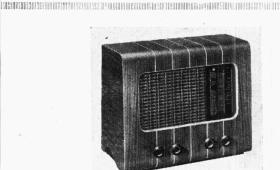
"TRADER" SERVICE SHEET

PYE K47C

846

TRANSPORTABLE A.C./D.C. TABLE RECEIVER



FRAME aerial for M.W. and L.W. and a plate aerial for S.W. are provided in the Pye K47C, a 4-valve (plus rectifier) 3-band superhet designed for A.C. or D.C. mains of 200-250 V. There is provision for connecting an external aerial, and the circuit includes an R.F. amplifier.

A coupling transformer isolates the pick-up sockets from the mains, and these and the external speaker sockets are returned to the earth socket.

turned to the earth socket.

Release date and original price: October 1947; £22 is plus purchase tax.

CIRCUIT DESCRIPTION

On S.W., input from plate aerial is inductively coupled by L1 to single-tuned circuit L2, C38.

On M.W., tuned frame aerial input is provided by L3, C38, with the addition of loading coil L4 on L.W., and provision is made for the connection of an external aerial, which is operative on all bands, via series capacitor C3.

First valve (V1, Mullard metallized EF39) is a variable-mu R.F. pentode operating as signal frequency amplifier with tuned anode coupling by L5, C41 (S.W.), L6, C41 (M.W.) and aperiodic coupling by R5 (L.W.) to triode-hexode valve (V2, Mullard metallized CCH35) which operates as frequency changer with internal coupling.

Triode oscillator anode coils L10 (S.W.), L11 (M.W.) and L12 (L.W.) are tuned by C45. Parallel trimming by C42 (S.W.), C43 (M.W.) and C12, C44 (L.W.); series tracking by C13 (S.W.) and C14 (M.W. and L.W.). Inductive reaction coupling to control grid by coils L7 (S.W.), L8 (M.W.) and L9 (L.W.), with additional capacitative coupling across the impedance of the trackers, which are common to grid and anode circuits.

Third valve (V3, Mullard metallized EF39) is a second R.F. pentode, operating

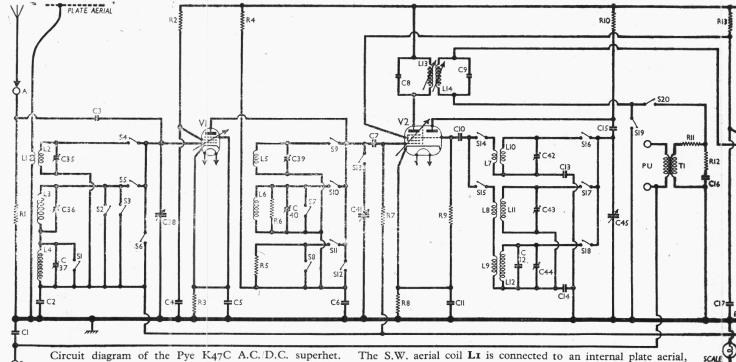
with fixed grid bias as intermediate frequency amplifier with tuned-primary, tuned-secondary transformer couplings C3, L13, L14, C9 and C20, L15, L16, C21, in which the tuning capacitors are fixed and alignment is carried out by varying the positions of the iron-dust cores.

Intermediate frequency 465 kc/s.

Diode second detector is part of double diode pentode output valve (V4, Mullard metallized CBL31). Audio frequency component in rectified output is developed across load resistor R17 and passed via A.F. coupling capacitor C26, manual volume control R18 and grid stopper R20 to control grid of pentode section. I.F. filtering by C23, R16 and C24 in diode circuit.

Second diode of V4, fed from V3 anode via C27, provides D.C. potential which is developed across load resistor R25 and fed back through a decoupling circuit as G.B. to R.F. and F.C. stages, giving A.V.C. Delay voltage, together with G.B. for pentode section, is obtained from the drop across R21, R22 in V4 cathode lead to chassis. Fixed tone correction in pentode anode circuit by C28, and provision for the connection of a low-impedance external speaker across T2 secondary via sockets on the internal speaker plugs.

For "Gram" operation, V3 is con-



Circuit diagram of the Pye K47C A.C./D.C. superhet. The S.W. aerial coil LI is connected to an internal plate aerial, the M.W. aerial tuning coil L3 is wound as a frame aerial, and socket A is provided for the connection of an external aerial via C3 to the control grid of the R.F. amplifier VI. This valve is R.-C. coupled on L.W. to the next valve. An isolating transformer couples the pick-up sockets to the I.F. amplifier V3, which becomes an A.F. amplifier on Gram. In some cases RI may be in parallel with C3, and the scale lamp circuit may be in the "negative" mains lead.

verted to an A.F. amplifier by connecting the secondary winding of the pick-up iso-lating transformer T1 in its grid circuit, via \$19, \$20 and a tone correcting network. The amplified signal developed across R15 in the anode circuit is fed via C22 and S22 to V4 C.G. circuit.

Voltage negative feed-back is provided from V4 anode via the potential divider network C30, R28, R29, C29, R30, C31, and limiting resistor R23, to the control grid circuit. Switches S25-S30 permit the frequency response to be modified by manipulation of the circuit arrangement, giving a four-position tone control: Fidelity, Brilliant, Mellow 1 and Mellow 2.

In the Fidelity position \$26 and \$28 close, so that C30, R28, R29, and R30, C31 in parallel, form the potential divider, and the voltage developed across R30 is fed back via C29 and R23.

In the Brilliant position, \$26 and \$28 are open, and \$25, \$27 closed. R23 is now directly connected to the potential divider and C29 and R30 are connected in series across C31.

In the Mellow positions, \$26 and \$28 close again, and \$25, \$27 open, as for Fidelity, but in position M1 \$29 closes, short-circuiting R29, and in position M2 \$30 closes, short-circuiting R28 and R29.

\$28 is shown in the circuit diagram as three separate switches a, b and c connected in parallel. Although it is contrary to our normal practice to show switches thus in the circuit diagram, it is necessary in this instance in order that the diagram shall agree with the practical switch data overleaf.

When the receiver is operated from A.C. mains, H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Mullard GY31), which, with D.C. mains, behaves as a low resistance. Smoothing by ironcored choke L18 and electrolytic capacitors C33, C34.

Valve heaters, together with scale lamps and adjustable ballast resistor, are connected in series across mains input. Mains R.F. filtering by C32, and earth isolation by C1.

COMPONENTS AND VALUES

R1		RESISTORS	Values (ohms)	Loca- tion
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R1	Aerial shunt	500.000	H5.
R3 V1 fixed G.B. 330 16 R4 V1 anode feed 1,000 H7 R5 V1 L.W. anode load 4,700 H7 R6 R.F. M.W. shunt 22,000 H6 R7 V2 fixed G.B. 330 J7 R9 V2 osc. C.G. 47,000 J7 R10 Ose. H.T. feed 47,000 J7 R11 Part P.U. tone cor- { 470,000 H8 R12 rector 150,000 H8 R13 S.G.'s H.T. feed 33,000 I8 R14 V3 G.B. resistor 220 H8 R15 V3 anode feed 4,700 G8 R16 I.F. stopper 47,000 G8 R17 Sig. diode load 470,000 G8 R18 Volume control 1,000,000 F5 R20 Grid stopper 47,000 G4 R21 AV.C. delay 220 F8 R23 A.V.C. delay 220 F8 <td>R2</td> <td></td> <td></td> <td></td>	R2			
R5	R3			
R5	R4	V1 anode feed		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R5	V1 L.W. anode load	4,700	H7
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R6	R.F. M.W. shunt		H6
R8 V2 fixed G.B. 330 J7 R9 V2 osc. C.G. 47,000 I7 R10 Osc. H.T. feed 47,000 I7 R11 Part P.U. tone cor- { 150,000 H8 R13 S.G.'s H.T. feed 33,000 I8 R14 V3 G.B. resistor 220 H8 R15 V3 anode feed 4,700 G8 R16 I.F. stopper 47,000 G8 R17 Sig. diode load 470,000 G8 R18 Volume control 1,000,000 F5 R19 FB. coupling 4,700 C4 R21 V4 pent. G.B. and { 220 G8 R22 A.V.C. delay 220 F8 R23 FB. coupling 1,000,000 G8 R24 A.V.C. decoupling 1,000,000 G8 R25 A.V.C. diode load 1,000,000 G8 R26 V5 surge limiter 82 26 Heater ballast 750* 22,	R7.	V2 hex. C.G		J6
R10	R8	V2 fixed G.B		J7
R10	R9	V2 osc. C.G	47,000	J7
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R10	Osc. H.T. feed	47,000	17
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R11	Part P.U. tone cor-		H8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R12		150,000	H8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R13		33,000	18
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R14	V3 G.B. resistor	220	$\mathbf{H}8$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			4,700	G8
R17 Sig. diode load 470,000 G8 R18 Volume control 1,000,000 F5 R19 FB. coupling 4,700 F8 R20 Grid stopper 47,000 C4 R21 A.V.C. delay 220 G8 R23 FB. coupling 15,000 F5 R24 A.V.C. decoupling 1,000,000 G8 R25 A.V.C. diode load 1,000,000 G8 R26 V5 surge limiter 82 E6 R27 Heater ballast 750* D3 R28 Tone control resis- 22,000 F5 R30 Tors 47,000 G6	R16	I.F. stopper	47,000	G8
R19			470,000	G8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Volume control		F5
R21 R22 pent. G.B. and { 220 G8 R25 A.V.C. delay { 220 F5. B. coupling 1,000,000 G8 R25 A.V.C. diode load 4,000,000 G8 R26 R27 R27 R28 R29 tors { 27,000 F5 Y60 R30 S22,000 F5 47,000 G6 R30 R30 S22,000 F5 47,000 F5 R30 S22,000 F5 R30 S22,000 F5 R30 S22,000 R30 R30 S22,000 R30 R30 S22,000 R30 R30 S22,000 R30 R30 R30 R30 R30 R30 R30 R30 R30	R19			F8
R22 A.V.C. delay 220 F8 R23 FB. coupling 15,000 F5 R24 A.V.C. decoupling 1,000,000 G8 R25 A.V.C. diode load 1,000,000 G8 R26 V5 surge limiter 82 E6 R27 Heater ballast 27,000 F5 R28 Tone control resis- 22,000 F5 47,000 G6	R20	Grid stopper	47,000	C4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	R21	V4 pent. G.B. and	220	G8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R22	A.V.C. delay \		F8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		FB. coupling	15,000	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		A.V.C. decoupling	1,000,000	
R27 Heater ballast 750* D3 R28 Tone control resis- 27,000 F5 R30 tors 47,000 G6	R25	A.V.C. diode load	1,000,000	G8
$ \begin{bmatrix} R28 \\ R29 \\ R30 \end{bmatrix} \begin{cases} Tone \ control \ resis- \\ tors & \dots \end{cases} $				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Heater ballast		
$\begin{bmatrix} R29 \\ R30 \end{bmatrix}$ tors $\begin{bmatrix} 22,000 \\ 47,000 \end{bmatrix}$ $\begin{bmatrix} 66 \\ G6 \end{bmatrix}$		Tone control regis-		
K30) (47,000 G6			22,000	
24 4 A	R30	,	47,000	G6
	超過機			Į.

* Fanned at $570[\Omega + 90 \Omega + 90 \Omega]$ from V5

	CAPACITORS	Values (µF)	Loca- tion
C1	Earth isolator	0.01	18
C2	V1 C.G. decoupling	·0·1	B2
C3	Aerial series	0.000005	H_5
C4 .	V1 S.G. decoup	0.1	16
C5	V1 cath. by-pass	0.1	-H6
C6	V1 anode decoup,	0.1	$\mathbf{H}6$
C7	V2 hex. C.G	0.0001	16
C8	1 1st I.F. transformer	0.00007	B4
C9	f tuning \	0.00007	B4
C10	V2 osc. C.G	0.0001	17
C11	V2 cath. by-pass	0.1	J7
C12	L.W. fixed trim	0.00033	H7
C13	Osc. S.W. tracker	0.005	17
C14	M.W., L.W. tracker	0.00057	H7
C15	Osc. anode coup	0.0001	17
C16	P.U. tone corrector	0.002	H8
C17	S.G.'s decoupling	0.1	18
C18	\ V3 cath. by-passes \{	0.1	H8
C19*		50.0	J8
C20	2nd I.F. trans-	0.00014	C4
C21	former tuning \	0.00014	C4
C22	V3 anode capacitor	0.1	H7
C23	I.F. by-passes {	0.0001	G8
C24) (0.0001	G8
C25*	V4 cath. by-pass	25.0	F8
C26	A.F. coupling	0·01 0·00001	G8 H8
C27	A.V.C. coupling		G7
C28	Tone corrector	$0.001 \\ 0.02$	G5
C29	Parts of negative	0.02	G6
C30 C31	feed-back circuit)	0.02	G6
C32	R.F. by-pass	0.01	F8
C33*		16:0	C3
C34*	H.T. smoothing }	24.0	C3
C351	Aerial S.W. trim	0.00005	B2
C36‡	Aerial M.W. trim	0.00005	A3
C37‡	Aerial L.W. trim	0.00005	A3
C38‡	Aerial tuning	0.000532	B2
C391	R.F. S.W. trim	0.00005	H6
C401	R.F. M.W. trim	0.000015	H6
C41†	R.F. tuning	0.000532	B3
C421	Osc. S.W. trim	0.00005	17
C43†	Osc. M.W. trim	0.00005	H7
C44:	Osc. L.W. trim	0.00005	H7
C45†	Oscillator tuning	0.000532	B3

* Electrolytic." † Variable. ‡ Pre-set.

C20 / S / LL6	C27 R16 C26 R20 R17 R19 R23 R23 S26 S27 A B C31 R30 C31 C31 C31 C31 C31 C31 C31 C	V2 MET V4
SCALE GRAPS GRAP LAMPS GRAPS G	OR V5 R26 C32 SAFETY SOCKETS M.	VS OF DC AINS

OTI	HER COMPONENTS	Approx. Values (ohms)	Loca- tion
L1 L2 L3 L4 L5 L6	Aerial S.W. coup Aerial tuning coils R.F. S.W. tuning R.F. M.W. tuning	0·1 Very low 1·0 8·0 Very low 2·0	B2 B2 A2 A3 H6 G6
L7 L8 L9 L10 L11	Osc. S.W. reaction Osc. M.W. and L.W. { reaction, total { Osc. tuning_coils }	24·0 2·25 Very low 3·8	17 H7 H7 17 H7
L12 L13 L14 L15	1st I.F. { ,Pri } trans. { Sec } 2nd I.F. } Pri	4·5 10·0 10·0 6.5 6.5	H7 B4 B4 C4 C4
L16 L17 L18 T1	f trans. \ Sec Speech coil H.T. choke Pick-up \ Pri trans. \ Sec	2·5 530·0 1,150·0 5.200·0	D2 G8 G8
T2 S1- S24	Output { Pri Sec Waveband switches	550·0 0·3	E7 E7
S25- S30 S31, S32	Tone control switches Mains switches	=	G5 G6
F1,F2	Mains fu es, 1.0 A.	_	D4

DISMANTLING THE SET

The bottom of the cabinet is fitted with a detachable cardboard cover, upon removal of which (four round-head wood screws) access may be gained to most of the components beneath the chassis deek. Removal of the chassis, however, is only a few moments' work.

Removing Chassis.—Remove the four control knobs (pull-off) after slackening their recessed grub screws.

(Continued overleaf)

The Wireless & Supplement to Electrical Trader, January 24, 1948

Waveband Switch Diagrams and Table

Withdraw the two speaker lead plugs from their sockets at the rear of the chassis. Remove the two fixing screws from the lower rear corners of the chassis. Withdraw chassis, about two inches, then lift the rear edge and slide it out. It should be noted that if it is desired to operate the chassis on the bench, the mains safety plug, which is secured to the receiver back by a paxolin and plywood carrier (two wood screws), must be in position in its sockets beneath the mains fuse panel. Removing Speaker.—With the chassis removed free the speaker leads from the soft metal clip on the side of the cabinet, and remove the four nuts (with spring washers) securing the speaker to the sub-baffle. When replacing, the connecting panel should point towards the bottom right-hand corner of the cabinet, when viewed from the rear.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receiver when it was operating on A.C. mains of 222 V. using the 216-235 V tapping on the heater ballast resistor.

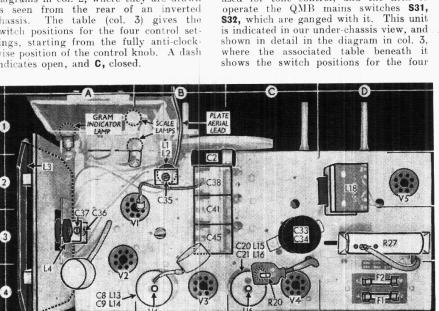
The receiver was tuned to the lowest wavelength on the M.W. band, and the volume control was at maximum, but there was no signal input. Voltages were measured on the 400 V scale of a model 7 Universal Avometer, chassis being the negative connection.

Valve		Anode Current (mA)		Screen Current (mA)
V1 EF39	205	8·3 2·1)	137	2.4
V2 CCH35		$\left\{\begin{array}{c} 2 \\ 1 \\ 2 \\ 8 \end{array}\right\}$	87	$2 \cdot 1$
V3 EF39	185	5.5	87	1.7
V4 CBL31 V5 CY31†	196	33.0	212	3.9

† Cathode to chassis, 250 v. D.C.

GENERAL NOTES

Switches.-S1-S24 are the waveband and radio/gram change-over switches, ganged in three rotary units beneath the chassis. These units are indicated in our underchassis view, and shown in detail in the diagrams in col. 2, where they are drawn as seen from the rear of an inverted chassis. The table (col. 3) gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed.



Plan view of the chassis, showing the frame winding L3, with trimmers and L.W. loading coil L4, forming a vertical assembly on the left. The heater circuit ballast resistor R27, seen on the right, should be rated at about 45W.

\$3 -55-C	\$24 \$24 \$3 \$51 \$2
\$7 \$9 \$8-\$10 \$12	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
\$ 516 5 17 19 5 18 520	\$327 \$21 \$15

Diagrams of the three waveband switch units drawn as seen when viewed from the rear of an inverted chassis, numbered in diamond enclosures to agree with the under-chassis illustration. The associated table is on the right.

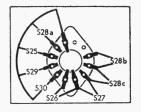
\$25-\$30 are the tone control switches, ganged in a single five-position unit beneath the chassis. Four positions are used for tone control, and the fifth to

Switch	S.W.	M.W.	L.W.	Gram.
S1		С		
S2 S3 S4 S5	C		11-Maria	
S3	C	***************************************	"	
SI	C		С	C
S5	-	C	C	0
86	-			C
87 88	C	C		
S9	C	J		
S10		C		
S11			С	
$\tilde{S12}$	-			C
S13	С	C	1	1.000
S14	С		_	
S15		С	C	-
S16	C	-		
S17		C		
S18 S19	0	0	č	
519	C	U		C
S20	C	C	С	
S21 S22	C	C	c	C
S23	C	С	C	
S24		_		C

tone control settings, starting from the "OFF" position and turning the control A dash indicates open, and clockwise. C, closed.

In order to show clearly the action of \$28, this has been divided into three parts, numbered a, b, c, as these are widely separated on the unit and connected in parallel. If all the parallel connections

Tone Control Switch Unit



Switch	FID	BRI	M1	M2
S25		С		
S26	C		C	C
S27	, ·	С		
S28a	С			
S28b				С
S28c			C	
S29			C	
S30				С

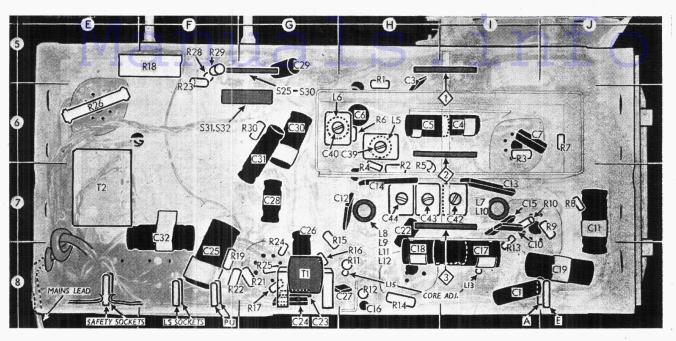
Diagram of the tone control switch unit \$25-\$30 (above), as seen from the rear of an inverted chassis with the mains switch removed. S28a, b and c are connected in parallel. Below it is the associated switch table.

on the switch unit were shown as such they would confuse the diagram.

The sketch in col. 4 shows this unit again, in the same position, as it appears when wired ready for fitting into the chassis. When a new unit is fitted, it is advisable to wire it up thus beforehand,

while all the tags are accessible.

External Speaker. — The secondary winding of the output transformer T2 is brought out to a pair of sockets at the rear of the chassis, and from these the internal speaker or a low impedance $(2-4 \Omega)$ external speaker may be operated. If both are required together, the external



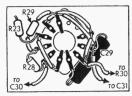
Under-chassis view. The waveband switch units, numbered 1, 2 and 3 in diamond enclosures, are indicated right of the centre, and the tone control switch unit S25-S30 is indicated left of centre. These units are all shown in detail in the diagrams in cols. 2 and 3. The pins shown in the safety sockets at the bottom left corner are normally fixed to the back cover of the receiver.

speaker plugs may be inserted in sockets in the tops of the internal speaker plugs.

Scale and Indicator Lamps.—These are three Osram M.E.S. type lamps, with small clear spherical bulbs, rated at 4 V. 0.3 A. In early versions they were wired between the "negative" side of the mains and chassis, instead of directly in the heater circuit as in our sample, and they were then rated at 6 V, 0.3 A.

Capacitors C33, C34.—These are two

dry electrolytics in a tubular metal con-



Sketch showing the tone control switch unit, wired ready for fitting into the chassis.

tainer on the chassis deck. Of the three tags on its base, the red lead is the positive of C33 (16 μ F), the yellow is the positive of C34 (24 μ F), and the black is the common negative. Both are rated at 350 V D.C. working, but the red-tagged section is rated as reservoir. Our unit was a Hunt's List No. K12.

Fuses.—F1 and F2 are the mains circuit fuses, rated at 1 A each, 14in in length.

CIRCUIT ALIGNMENT

1.F. Stages.—Connect signal generator via an $0.1\mu F$ capacitor in the "live" lead, to control grid (top cap) of V2 and the E socket, removing the original top cap connector but connecting a $500,000\Omega$ resistor between the top cap of the

valve and the A.V.C. line. A convenient point on the A.V.C. line is the tag on the frame aerial connecting panel to which is connected

aerial connecting panel to which is connected a brown plastic covered lead. Switch set to M.W., turn volume control to maximum, and tune to 570 m on scale. Feed in a 465 kc/s (645.16 m) signal, and adjust the cores of L13, L14, L15 and L16 (chassis locations 18, B4, H8, C4) for maximum output. Finally, remove the 500,000 Ω resistor and replace top cap.

signal generator lead to A socket, via a suitable dummy aerial.

M.W.—With set still switched to M.W., tune to 200 m on scale, feed in a 200 m (1,500 kc/s) signal, and adjust C43 (H7), C40 (G6) and C36 (A3) for maximum output. Tune to 500 m on scale, feed in a 500 m (600 kc/s) signal, and check calibration.

L.W.—Switch set to L.W., tune to 1,200 m on scale, feed in a 1,200 m (250 kc/s) signal, and adjust C44 (H7) and C37 (A3) for maximum output. Tune to 1,800 m on scale, feed in an 1,800 m (166.7 kc/s) signal, and check calibra-

S.W.—Switch set to S.W., using a 400 Ω dummy aerial, tune to 17.5 m on scale, feed in dummy aerial, tune to 17.5 m on scale, feed in a 17.5 m (17.14 Mc/s) signal, and adjust C42 (17), C39 (H6) and C35 (B2) for maximum output. Feed in a 43 m (6.98 Mc/s) signal, tune it in, and check calibration. If it is out, adjust the turns of L10 (17) to correct it; then adjust the turns of L5 (H6) and L2 (B2) for maximum output. Repeat the S.W. adjustments

DRIVE CORD REPLACEMENT

Four feet of Nylon braided glass yarn is sufficient for the drive cord replacement, this length including an ample margin for tieing

The scale glass must first be dismounted by removing the upper clamp (two set screws) and slackening the screws in the bottom one. The glass can then be lifted out, with its rubber packing pieces.

The sketch (next col.) then shows the course taken by the cord, as seen when viewed from the front of the chassis with the gang at

maximum, although in practice the lower portion is partly obscured by metal plates.

One end of the cord should be tied to the free end of the tension spring, which is hooked to its anchor. The cord then passes out of the drum through the gap, clockwise round the drum, down under the guide pulley, then through the slot in the scale backing plate and under the drive spindle round which it makes 2½ turns anti-clockwise. Finally it goes up to the top pulley, over it, and down under the gang drum back to the free end of the

Sketch showing the tuning drive cord system as seen from the front of the chassis, after removing the scale Cursor panel, when the gang is at maximum. Felt pads on the ends of the cursor rub on the scale panel. Control 2 turns round drive spindle

spring, passing out of the scale assembly through the upper slot.

The cursor carrying plate is clamped lightly on to the long vertical run of cord, then fixed with the cursor about 1½in below the centre of the upper pulley. Fine adjustment can be made by turning the drum in the gang spindle when the scale is in position. With the gang at maximum, the cursor should be level with the spots at the tops of the three scales. The felt pads on the cursor rub on the edges of the scale panel. of the scale panel.

Printed in England by The Cornwall Press Ltd., Paris Garden, London, S.E.1