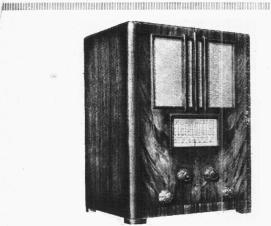
"TRADER" SERVICE SHEET

BLUE SPOT "POPULAR"



The Halcyon Briton Five able model. The radiogram has an additional knob below those seen here.

HREE wavebands are employed in the Halcyon Briton Five receiver, with a band-pass input circuit on MW and LW. The SW range is 16.5 to

The receiver is a 4-valve (plus rectifier) superhet designed for use with AC or DC mains of 195-260 V. No provision is made for a gramophone pick-up.

The Blue Spot Popular employs an identical chassis, while in the Briton Five radiogram a modified chassis, fully described overleaf under "Radiogram Modifications," is used.

Release date, all models: 1936.

Original prices: Halcyon Briton Five, model, £10 10s.; Radiogram, £18 18s.; Blue Spot Popular, £10 10s.

CIRCUIT DESCRIPTION

Aerial input on MW and LW via isolating capacitor C1 and coupling coils L1, L2 to inductively coupled band-pass filter. Primary coils L3, L4 are tuned by C22; secondaries L8, L9 are tuned by C24. Coupling by coils **L5**, **L6**.

On SW, input is via C1 and coupling capacitor C3 to single tuned circuit L7, C24, and L8, L9 are short-circuited by S4.

First valve (V1, Tungsram metallised VO13) is an octode operating as frequency changer with electron coupling. Oscillator grid coils L10 (SW), L12 (MW) and L13 (LW) are tuned by C25. Parallel trimming by C26 (MW); series tracking by C6, C28 (MW), while C27 is added in series with them on LW. Reaction coupling from anode by coils L11 (SW) and L14, L15 (MW and LW), S8 short-circuiting the latter pair on SW.
Second valve (V2, Tungsram metallised

VP13B) is a variable-mu RF pentode operating with fixed grid bias, derived

from the drop along R4, as intermediate frequency amplifier with tuned-primary, tuned-secondary transformer couplings C29, L16, L17, C30 and C31, L18, L19,

"BRITON= FIVE"

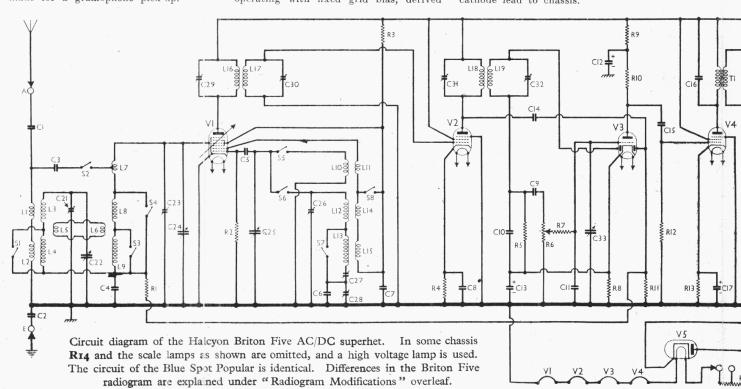
Intermediate frequency 130.5 kc/s.

Diode second detector is part of double diode triode valve (V3, Tungsram metallised DDT13). Audio frequency component in rectified output is developed across load resistor **R5** and passed via AF coupling capacitor C9, manual volume control R6 and series resistor R7 to control grid of triode section, which operates as AF amplifier.

IF filtering by C10, R7 and C11. R7 also acts in conjunction with variable capacitor C33 to form the variable tone control in the manner of a potential divider, the comparatively low impedance of C33 when at maximum capacity, as compared with R7, shunting the control grid circuit heavily at upper audio frequencies and thus emphasising the bass frequencies, while the effect is less em-

phatic when **C33** is at minimum.

Second diode of **V3**, fed from **V2** anode via **C14**, provides DC potential which is developed across load resistor R11 and fed back through a decoupling circuit as GB to frequency changer valve, giving automatic volume control. Delay voltage, together with GB for triode section, is obtained from the drop along R8 in cathode lead to chassis.



Under-chassis view. The waveband switches are all indiviidentidually fied here. The trimmers C21, C23 and C26 are also indicated, but their adjustments are reached through holes in the chassis deck.

Resistance-capacity coupling by R10, C15 and R12 between V3 triode and pentode output valve (V4, Tungsram PP36 or Mullard Pen 36C). Fixed tone correction by C16 in anode circuit. Provision for connection of low impedance external

speaker by sockets across the secondary of the internal speaker input transformer T1.

When the receiver is operating from AC mains, HT current is supplied by half-wave rectifying valve (V5, Tungsram V30) which, with DC mains, behaves as a low resistance. Smoothing is effected by speaker field L22 and electrolytic capacitors C18, C19.

Valve heaters, together with scale lamps (which are shunted by R14), and tapped ballast resistor R15, are connected in series across mains input circuit. RF filtering by chokes L23, L24 and C20, which by-passes the rectifier.

DISMANTLING THE SET

The cabinet is fitted with a detachable bottom, upon removal of which (six countersunk head wood screws) access may be gained to most of the components beneath the chassis.

Removing Chassis.—remove the four control knobs (recessed grub screws);

unsolder from the speaker and input transformer the four leads connecting them to chassis;

remove the four self-tapping screws (with washers) holding the chassis to the bottom of the cabinet.

When replacing, connect the speaker leads as follows: Blue lead with yellow tracer to upper tag on right of transformer and upper tag on speaker field coil panel; yellow lead with black tracer to lower tag on transformer; red lead to lower tag on speaker field coil panel; brown lead with green tracer and earthing tag to one of the speaker fixing

Removing Speaker.—Remove the nuts (with washers) from the three screws holding the speaker to the sub-baffle.

When replacing, the transformer should be on the right, and if the leads have been unsoldered they should be connected as described previously.

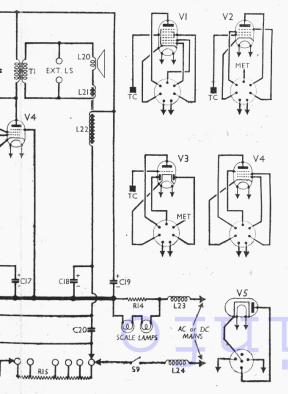
COMPONENTS AND VALUES

	CAPACITORS	Values (µF)
C1.	Aerial isolator	0.0005
C2:	Earth isolator	0.1
C3	Aerial SW coupling	0.0005
C4:	V1 pent. CG decoupling	0.1
C5-	V1 osc. CG capacitor	0.0001
C6	Osc. fixed MW tracker	0.0015
C7	V1 HT feed decoupling	0.1
C8-	V2 cathode by-pass	0.1
C9	V3 triode AF coupling	0.0005
C10	If by-pass capacitors {	0.0001
C11)	0.0001
C12*	V3 triode anode decoup-	
CHOR	ling	2.0
C13*	V3 cathode by-pass	50.0
C14	V3 AVC diode coupling	0.0001
C15 C16	AF coupling to V4 Fixed tone corrector	$0.1 \\ 0.005$
C17*	V4 cathode by-pass	50.0
C18*		16.0
C19*	HT smoothing capacitors {	16.0
C20	Mains RF by-pass	0.05
C21†	B-P pri. MW trimmer	0.00003
C22†	Band-pass pri. tuning	0.00045
C231	B-P sec. MW trimmer	0.00003
C24+	Band-pass sec. tuning	0.00045
C25†	Oscillator circuit tuning	0.00045
C261	Osc. circ. MW trimmer	0.00003
C27‡	Osc. circ. LW tracker	0.00075
C28‡	Osc. circ. MW tracker	0.00075
C29‡	1st IF trans. pri. tuning	0.000178
C3)‡	1st IF trans. sec. tuning	0.000178
C31‡	2nd IF trans. pri. tuning	0.000178
C3 2‡	2nd IF trans. sec. tuning	0.000175
C33†	Variable tone control	0.0005

 $\begin{array}{c} \text{anel} \; ; \\ \text{arth-} \\ \text{xing} \end{array}$

† Variable.

‡ Pre-set.



Radio

692 HALCYON BRITON FIVE

Supplement to The Wireless & Electrical Trader, October 7, 1944

	RESISTORS	Values (ohras)
R1	V1 pent, CG decoupling	250 000
R2	V1 osc, CG resistor	50 000
R3	V1 SG and osc. HT feed	10,000
R4	V2 GB resistor	300
R5	V3 signal diode load	1,000.000
R6	Manual volume control	1,000,000
R7	IF stopper and part tone	
	control	1,000,000
R8	V3 GB and AVC delay	1,000
R9	V3 triode anode decoup-	
	ling	10,000
R10	V3 triode anode load	50,000
R11	V3 AVC diode load	1,000,000
R12	V4 CG resistor	250,000
R13	V4 GB resistor	150
R14	Scale lamps shunt	20
R15	Heater circuit ballast	760

† Tapped at 50 $\Omega+425\,\Omega+100\,\Omega+100\,\Omega+85\,\Omega$ from V5 heater end.

O	THER COMPONENTS	Approx. values (ohms)
$\begin{array}{c} L1 \\ L2 \end{array}$	Aerial coupling coils, total	4.5
L3 L4	Band-pass primary coils {	$\frac{2 \cdot 6}{28 \cdot 5}$
L5 L6	Band pass coupling coils {	Very low Very low
L7 L8	Aerial SW tuning coil	Very low
L9	Band-pass secondary coils {	28.0
$\begin{array}{c} L10 \\ L11 \end{array}$	Osc. SW tuning coil Osc. SW reaction coil	Very low 0.2
L12 L13	Osc. MW tuning coil Osc. LW tuning coil	$\frac{2 \cdot 2}{20 \cdot 0}$
L14	Oscillator MW and LW	
$\begin{array}{c} L15 \\ L16 \end{array}$	reaction coils, total 1st IF trans. {Pri	3·5 65·0
L17 L18	(Sec	65·0 65·0
L19 L20	Speaker speech coil	65·0 1·6
L21	Hum neutralising coil	0.1
L22 L23	Speaker field coil Mains RF filter chokes {	650·0 3·2
L24 T1	Speaker input { Pri.	3.2
S1-S8	trans. Sec	0.5
S1-58 S9	Mains switch, ganged R6	

but tuned to the lowest wavelength on the MW band.

Voltages should be measured with a high resistance meter whose negative lead is connected to chassis.

Valve	Anode Voltage (V)	Anode Current (mA)	Screen Voltage (V)	Screen Current (mA)
V1 VO13	$\begin{cases} 192 \\ \text{Osci} \\ 102 \end{cases}$	$\left\{ \begin{array}{c} 2 \cdot 9 \\ \text{llator} \\ 3 \cdot 3 \end{array} \right\}$	102	5.4
V2 VP13B V3 DDT13	192 75	6.7	192	2.1
V4PP36 V5 V30	178 240†	41.0	192,	5.3
19 150	2401			

† Cathode to chassis, DC.

GENERAL NOTES

Switches.—S1-S8 are the waveband switches, ganged in a single three-position rotary unit beneath the chassis. The switches are individually identified in our under-chassis view, while the switch positions for the three control settings are shown in the table below, starting from the SW position of the control spindle and turning clockwise. A dash indicates open, and **C** closed.

sw	MW	LW
С	С	
C	C	
Ċ	_	
Q)s	С	C
C	С	pagence .
	0000	c c c c c c c c c c c c c c c c c c c

Coloured spots on the control knob indicate the switch position. These are green (SW), black (MW) and red (LW), and the scale markings are coloured to agree with them.

A section of the circuit diagram overleaf, redrawn to show the modifications in the radiogram version. V3 becomes a double diode, and V2 operates gram as an AF The amplifier. potential divider R18, R19 is introduced to provide the AVC delay potential.

VALVE ANALYSIS

Valve voltages and currents in the table (next_col.) are approximately those to be expected in an average chassis when the receiver is operating with the voltage adjustment correctly set, the volume control at maximum, with no signal input,

 ${\bf S9}$ is the QMB mains switch, ganged with the manual volume control ${\bf R6.}$

Coils.—All the MW and LW aerial circuit and band-pass coils, L1-L6 and L8, L9, are wound on a common wooden former and mounted beneath the chassis beside the switch unit. L2 is wound underneath L4. The SW aerial and oscil-

lator circuit coils L7 and L10, L11 are also beneath the chassis, L11 being the fine winding on the oscillator unit, interwound with L10.

The MW and LW oscillator circuit coils L12-L15, and the IF transformers L16, L17 and L18, L19, are in three screened units on the chassis deck, with associated pre-set capacitors. The tracker adjustments C27, C28 in the oscillator unit are covered by a small fibre strip, and the fixed tracker C6 is housed inside the unit.

fixed tracker C6 is housed inside the unit.

The mains RF filter chokes L23, L24 are wound on a common wooden former and mounted on the rear member beneath the chassis.

Capacitors C12, C13, C17.—These are three dry electrolytics in separate tubular cardboard containers mounted in the wiring beneath the chassis. C12 is rated at $2\mu F$, 250 V working; C13 and C17 are rated at 50 μF , 12 V working.

Capacitors C18, C19.—These are two dry electrolytics in a single rectangular waxed cardboard container beneath the chassis, having a common negative (black) lead. The red lead is the positive of C18, and the yellow lead that of C19. Both sections are rated at 16 μ F, 300 V working.

Scale Lamps.—These are two Osram MES types, with clear spherical bulbs, rated at 3.5 V, 0.15 A. They are connected in series with the mains lead to chassis, so that they are energised by both heater and HT current, and are shunted by R14. See note under "Chassis Divergencies."

External Speaker.—Provision is made for the connection of a low impedance (about 3-5 Ω) external speaker.

Mains Voltage Adjustment. — The heater circuit ballast resistor R15 is provided with six tappings, including one at each end, for mains voltage adjustment. Four of these, grouped at one end of the unit, provide "coarse" adjustment for mains of 190 V, 210 V, 230 V and 260 V respectively, reading from the centre outwards, while a "fine" adjustment for intermediate voltages is obtained by including or amitting the section between the two tappings at the other end, which drops an additional 10 V if included.

Two leads are used at the "coarse"

Two leads are used at the "coarse" end, one from the mains and one to V5 anode. If the former is connected to the appropriate tapping, the latter may be attached to the next tag, or next but one, to safeguard the valve from current surges and, in the case of 250-260 V mains, reduce the voltage applied to the rectifier.

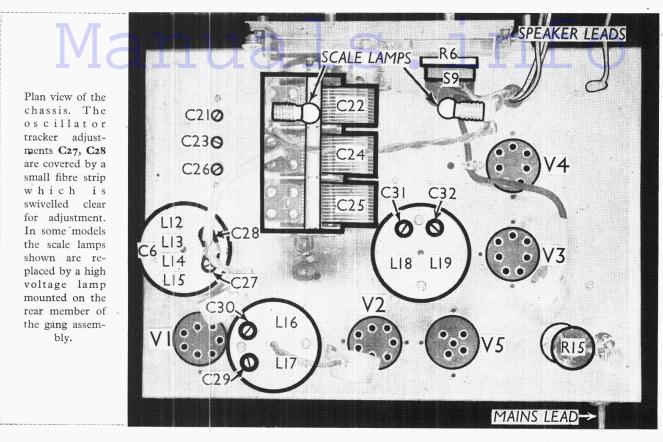
Some chassis are fitted with a different kind of resistor, having only one tapping at one end and five or six at the other. In these cases no separate "fine" adjustment is needed, as sufficiently close rating is obtained from the increased number of

tappings in the first group.

Chassis Divergencies.—Apart from the alternative arrangement of R15, several other modifications may be found. C1 may be 0.01 µF, instead of 0.0005 µF.

V4 may be a Mullard Pen 36C valve. The scale lamps shown in our information may be omitted, and a high-voltage lamp substituted for them.

When this is done, R14 is short-circuited, and an MES lampholder on a



small bracket is bolted to the rear member of the tuning gang, through which the holder shell is connected to chassis. The "pip" contact of the holder is taken via a flying lead to the voltage adjustment tapping on R15, where it might well be fixed permanently to, say, the 210 V setting lug.

A suitable lamp would be the Ismay type C, rated at 230 V, 10 W.

Where the Pen 36C valve is used as V4, the suppressor will, of course, be returned internally to the cathode instead of pin 1. No wiring modification is necessary.

Some chassis employed a Tungsram DD13, and in these models the circuit will be like that shown for the radiogram, but the gram switching will be omitted and V2 not operate as an AF amplifier.

RADIOGRAM MODIFICATIONS

In the radiogram version the chassis is modified to permit the IF amplifier V2 to operate as an AF pre-amplifier for the pick-up. The double diode triode valve V3 is replaced by a double diode valve (Tungsram DD13), and the AF output on gram from V2 is fed via the manual volume control directly to V4. On radio, the circuit is little different from our diagram overleaf except that the triode section of V3 is omitted and the output from the diode circuit is fed via R6 directly to the output valve.

The gramophone motor is connected to the mains input circuit, but normally an AC motor is fitted. Unless, therefore, a universal motor has been fitted, the radiogram must not be connected to DC mains until the motor has been disconnected, when the receiver may be used on radio only.

The revised part of the circuit is shown in the diagram in cols. 1 and 2 opposite.

Components occupying the same positions and having the same values as in the receiver diagram overleaf still bear the same numbers. Other components in the radiogram circuit bear numbers higher than the highest in the tables (col. 6 overleaf and col. 1 opposite); their values are given in the table below.

The pick-up is inserted in the return lead from V2 CG, between L17 and chassis, and S14 short-circuits it on radio. V2 operates as a triode, the screen acting as an anode with R17 as load resistor. R16 and C34 decouple the circuit.

The AF output is coupled via C35, S12 and R6, R7, C33 to V4 CG.

\$10, \$11, \$13 and \$14 close on radio, while \$12 opens. On gram, the positions are reversed.

In order to obtain delay bias for AVC, V3 cathode is taken to the junction of

Additional Components

Resistors		Capacitors	
R16 R17 R18 R19	$\begin{array}{ccc} \dots & 10,000 \Omega \\ \dots & 50,000 \Omega \\ \dots & 100,000 \Omega \\ \dots & \dagger 50,000 \Omega \end{array}$	C34 C35 C36	$\begin{array}{ccc} & 2\mu F \\ & 0.1\mu F \\ & 0.1\mu F \\ or & 0.25\mu F \end{array}$

† May be $15,000 \Omega$.

R18 and R19, which form a potential divider across the HT circuit.

Physically, the radio/gram change-over switch is an additional unit fitted centrally on the front member of the chassis.

CIRCUIT ALIGNMENT

IF Stages.—Connect signal generator to control grid (top cap) of V1 and E socket, feed in a 130.5 kc/s (2,299 m) signal, and adjust C32, C31, C30 and C29 for maximum output, keeping the volume control at maximum and the input signal low to avoid AVC action. The output should now be checked at 5 kc/s above and below 130.5 kc/s (135.5 kc/s and 125.5 kc/s), where the output readings should be approximately equal. If they are not, repeat the adjustments.

RF and Oscillator Stages.—Transfer signal generator leads to A and E sockets, via a suitable dummy aerial. With the gang at maximum, the pointer should cover the 50 m mark on the SW scale.

MW.—Switch set to MW, tune to 250 m on scale, feed in a 250 m (1,200 kc/s) signal, and adjust C26, then C21 and C23 for maximum output. If two peaks are found for C26, select that involving the lesser trimmer capacity.

Feed in a 500 m (600 kc/s) signal, tune it in, and adjust **C28** for maximum output while rocking the gang for optimum results

LW.—Switch set to LW, feed in a 1,900 m (158 kc/s) signal, tune it in, and adjust C27 for maximum output while rocking the gang for optimum results.