# "TRADER" SERVICE SHEET 11 1 SERVICE SHEET 11 SERVI

A PLATE aerial for S.W. operation and a frame aerial for the M.W. and L.W. bands are fitted in the Invicta 31, so that the receiver may be operated on the four wavebands provided if desired in the absence of an external aerial. A normal aerial may be fitted, however, in permanent installations.

The receiver is a 3-valve (plus rectifier) superhet for operation from A.C. mains of 200-250 V, 40-100 c/s. The four waveband ranges are: 14-40 m (S.W.1), 60-200 m (S.W.2), 200-550 m (M.W.) and 900-2,000 m (L.W.). Provision is made for the connection of a gramophone pickup and an external speaker.

It should be carefully noted that the rectifier may be an AZ31 or an EZ35. This is explained overleaf.

Release date and original price: May 1948; £18 18s. plus purchase tax.

## Four-Band A.C. Superhet

#### CIRCUIT DESCRIPTION

On the two S.W. bands, input from external or plate aerial is inductively coupled by L1 to single-tuned circuit L3, C30 on S.W.1, and directly coupled, via a tapping, to single-tuned circuit L4, C30.

On M.W. and L.W., frame aerial input

On M.W. and L.W., frame aerial input is provided by L7, in conjunction with loading coils L5 (M.W.) and L6 (L.W.), tuned by C30. Provision is made for the connection of an external aerial, which is operative on all bands, insertion of the aerial plug automatically opening S4 to remove the short-circuit across the aerial coupling coil L2.

First valve (V1, Mullard metallized ECH35) is a triode-hexode operating as frequency changer with internal coupling. Triode oscillator grid coils L8 (S.W.1), L9 (S.W.2), L10 (M.W.) and L11 (L.W.) are tuned by C31, with parallel trimming by C32 (S.W.1), C33 (S.W.2), C34 (M.W.) and C14, C35 (L.W.); and series tracking

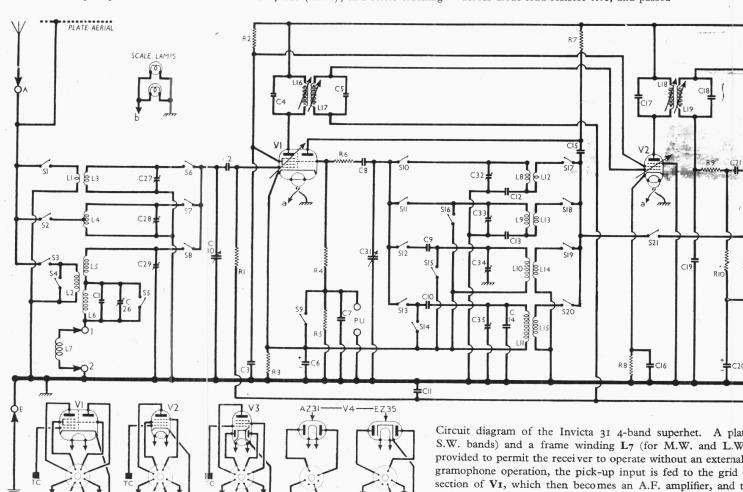
by C12 (S.W.1), C13 (S.W.2), C9 (M.W.) and C10 (L.W.). Reaction coupling from anode, via C15, by coils L12 (S.W.1), L13 (S.W.2), L14 (M.W.) and L15 (L.W.), additional coupling on the two S.W. bands being obtained by the inclusion of the tracking capacitors, which form a common impedance in the grid and anode circuits.

Second valve (V2, Mullard metallized EF39) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C4, L16, L17, C5 and C17, L18, L19, C18, in which the tuning capacitors are fixed and alignment adjustments are made by varying the positions of the iron-dust cores.

#### Intermediate frequency 465 kc/s.

Diode second detector is part of double diode pentode output valve (V3, Mullard metallized EBL31). Audio frequency component in rectified output is developed across diode load resistor R10, and passed

passed via S21 to V3 pentode. Where V4 is an EZ35, R21



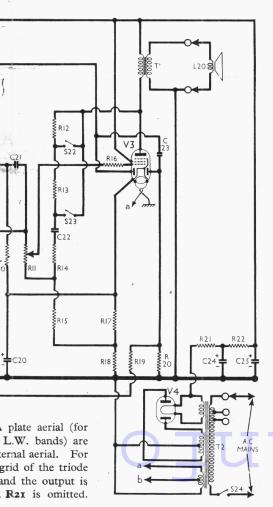
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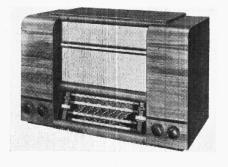
via A.F. coupling capacitor C21, manual control R11, and C.G. stopper R16, to control grid of pentode section. I.F. filtering by C19, R9 in diode circuit, and R16 in V3 C.G. circuit.

Second diode of V3, fed from L19 via C23, provides D.C. potential which is developed across load resistor R20 and fed back, through a decoupling circuit R19, C11, as G.B. to F.C. and I.F. valves, giving automatic gain control. Delay voltage, together with G.B. for pentode section, is obtained from the drop across R17, R18 in V3 cathode lead to chassis.

Three-position tone control is provided via the potential divider network R12, R13, C22, R14, R15 and S22, S23, which is connected across the output of V3 pentode section. The fraction of the output which is developed across R15 is applied to the control grid circuit of the valve, via R11, giving negative feed-back, and the frequency response is modified from the "Brilliant" condition (both switches open) to "Normal" (S22 closed), or "Mellow" (S23 closed).

For "Gram" operation, when **S9** opens, **V1** triode section is converted to an A.F. amplifier by connection of the pick-up, shunted by **R5**, **C7**, in its grid circuit. The amplified A.F. voltages developed





across the triode anode load resistor R7 are fed, via C15 and S21, to V3 C.G. circuit.

H.T. current is supplied by full-wave rectifying valve (V4, Mullard AZ31 or EZ35). Smoothing by resistor R22 and electrolytic capacitors C24, C25.

#### **COMPONENTS AND VALUES**

	RESISTORS	Values (ohms)	Loca- tions
R1	V1 hex. C.G	1,000,000	B2
R2	S.G.'s H.T. feed	47,000	L4
R3	V1 fixed G.B	220	$L_3$
R4	V1 triode C.G. re-	47,000	M4
R5	sistors \	200,000	M4
R6	Osc. stabilizer	56	M4
R7	Osc. H.T. feed	47,000	M4
R8	V2 fixed G.B	220	L5
R9	I.F. Stopper	47,000	$K_5$
R10	Sig. diode load	470,000	K5
R11	Volume control	1,000,000	G3
R12	) Negative feed-back (	100,000	H3
R13		33,000	$H_3$
R14	potential divider	15,000	G3
R15	resistors (	4,700	J4
R16	V3 C.G. stopper	100,000	D2
R17	V3 C.G. stopper $V3$ G.B., A.G.C. delay resistors	150	J4
R18	delay resistors \	330	J4
R19	A.G.C. decoupling	1,000,000	K5
R20	A.G.C. diode load	1,000,000	K5
R21	V4 surge limiter	100	J5
R22	H.T. smoothing	1,500	J4
		,	

	CAPACITORS	Values (μF)	Loca- tions	
C1	Aerial L.W. trim	0.000022	B2	
$\overline{C2}$	V1 hex. C.G	0.0003	A1	
$\overline{\text{C3}}$	S.G.'s decoupling	0.02	L5	
C4	1st I.F. transformer	0.00007	C2	
C5	} tuning (	0.00007	C2	
C6*	V1 cath. by-pass	50.0	L4	
C7	P.U. tone corrector	0.005	M4	
C8	V1 osc, C.G.	0.0001	03	
C9	Osc. M.W. tracker	0.00057	N3	
C10	Osc. L.W. tracker	0.00034	03	
C11	A.G.C. decoupling	0.1	L5	
C12	Osc. S.W.1 track	0.005	M3	
C13	Osc. S.W.2 track	0.002	N4	
C14	Osc. L.W. trimmer	0.00014	M4	
C15	Osc. anode coupling	0.02	M3	
C16	V2 cath. by-pass	0.1	$L_5$	
C17	2nd I.F. transfor-	0.00014	$\overline{D2}$	
C18	mer tuning (	0.00014	$\overline{\mathrm{D2}}$	
C19	I.F. by-pass	0.0001	K5	
C20*	V3 cath, by-pass	50.0	$\widetilde{\mathrm{H}}_{5}$	
C21	A.F. coupling	0.01	$\overline{K5}$	
C22	FB. coupling	0.01	$H_3$	
C23	A.G.C. coupling	0.000022	K5	
C24*	H.T. smoothing	32.0	E1	
C25*	capacitors	32.0	E1	
C261	Aerial L.W. trim.	0.00003	B2	
$C27\dot{t}$	Aerial S.W.1. trim.	0.00003	B2	
C28‡	Aerial S.W.2, trim.	0.00003	A2	
C291	Aerial M.W. trim.	0.00003	B2	
C30†	Aerial tuning	0.000537	B1	
C31†	Oscillator tuning	0.000537	B1	
C321	Osc. S.W.1. trim	0.00004	N4	
C33‡	Osc. S.W.2. trim	0.00004	N4	
C34‡	Osc. M.W. trim	0.00004	04	
C35‡	Osc. L.W. trim	0.00004	04	

\* Electrolytic. † Variable. ‡ Pre-set.

ОТІ	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1	Aerial coupling f	0.1	B2
L2	) coils (	68.0	B2
L3		Very low	B2
L4	Aerial tuning coils	0.3	A2
$L_5$	( started starting come	$2 \cdot 3$	B2
L6	)	12.7	$_{ m B2}$
L7	Frame aerial	0.6	A2
L8		Very low	N3
L9	Oscillator tuning	0.3	N4
L10	coils	$2 \cdot 2$	M3
L11	)	3.3	M4
L12	0	18.0	N3
L13	Oscillator reaction	23.0	N4
L14	coils	68.0	M3
L15	, , ,	83.0	M4
L16	$1st I.F. trans. \begin{cases} Pri. \\ Sec. \end{cases}$	8.0	C2
L17	2 70 1	8.0	C2
L18	} 2nd I.F. trans. { Pri. Sec.	6.0	D2
L19 L20		6.0	D2
L20	Speech coil	2.5	-
m a	Output f Pri	340.0	K4
T1	trans. \ Sec	0.1	K4
	Pri., total	26.0	F2
T2	Heat. sec.	Very low	F2
12	Mains Rect. heat.		***
	trans. sec.,	Very low	F2
	H.T. sec.,	***	
S1-S21	total	510.0	F2
91-921	W/band and Gram.		
600	switches		
S22	Tone control		TTO
S23	switches	-	H3
S24	Mains sw., g'd R11		G3

#### **VALVE ANALYSIS**

Valve voltages and currents given in the table below are those measured in our receiver when it was operating on mains of 223 V, using the 220-230 V tapping on the mains transformer. The receiver

,	Valve		Anode Current (mA)	Voltage	
V1	ЕСН35	$\left\{ \begin{matrix} 243 \\ \text{Oscil} \\ 86 \end{matrix} \right.$	$\left\{\begin{array}{c} 1.5 \\ \text{lator} \\ 3.4 \end{array}\right\}$	66	2.1
V2	EF39	243	5.5	66	1.6
	EBL31	233	35.0	243	4.3
V4	AZ31*	330†			1

\* May be EZ35. See "Alternative Rectifiers." † Each anode, A.C.

was tuned to the lowest wavelength on the M.W. band, and the volume control was at maximum, but there was no signal input.

Voltages were measured on the 400 V scale of a model 7 Avometer, chassis being the negative connection.

#### DISMANTLING THE SET

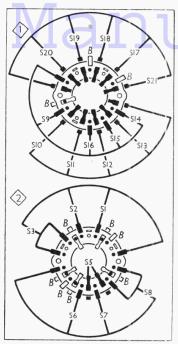
The cabinet is provided with a detachable bottom cover, upon removal of which (four round-head wood screws) access may be gained to the majority of the underchassis components, including several which are involved in circuit alignment. Removing Chassis.—Remove the four con-

trol knobs (recessed grub screws) from the front of the cabinet;

unplug the internal speaker leads from sockets on the rear edge of the chassis, and unsolder the white plastic-covered lead which is connected to the plate aerial inside the top of the cabinet;

remove the four 2BA cheese-head screws (with steel washers, rubber grommets and brass sleeves) securing the chassis

#### Switch Diagrams and Table



Diagrams of the waveband switch units, drawn as seen when viewed from the rear of an inverted chassis. B indicates blank tags. The associated table is on the right of these diagrams, in col. 2. S4 is shown in location M5 in our chassis illustration opposite.

to the base of the cabinet, and slide out the chassis.

When replacing, two of the specially shaped rubber grommets should be fitted to each chassis retaining screw, one going on each side of the cabinet base, with a brass sleeve between them; a flat steel washer fits beneath the head of each screw. This operation is simplified if the two front grommets are placed

Switch	Gram.	S.W.1	S.W.2	M.W.	L.W.
S1 S2 S3 S4 S5 S6 S7 S8 S9 S10 S11 S12 S13 S14 S15 S16 S17	Gram.	S.W.1	s.w.2	ccc   cc   c   c   c	L.W.
\$18 \$19 \$20 \$21	C	_	- -	C	C

† Opens upon insertion of external aerial plug

in position in their recesses before inserting the chassis. A felt washer should be fitted between each control knob and the front of the cabinet.

Removing Speaker.—Unplug the two leads from sockets on the rear edge of the chassis and remove the four 4BA nuts securing the speaker to the sub-baffle. When replacing, the connecting panel should be at the top.

#### **GENERAL NOTES**

Switches.—S1-S3 and S5-S21 are the waveband and radio/gram change-over switches, ganged in two rotary units beneath the chassis. These units are indicated in our under-chassis view, and shown in detail in the diagrams in col. 1, where they are drawn as seen when viewed from the rear of an inverted chassis.

The table above gives the switch positions for the five control settings, starting from the fully anti-clockwise (gram) position of the control spindle. A dash indicates open, and C, closed.

S4 is associated with the aerial socket,

\$4 is associated with the aerial socket, and opens automatically upon insertion of a suitable aerial plug.

**\$22, \$23** are the tone control switches, in a 3-position rotary unit beneath the

chassis. This again is indicated in our under-chassis view. It is very simple, but it is shown in detail in the diagram below, where it is drawn as seen from the rear of an inverted chassis.

S24 is the O.M.B. mains switch, ganged

**824** is the Q.M.B. mains switch, ganged with the manual volume control **R11**.

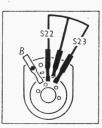
Scale Lamps.—There are two of these, rated at 6.5 V, 0.3 A. They have M.E.S. bases, and large, clear spherical bulbs.

Coils.—All the aerial circuit coils (L1-L3; L5-L6) excepting the S.W.2 unit (L4) and frame winding (L7) are in a single unit on the chassis deck. L4 is beside it, and L7 is mounted on the end of the chassis. The oscillator circuit coils are in two units beneath the chassis, the S.W. coils L8, L9, L12, L13 being in one unit and the M.W. and L.W. coils L10, L11, L14, L15 being in the other.

External Speaker.—Two sockets are provided at the rear of the chassis for the connection of the internal speaker or a low impedance (about  $2\Omega$ ) external speaker. If both are required together, the external speaker plugs may be inserted in the sockets in the plugs of the internal speaker.

Capacitors C24, C25.—These are two dry electrolytics in a single tubular metal con-

Diagram of the tone control switch unit, as seen from the rear of an inverted chassis.



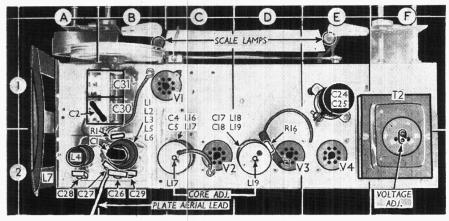
tainer, mounted on the chassis deck. Our sample was a Dubilier type CT unit, rated at  $32+32~\mu F$ , 350~V~D.C. working, 140 mA A.C. maximum. The two positive connections are brought out to two plain tags on the base, and the case forms the common negative connection.

Alternative Rectifiers.—V4 may be an AZ31 (with a 4 V filament) as in our sample, or an EZ35 (with a 6.3 V heater and an isolated cathode). The surge-limiting resistor R21 is omitted when the slower-heating EZ35 is used, but the only other difference is in the heater winding on T2 and the valve holder wiring.

It will be seen from our base connection diagrams beneath the circuit diagram (where both types are shown) that the basings are different, but in the chassis, the cathode and heater (pins 7 and 8) are joined together. Care should be exercised, therefore, when replacing with an AZ31 that the chassis in question has a 4 V secondary winding, as otherwise the valve will be damaged.

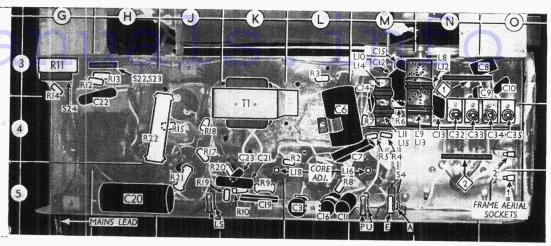
Chassis fitted with the AZ31 bore serial numbers between 575800 and 580100. Our sample, for instance, bore the serial number 577488, and was fitted with an AZ31.

Other Divergencies.—In a very small number of models C1 was omitted. In some chassis R2 may be  $22,000\Omega$  instead of  $47,000\Omega$ .



Plan view of the chassis. Rr and R6 are actually concealed in sleeving, the latter being mounted in the lead to V3 top cap connector. The frame aerial winding L7 is seen on the extreme left of the chassis. The four aerial circuit trimmers are seen grouped round the aerial coils on the left.

Under-chassis view. The two waveband switch units are indicated here by diamon ds numbered I and 2 to agree with the diagrams in col. 1, where they are shown in detail. Switch S4, which is operated by the aerial plug, is indicated in location M5.



#### DRIVE CORD REPLACEMENT

Forty inches of Nylon braided glass yarn is required for the drive cord, which should be run as shown in the sketch

First thread the cord through the cursor carriage as shown in the sketch, with the free ends of the cord emerging from the rear of the carrier. Thread the righthand end of the cord through the entry hole in the rim of the drum, then tie a loop about in diameter and slip it into the groove round the centre boss of the drum.

Slide the cursor along the cord so that it takes up a position somewhere on the upper horizontal run, and complete the circuit as shown, making two turns round the control spindle and tying off so that the tension spring is extended to about 11 times its closed length.

With the spring unhooked, the cursor can be slid comfortably along the cord to

resistor between the top cap of the valve and chassis.

Switch set to M.W., turn gang and volume control to maximum, feed in a 465 kc/s (645.16 m) signal, and adjust the cores of L16, L17, L18 and L19 (location references M5, C2, K5, D2) for maximum output. Finally, remove the  $100,000 \Omega$  resistor and replace V1 top cap connector.

R.F. and Oscillator Stages. - With the gang at maximum capacitance the cursor should be vertical and coincident with the high wavelength ends of the four scales. It may be adjusted in position by sliding the cursor carriage along the drive cord. Transfer "live" signal generator lead to "A" socket, via a suitable dummy aerial.

M.W.-Switch set to M.W., tune to 200 m on scale, feed in a 200 m (1,500 kc/s) signal, and adjust C34 (O4) and C29 (B2) for maximum output. Tune to 500 m on scale, feed in a 500 m (600 kc/s)signal, and check calibration.

S.W.2.—Switch set to S.W.2, tune to 60 m on scale, feed in a 60 m (5.0 Mc/s) signal, and adjust C33 (N4) and C28 (A2) for maximum output. Tune to 200 m on scale, feed in a 200 m (1,500 kc/s) signal, and check calibration.

#### Service Short Cuts

#### Vibrating Barretter

I have recently experienced a familiar trouble on an A.C./D.C. receiver using a barretter in the heater circuit. The barretter is mounted sufficiently close to the speaker to feel the influence of its magnetic field, and when it is operated on A.C. mains, the alternating flow of current in the resistance element causes the wire to be attracted and repelled at mains frequency, so that it vibrates visibly.

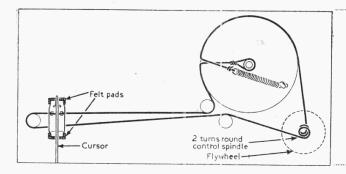
In this particular model, a G.E.C. BC4835, the vibration was so violent that adjacent wires touched, causing crackles in the speaker. I cured it in this case by fitting an iron screen between the barretter and the speaker, but I think some kind of screen should be fitted in all cases, as much milder vibration than this can shorten the life of the barretter considerably.-H. B.,

### Crewe. Marconiphone 262

A Marconiphone 262 I had in recently gave very distorted results on high notes, almost as though the speech coil was faulty, but another speaker sounded just as bad.

It was noticed that what appeared to be a 2 µF bias decoupling capacitor in the block had been replaced by a 2 µF electrolytic type, but as this capacitor is part of an audio feed-back circuit to the detector anode (actually it was C10 in "Trader" Service Sheet 518), to increase low note response, the electrolytic type was not suitable.

Replacing it with a 2 µF paper capacitor completely restored the quality of tone, although the electrolytic capacitor appeared to be perfectly O.K. on test.-L. T., Scar-



Sketch showing the tuning drive system as it appears when viewed from the front, with the gang at minimum capacitance, which is the correct position for fitting a new cord.

approximately the correct position, final adjustment being made on the taut cord with the scale in position after replacing the chassis in the cabinet.

#### CIRCUIT ALIGNMENT

For these operations the chassis must be in position in the cabinet.

i.F. Stages.—Connect signal generator, via an 0.1 μF capacitor in the "live" lead, to control grid (top cap) of V1 and the E socket, after removing the original top cap connector and joining a 100,000 Ω

L.W.—Switch set to L.W., tune to 1,000 m on scale, feed in a 1,000 m (300 kc/s) signal, and adjust C35 (O4) and C26 Tune to (B2) for maximum output. 2,000 m on scale, feed in a 2,000 m (150 kc/s) signal, and check calibration.

S.W.1.—Switch set to S.W.1, tune to 15 m on scale, feed in a 15 m (20 Mc/s) signal, and adjust C32 (N4) and C27 (B2) for maximum output, while rocking the gang. Tune to 40 m on scale, feed in a 40 m (7.5 Mc/s) signal, and check calibration.

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