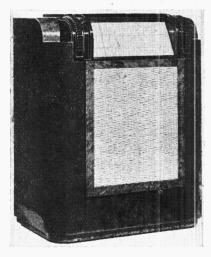
EKCO UAW88 "TRADER" SERVICE SHEET

4-BAND AC/DC SUPERHET



SPIN-WHEEL tuning, provision for connecting a dipole aerial and a special waveband for the reception of the sound channel accompanying television transmissions (for use only in districts within a few miles radius of the transmitting station) are salient features in the Ekco UAW88, a 4-valve (plus rectifier) 4-band superhet designed for AC or DC mains of 200-250 V, 40-100 c/s in the case of AC.

The set is housed in a plastic cabinet of which two alternative finishes are available: walnut and black and ivory. The SW range is 16-50 m.

Release date, 1937.

Original prices: in walnut finish cabi-£13 13s.; black and ivory, £14 0s. 6d.

CIRCUIT DESCRIPTION

Aerial input, from socket A1, is via isolating condenser C1, then on MW via coupling condenser C5 and tapping on L3 and on LW via coupling coil L2, to inductively coupled band-pass filter. Primary coils L3, L4 are tuned by C37; secondary coils L9, L10 by C43. Coupling is effected by mutual inductance of primary and secondary windings. On LW, aerial circuit is shunted by IF filter

L1 and C3. Image suppression by C42.
On television sound, referred to as "TS", and SW bands, input is via S1 and coupling coil L5 (TS) or S2 and L6 (SW) to single-tuned circuits L7, C43 (TS) or L8, C43 (SW). If an ordinary aerial is used, it should be connected to socket A1. If a dipole is used, its leads go to the socket A1 and the unmarked socket (A2 in our circuit diagram) immediately below. Socket "E" should be connected to earth in either case.

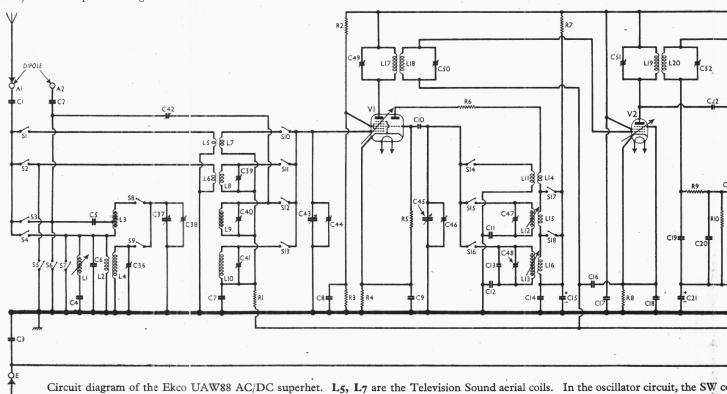
Tuned circuits are connected via selector switches \$10 (TS), \$11 (SW), \$12 (MW) and \$13 (LW) to CG of first valve (V1, Mullard metallised TH21C), a triodehexode operating as frequency changer with internal coupling. Triode oscillator grid coils **L11** (TS and SW), **L12** (MW) and L13 (LW) are tuned by C45; parallel trimming by C46 (SW), C47 (MW) and C13, C48 (LW); series tracking by C11 (fixed-MW), C12 (fixed-LW) and adjustable iron-dust cores in both cases. Reaction by coils L14 (TS and SW), L15 (MW) and **L16** (LW).

No separate oscillator circuit is provided for the television sound band, a harmonic of the SW band serving the pur-

Second valve (V2, Ekco metallised VPU1 or Mullard VP13C) is a variable mu RF pentode operating as intermediate frequency amplifier with tuned-primary, tuned-secondary transformer couplings C49, L17, L18, C50 and C51, L19, L20, C52.

Intermediate frequency 126.5 kc/s.

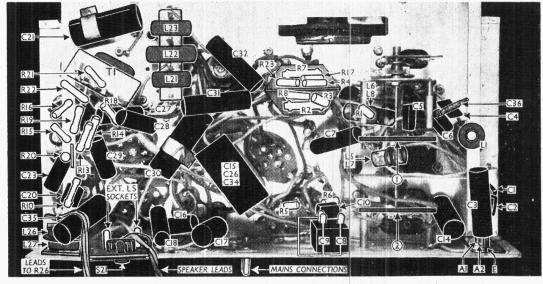
Diode second detector is part of double diode triode valve (V3, Ekco metallised DTU1 or Mullard TDD13C). Audio frequency component in rectified output is developed across load resistor R10 and passed via AF coupling condenser C23 and manual volume control R11 to CG of



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operating harmonically. The extreme right-hand end-section of R26 acts as a surge limiter for V5

Under-chassis view. The waveband switch units are indicated by numbers I and 2 to agree with the detailed diagrams in col. 2 overleaf, the arrows indicating the direction in which they are viewed. **R26** is not mounted on the chassis, but the leads to it are indicated here.



triode section, which operates as AF amplifier.

IF filtering by R9, C19 and C20. Highnote compensation by C24, connected between C23 and triode CG. Variable tone control by RC filter C25, R12 between CG and chassis.

Second diode of **V3**, fed from **V2** anode via **C22**, provides DC potential which is developed across load resistor R16 and fed back through decoupling circuits as GB to FC and IF valves on all bands, giving automatic volume control.

Since R16 is returned to V3 cathode, no delay is imposed on the commencement of AVC action, but a positive bias, derived from the drop along R17, will be

applied via the AVC line to V1 and V2, off-setting partly the negative bias obtained from their cathode resistors. Otherwise, R17 provides GB for the triode section of V3.

Resistance-capacity coupling by R14 in triode anode circuit and, in series between anode and chassis, C27, R18, R19 and R20, between V3 triode and pentode output valve (V4, Mullard Pen36C). At this stage gain and tone control modifications and a negative feed-back system are intro-The feed-back voltages are duced. developed across a separate secondary winding on the output transformer T1 and fed via R21 to the coupling resistor R22 which is inserted in the control grid

lead to V4, so that the voltages are fed back from the anode circuit to the grid

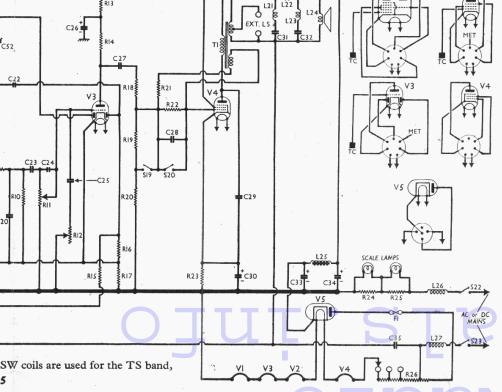
Tone and gain modifications are effected by \$19 and \$20, which form part of the waveband switch group. S20 closes on the SW band, eliminating the negative feed-back action, and \$19 closes on the TS band, short-circuiting R19 and reducing the coupling efficiency between V3 and V4. R21 acts as a buffer, preventing the feed-back secondary winding from becoming short-circuited when \$20 closes for SW operation.

Fixed tone correction by C29 in V4 anode circuit. A special filter circuit comprising L21, L22, L23 and C31, C32 is introduced between the normal secondary winding of T1 and the speech coil to suppress whistles and other interference above 8,000 c/s. The speech coil of the internal speaker has an impedance of 30 Ω , which is higher than usual, but the speech coil secondary of T1 is tapped to make provision for the use of the normal external speaker of about 4 Ω impedance. The switch \$21 permits the internal speaker to be muted, and as one side of the circuit is returned directly to the E socket, the external speaker is safe to handle if a good earth connection is made

When the receiver is operating from AC mains, HT current is supplied by IHC half-wave rectifying valve (V5, Mullard URIC) which acts merely as a low resistance path on DC mains. Smoothing is effected by iron-cored choke L25 and electrolytic condensers C33 and C34.

Valve heaters, together with adjustable ballast resistor R26 and scale lamps (with their shunt resistors R24, R25), are connected in series across the mains input, the scale lamps going in the negative lead between the mains and chassis so that while the switching surge does not over-load them unduly, the heater current through them is augmented by the anode current when the valve heaters warm up.

Fuse F1 in the anode lead to V5 protects the valve in a case of electrolytic breakdown or similar short-circuit, while a section at one end of R26 which is also included in V5 anode lead protects the valve against current surges.



COMPONENTS AND VALUES

	Λ / Λ	
	CONDENSERS	Values (μΙ')
C1 C2	Mains isolating condensers {	0.001
3	S Mains Boldenig condition	0.1
C4	Aerial IF filter tuning	0.00015
C5	Aerial MW coupling	0.001
C6	Aerial capacity swamp	0.001.
07	V1 hept. CG decoupling	0.04
C8 C9	V1 SG decoupling	0·1 0·1
C10	V1 cathode by-pass	0.00005
C11	V1 osc. CG condenser Osc. circuit MW tracker	0.003
C12	Osc. circuit LW tracker	0.0008
C13	Osc. LW fixed trimmer	0.00005
C14) Wi are anode decoupling	0.1
C15*	V1 osc. anode decoupling {	$2 \cdot 0$
C16	V2 CG decoupling	0.04
C17	HT circuit RF by-pass	0.1
C18	V2 cathode by-pass	0.1
C19	IF by-pass condensers	0.0002
C20		0.0002
C21*	V3 cathode by-pass	50.0
C22 C23	Coupling to V3 AVC diode AF coupling to V3 triode	0.000015 0.01
C24	High-note compensator	0.00006
C25	Part of tone control	0.004
C26*	V3 triode anode decoupling	2.0
C27	AF coupling to V4	0.01
$\tilde{C}28$	Feed-back coupling	0.03
C29	Fixed tone corrector	0.004
C30*	V4 cathode by-pass	50.0
C31	Whistle filter tuning con-	0.2
C32	\ \ densers \	0.2
C33*	HT smoothing condensers	8.0
C34*		24.0
C35	Mains RF by-pass B-P pri. LW trimmer	0.1
C36‡	Band-pass pri. tuning	
C381	B-P pri. MW trimmer	
C391	Aerial SW trimmer	
C40	B-P sec. MW trimmer	
C411	B-P sec. LW trimmer	
C42‡	Image suppressor	
C43†	TS, SW and B-P tuning	
C44‡	Aerial TS trimmer	
C45†	Oscillator circuit tuning	
C46‡	Osc. circuit SW trimmer	
C47‡	Osc. circuit MW trimmer	
C48‡	Osc. circuit LW trimmer	
C49‡	1st IF trans. pri. tuning	
C50‡	1st IF trans. sec. tuning 2nd IF trans. pri. tuning	
C51‡	2nd IF trans. pri. tuning 2nd IF trans. sec. tuning	

* Electrolytic. † Variable. ‡ Pre-set.

,	OTHER COMPONENTS	Approx. Values (olims)
L1 L2	Aerial IF filter coil Aerial LW coupling coil	40.0
L3	Band-pass primary coils {	2.5
$_{ m L5}^{ m L4}$	Aerial TS coupling coil	30.0 Very low
$\overline{L6}$	Aerial SW coupling coil	0.4
L7	Aerial TS tuning coil	Very low
$_{L9}^{L8}$	Aerial SW tuning coil	0.05 2.5
L10	Band-pass secondary coils {	27.0
L11	Oscillator TS and SW tun-	
T 10	ing coil	0·05 3·0
$^{ m L12}_{ m L13}$	Oscillator MW tuning coil Oscillator LW tuning coil	9.0
L14	Oscillator TS and SW re-	
	action	0.4
$^{ m L15}_{ m L16}$	Oscillator MW reaction Oscillator LW reaction	0·6 2·0
L17	(Dri	80.0
L18	st IF trans. Sec	60.0
$^{\rm L19}_{\rm L20}$	$\left. \left. \right. \right\}$ 2nd IF trans. $\left\{ \left. \begin{array}{ll} \operatorname{Pri.} & \dots \\ \operatorname{Sec.} & \dots \end{array} \right. \right.$	0.03
L20 L21	Sec	2.5
L22	Parts of whistle filter	5.5
L23)	2.5
$\frac{L24}{L25}$	Speaker speech coil HT smoothing choke	24·0 360·0
L26)	2.0
L27	Mains RF filter coils {	2.0
	Output { Pri Normal sec	320·0 4·0
T1	trans. Normal sec Feed-back sec.	28.0
S1-S20	Waveband switches	
S21	Interval speaker switch	
S22S23 F1	Mains switches, ganged R11 V5 anode fuse, 0.5A	-

6	RESISTORS	Values (ohms)
R1 R2 R3 R4 R6 R7 R8 R9 R10 R11 R12 R14 R15 R16 R17 R18 R19 R20 R21 R22 R24 R25 R26	V1 hept. CG decoupling V1 SG potential divider { V1 fixed GB resistor V1 osc. CG resistor V1 osc. anode stabiliser V1 osc. anode HT feed V2 fixed GB resistor If stopper V3 signal diode load Wanual volume control V3 triode anode decoupling V3 triode anode decoupling V3 triode anode load V3 triode anode load V4 CG resistor V4 CG resistor Feed-back coupling re- sistors V4 GB resistor Scale lamp shunts Heater circuit ballast	250,000 15,000 30,000 250 250 250,000 5,000 250,000 1,000,000 1,500,000 1,000,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 250,000 260,000

† Tapped at $100\,\Omega$ |+ $100~\Omega$ + $400~\Omega$ + $45~\Omega$ from V4 heater end.

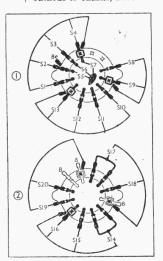
VALVE ANALYSIS

Valve voltages and currents given in the table below are those quoted in the makers' manual. They represent conditions in an average receiver when it is operating from mains of 230 V, with the voltage adjustment properly set, with the receiver tuned to 200 m, but with no signal input.

Voltages were measured with a 1,000

Valve	Anode Voltage (V)	Anode Current (mA)	Screen Voltage (V)	Screen Current (mA)
V1 TH21C	$\begin{cases} 175 \\ \text{Oscil} \\ 135 \end{cases}$	$\begin{pmatrix} 3.5 \\ lator \\ 6.7 \end{pmatrix}$	65	4.8
V2 VPU1	175	6.7	175	.2.8
V3 DTU1 V4 Pen36C	80 160	1·2 39·0	175	5.8
V5 UR1C	200†	38.0	170	_

† Cathode to Chassis, D.C.



Diagrams of the two waveband switch units, as seen from the rear of the underside of the chassis. **B** indicates a blank tag, and **Be** a bearer.

ohms-per-volt meter whose negative lead was connected to chassis.

If V2 should become unstable when measurements are being made of its anode current, it can be stabilised by connecting a non-inductive condenser of about 0.1 μF from grid (top cap) to chassis.

DISMANTLING THE SET

Removing Speaker.—The speaker must be removed before it is possible to remove the chassis.

Unsolder from the terminal panel on the speaker the leads connecting it to

Slacken the nuts holding the four clamps to the speaker rim, and lift out the speaker.

When replacing, the terminal panel should point towards the bottom left-hand corner of the cabinet.

There are only two connecting leads to the speaker, and it is immaterial which way round they are connected to the tags on the speaker.

Removing Chassis.—Remove the speaker as explained above;

remove the two screws (with lockwashers) holding the scale assembly brackets to the top of the cabinet;

remove the four screws (with lockwashers) holding the front and rear of the chassis to the cabinet;

remove the four screws (with lockwashers) holding the vertical supports to the base of the cabinet;

remove the two clamps (nuts and lock-washers) holding the front of the chassis to the sub-baffle.

If the rear is tilted upwards, the chassis may now be withdrawn.

When replacing, several packing pieces (rectangular press-board washers) may be required between the bottoms of the vertical supports and the base of the cabinet to level the chassis squarely and impose an even strain on the plastic cabinet.

Finally, do not omit to re-wax the heads of the screws in the base of the cabinet.

GENERAL NOTES

switches.—\$1-\$20 are the waveband switches, ganged in two rotary units beneath the chassis. These units are indicated in our under-chassis view, where they are identified by numbers and circles, with arrows to show the direction in

Switch Table

				Marine Marine Commission Commissi
Switch	LW	MW	sw	TS
Switch S1 S2 S3 S4 S5 S6 S7 S8 S9 S10 S11 S12 S13 S14			C	C
\$15 \$16 \$17 \$18 \$19 \$20	<u>c</u>	C - C - C - C - C - C - C - C - C - C -	0 0 0 0	0 0

which they are viewed in the diagrams in col. 2, where they are shown in detail. The table (col. 3) gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control spindle when viewed from its free end (control drum lever in bottom position). A dash indicates open, and C, closed.

\$21 is the internal speaker switch, which is mounted at the rear of the chassis near the external speaker sockets, and controlled by a small milled knob. When this is unscrewed, the internal speaker speech coil circuit is broken, thus muting the speaker.

\$22, \$23 are the QMB mains switches, ganged with the volume control R10.

Coils.-L1 is mounted beneath the chassis, and has an adjustable iron core, reached through a hole in the chassis deck. L2, L3, L4, L9, L10 and L11-L16 are in two screened units on the chassis deck. The first of these units contains four trimmers reached through holes in the top of the can. The second contains two trimmers (reached through holes in the top of the can) and the three fixed condensers C11, C12, C13, while the cores of L12 and L13 are adjustable through holes in one side of the can, their positions being indicated approximately in our plan view. L5, L7 and L6, L8 are on small tubular formers, supported directly on their switch units beneath the chassis.

L17, L18 and L19, L20 are the IF transformers in two further screened units on the chassis deck. They contain their associated trimmers, while the second also includes R9, C19 and C22.

The whistle filter coils L21-L23 are on a single former beneath the chassis, and are unscreened.

L25 is the HT smoothing choke, mounted near the centre of the chassis deck, while the mains RF filter coils L26, L27 are wound in a single assembly mounted at one end of the rear chassis member. Fuse F1 is mounted on L25.

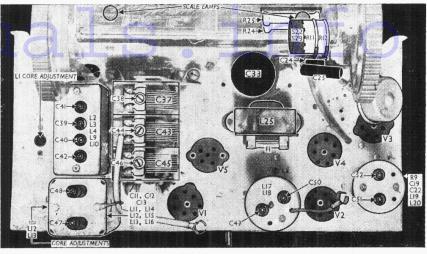
Scale Lamps.—These are two Osram MES types, rated at 6.2 V, 0.3 A. They are shunted by resistors R24, R25 which are mounted on an insulating panel fitted to the chassis deck beneath the scale assembly.

The lamps may be reached for replacement purposes by removing the three small cheese-head screws, at the top of the inside of the cabinet, which hold the moulded escutcheon in place, removing the escutcheon and lifting the hinged scale panel from the bottom.

External Speaker .- Two sockets are provided at the rear of the chassis for a low impedance (4 Ω) external speaker. The internal speaker can be muted by unscrewing \$21.

Condensers C15, C26, C34.—These are three dry electrolytics in a single carton beneath the chassis, with a common negative (black) lead. The yellow leads are the positives of C15 and C26 (both of 2 μF condensers), and the red lead is the positive of C34 (24 μ F).

Condenser's C8, C9.—These are two 0.1 µF paper condensers in a metal-cased unit at the inside of the rear of the chassis. The tag nearest the chassis deck is common to both condensers. The other



Plan view of the chassis. All the pre-set coil and condenser adjustments are indicated with the exception of C36, which is beneath the chassis.

connection of each goes to one of the two tags as shown in the under-chassis view.

Condensers C13, C36.—These are small condensers formed of wires spiralled over insulated wires. C13 is inside the oscillator coil unit, while C36 is beneath the chassis near the switch units. The latter is adjustable by sliding the spiralled winding over the straight wire.

Chassis Divergencies.—In our chassis, V2 CG decoupling condenser C16 was returned to V2 cathode as shown in our circuit diagram, but in the makers' diagram it is shown returned to chassis.

It may also be found in some chassis that the variable tone control components C25, R12 are reversed, C25 going to chassis, and that S21 is connected in the earthed lead to the speech coil L24, instead of going between L22 and L24, as they are shown that way in the makers' diagram. This will not affect the operation of the receiver, but it may lead to trouble when making tests if the alternatives are not expected.

CIRCUIT ALIGNMENT

IF Stages.—Connect signal generator to E socket, and via a 0.02 μ F condenser to grid (top cap) of V1, leaving existing cap in position. Switch set to LW, turn gang to maximum, volume control to maximum, and tone control to "Normal." Feed in a 126.5 kc/s (2,372 m) signal, and adjust C49, C50, C51 and C52 for maximum output.

RF and Oscillator Stages.—See that cursor line covers the 550 m mark when gang is at maximum. Volume control should be at maximum during alignment. Connect signal generator via a suitable dummy aerial to A and E sockets. When adjusting the cores of L1, L12 and L13, the trimmer tool used must be made entirely of insulating material.

TS.—Connect signal generator to A1 and E sockets, and feed in an 18 Mc/s (16.66 m) signal. Switch set to SW, and tune of 18 Mc/s on scale. Fully unscrew C46, then screw it in slowly. Two peaks

will be obtained, of which the first reached is correct. Adjust to this accurately.

Feed in a 20.75 Mc/s (14.3 m) signal (its second harmonic being 41.5 Mc/s), at full generator output. Then switch to TS and adjust C44 for maximum output.

SW.—Switch to SW, feed in a 15 Mc/s (20 m) signal, tune to 15 Mc/s on scale, and adjust C39 for maximum output.

MW.—Switch set to MW, tune to 200 m on scale, and feed in a 200 m (1,500 kc/s) signal. Fully unscrew C47 and then screw it in slowly, adjusting accurately to the first peak reached. Tune to 250 m on scale, feed in a 250 m (1,200 kc/s) signal, and adjust **C40** and C38 for maximum output. Tune to 500 m on scale, feed in a 500 m (600 kc/s) signal, and adjust iron core of L12 for maximum output, while rocking the gang for optimum results. Repeat the adjustments at 200, 250 and 500 m until a small adjustment at one end of the scale does not affect the calibration at the other end.

LW.—Switch set to LW, tune to 1,100 m on scale, feed in a 1,100 m (272.5 kc/s) signal, and adjust C48, C41 and C36 for maximum output. C36 is adjusted by sliding the spiralled wire on the insulating sleeve over the straight

Tune to 1,700 m. on scale, feed in a 1,700 m (176.5 kc/s) signal, and adjust core of L13 for maximum output, while

rocking the gang for optimum results.

IF Filter. — Leaving set tuned to 1,700 m, feed in a 126.5 kc/s signal at full generator output, and adjust core of L1 for minimum output. Reduce generator output, and adjust to 272.5 kc/s. Tune to 1,100 m on scale, and repeat LW alignment as above.

Image Rejector.-Switch set to MW feed in a 1,000 kc/s (300 m) signal at full generator output. Tune receiver to image of generator frequency (about 400 m) and adjust C42 for minimum output.

Tune to 250 m, feed in a 1,200 kc/s signal, and readjust C40 for maximum output.