**S1-S7** are the waveband and battery switches, ganged in a single rotary unit beneath the chassis. This is indicated in our under-chassis view, and shown in detail in the diagram below, where it is drawn as seen from the rear of an inverted chassis. The table below gives the switch positions for the three control settings, starting from the fully anticlockwise (off) position of the control knob. A dash indicates open, and **C**, closed.

Batteries.—The battery supplied with this receiver is an Ever Ready All-dry No. 3 com-

bined 90 V H.T. and 1.5 V L.T. unit. An alternative type is the "Batriumax" 103 layer-built battery of the same voltage ratings.

Drive Cord Replacement.—This is extremely simple and requires no description. It consists of a single loop of cord, anchored in the usual manner, passing half-way round the drive drum and half-way round the control spindle pulley.

The scale assembly must first be removed, however, which involves removing the pointer (pull-off) and the three control knobs with their backing plate. As the knob fixing screws are small, a watchmaker's screwdriver will be needed.

Divergencies.—Differences that occur in the ADP2 are that **C4**, which in our sample was 50 pF ($0.00005\mu\text{F}$) may be 100 pF, while **C15** may be omitted altogether; Osram valves may be used instead of those we quote, and their type numbers would be X14 (**V1**), Z14 (**V2**), HD14 (**V3**) and N14 (**V4**). In such versions **R10** becomes 820 Ω instead of 560 Ω .

In the earlier model ADP1, the frame aerial consisted of a M.W. winding and a L.W. winding, instead of a M.W. winding (our **L1**) and a loading coil (our **L2**), and the Osram range of valves given for the ADP2 was used, **R10** again being 820 Ω .

DISMANTLING THE SET

Removing Chassis.—Remove the two round-head wood screws securing the shelf above the battery compartment to the carrying case, and slide out the chassis, frame aerial and shelf to the extent of the speaker leads, which is sufficient for most purposes.

Remove the plywood shelf, which is secured to the chassis by three hexagon-head self-threading screws (with metal washers).

When replacing, if the speaker leads have been disconnected they should be re-soldered as follows: grey to a rivet head securing the speaker transformer connecting panel, and red and blue to the two tags on this panel.

Removing Speaker.—Remove chassis assembly as previously described, loosen the nuts securing the three speaker retaining clamps, swivel the clamps aside, and lift out the speaker.

When replacing, the speaker transformer should be at the bottom.

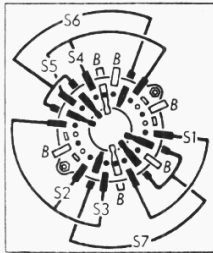
VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receiver when it was operating from a set of new batteries. The receiver was tuned to the lowest wavelength on the M.W. band, and the volume control was at maximum, but there was no signal input.

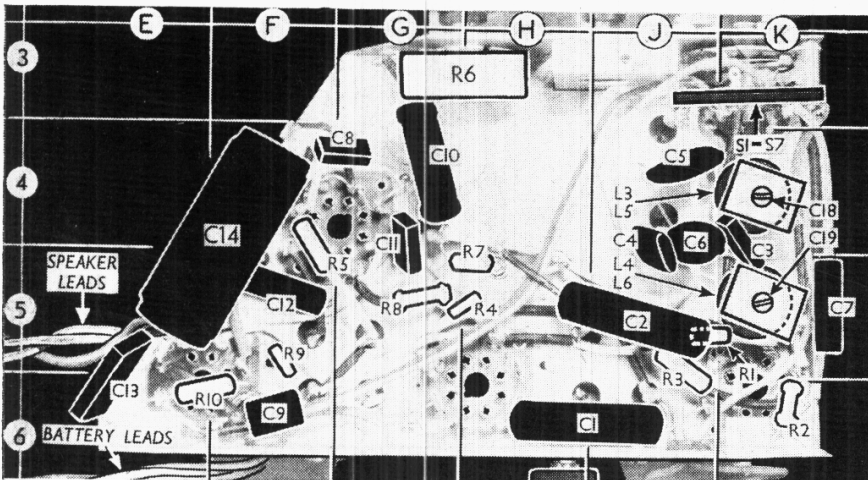
Voltages were measured on the 400 V scale of a model 7 Avometer, chassis being the negative connection.

Valve	Anode Voltage (V)	Anode Current (mA)	Screen Voltage (V)	Screen Current (mA)
V1 1A7GT	97	1.0	51	0.87
	70	0.9		
V2 1N5GT	97	0.68	97	0.17
V3 1H5GT	12	0.03	—	—
V4 3Q5GT	93	6.8	97	0.75

Diagram of the wavebandswitch unit, as seen from the rear of an inverted chassis. Below is the associated table.



Switch	Off	M.W.	L.W.
S1	—	C	—
S2	—	C	—
S3	—	—	C
S4	—	C	—
S5	—	—	C
S6	—	C	C
S7	—	C	C



Under-chassis view. A diagram of the **S1-S7** switch unit appears in col. 2 above.