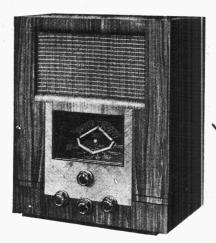
#### "TRADER" SERVICE SHEET

## 737

# PYE MPU/40

### AND MP/UC CONSOLE



The Pye MPU/40 AC/DC superhet.

Pye MPU/40, a SW band (designated SW1) of 13.5-50 m, a medium-short band (SW2) of 50-200 m, covering

the trawler frequencies, and MW and LW bands. The receiver is a 3-valve (plus rectifier) superhet designed to operate from AC or DC mains of 200-250 V, 25-100 c/s in the case of AC.

The MP/UC is a console version of the MPU/40, but its chassis is a little difrerent from that in the table model. The differences, which include another range of valves, are described overleaf.

Release date, both models, 1939.
Original prices: MPU/40, £11 11s.;
MP/UC, £14 3s. 6d.

#### CIRCUIT DESCRIPTION

Aerial input via mains isolating capacitor C1 and coupling coils L1 (SW1), L2 (SW2) and L3 (MW and LW) to single-tuned circuits L4, C32 (SW1), L5, C32 (SW2), L6, C32 (MW) and L7, C32 (LW), Mullard metallised ECH33) operating as frequency changer with internal coupling.

Triode oscillator anode coils L12 (SW1), L13 (SW2), L14 (MW) and L15 (LW) are tuned by C35. Parallel trimming by C10 (SW1), C8, C33 (MW) and C9, C34 (LW); series tracking by C12 (SW1), C13 (SW2) and C14 (MW and LW). Reaction coupling by grid coils L8 (SW1), L9 (SW2), L10 (MW) and L11 (LW).

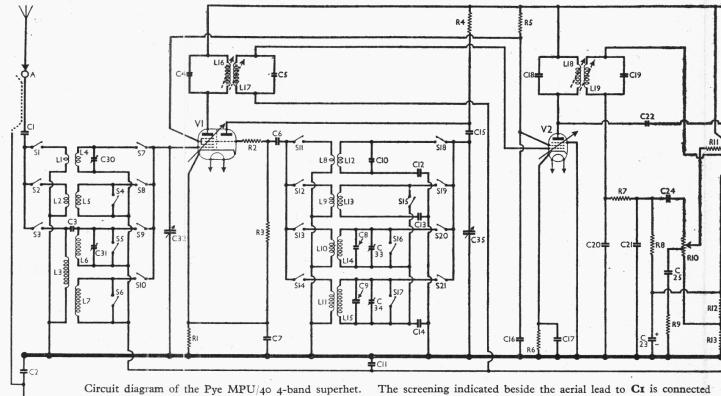
Second valve (V2, Mullard metallised

Second valve (V2, Mullard metallised EF39) is a variable-mu RF pentode operating as intermediate frequency amplifier with tuned-primary, tuned-secondary transformer couplings C4, L16, L17, C5 and C18, L18, L19, C19. All the tuning capacitors are fixed, and the coils of the first transformer are dust-iron cored. Tuning adjustments are made by adjusting the outer sections of the coils to vary their inductance. (See "Chassis Divergencies.")

#### Intermediate Frequency 462 kc/s.

Diode second detector is part of double diode pentode output valve (V3, Mullard CBL31). Audio frequency component in rectified output is developed across load resistor R8 and passed via AF coupling capacitor C24, manual volume control R10 and grid stopper R11 to CG of pentode section.

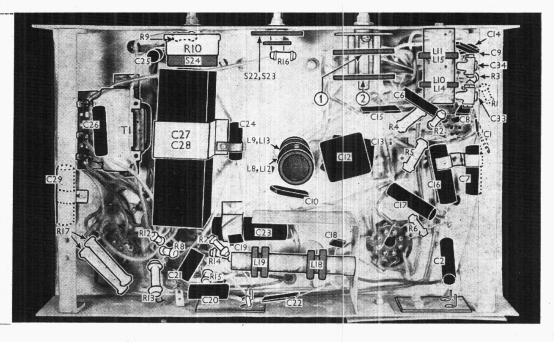
IF filtering by C20, R7 and C21 in diode circuit, and by R11 and the valve capacitance in the control grid circuit. Tone compensation by C25, R9 across the lower half of R10, restoring the bass normally



Circuit diagram of the Pye MPU/40 4-band superhet. The screening indicated beside the aerial lead to CI is connected to the earth socket. The first IF transformer L16, L17 is iron-cored, but the second (L18, L19) is air-cored. In the MP/UC console, the only obvious difference in the circuit diagram is the transposition of L23 from the negative side to the positive side of the HT circuit. Other differences are described in col. 5 overleaf.

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Under-chassis view. The waveband switchunits(marked I and 2) and the tone control unit (S22, S23) are indicated here and shown in detail in the diagrams in cols. 1 and 4 respectively overleaf. The SW oscillator coils are seen in the centre, while the MW and LW coils are mounted beside the waveband switch unit with their associated trimmers and cracker.



lost at low volume levels. Three-position tone control by C26, R16 and S22, S23, either switch closing or neither, according to the required high-note attenuation.

Provision for connection of low impedance external speaker by sockets in the internal speaker speech coil connecting internal speaker may be muted, the ex-

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ternal speaker plugs replacing them.

Second diode of V3, fed from V2 anode via C22, provides DC potential which is developed along load resistor R15 and fed back through decoupling circuit to FC and IF valves on all bands, giving auto-Delay voltage,

together with GB potential for V3 pentode, is obfrom tained  $_{
m the}$ drop along resistors R12, R13 which form a potential divider in the cathode lead to chassis.

When the receiver is operating from AC mains, HT current is supplied by half-wave rectifying valve (V4, Mullard CY31) which, with DC mains, behaves as a low resistance. Smoothing is effected by iron-cored choke L23, the negative HT lead to chassis, and dry electrolytic capacitors C27, C28. The speaker field coil L22 is connected directly across the rectified output, between the cathode and HT negative.

Valve heaters, together with ballast resistor R18 scale lamps, and are connected in series across the mains input circuit. Mains RF filtering is effected by C29, and fuses F1, F2 protect the input circuit against accidental short-circuits.

#### VALVE ANALYSIS

Valve ANALYSIS

Valve voltages and currents given in the tables below are those quoted in the makers' minuals and represent conditions to be expected in an average chassis.

The upper table (table model) was measured with the receiver operating from AC mains of 230 V, using the 220-230 V voltage adjustment tapping, and the lower one (console) with mains of 207 V, using the 200-210 V tapping.

Voltages should be measured with a high-resistance meter whose negative lead is connected to chassis.

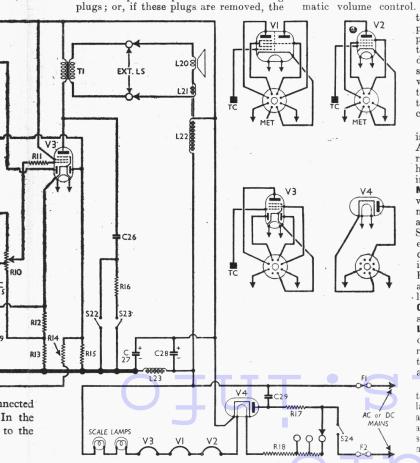
#### Table Model

Valve	Anode Voltage (V)	Anode Current (mA)	Screen Voltage (V)	Screen Current (mA)
V1 ECH33	100	$\left.\begin{array}{c} 1\cdot 4\\ \text{lator}\\ 4\cdot 0\end{array}\right\}$	65	1.6
V2 EF39 V3 CBL31	195 182	4·0 37·5	65 195	$\frac{1\cdot 2}{5\cdot 6}$
V4 CY31†			-	-
† Cathode to				
	Consol	e Mod	el	
V1 TH30C	{ 164 Oscil	$\frac{1.8}{\text{llator}}$	<b>el</b> 60	44
V1 TH30C V2 VP13C V3 Pen40DD	164 Oscil 66 164	1.8		44 2·2 5·2

<sup>\*</sup> Cathode to chassis, 194v, DC.

#### DISMANTLING THE SET

The cabinet is fitted with a detachable bettom, upon removal of which (four wood screws with brass distance-pieces) access may be gained to components beneath the chassis. Removing Chassis.—Remove the four control knobs (recessed grub screws); free the speaker and smoothing choke leads from the cleat on the side of the cabinet; remove the detachable bottom cover described above, revealing the heads of the four bolts holding the chassis to the bottom of the cabinet; remove these bolts (with metal and rubber washers and brass distance pieces, longer than the former ones.



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The chassis may now be withdrawn to the extent of the speaker leads, which is sufficient for normal purposes.

To free chassis entirely, withdraw the speech coil plugs from their sockets at the rear of the chassis and unsolder the two leads from the speaker field tags and the two leads from the smoothing choke L23 on the sub-baile. When replacing, fit a rubber washer to each fixing screw between the chassis and the bottom of the cabinet;

fit a metal washer, then a rubber washer and a brass sleeve to each fixing screw before inserting it in the pole in the bottom of the cabinet.

connect the red lead and the black lead to the two field coil tags (on a separate connecting panel on the speaker);
connect the green lead and yellow lead to the two tags on L23 (on the sub-baffle).

If hum is present when testing, reverse the two connections to the field coil.

Removing Speaker.—Unsolder the two leads from the field coil panel and withdraw the speech coil leads from their sockets at the rear of the chassis;
remove the four screws (with washers) holding the speaker to the sub-baffle.

When replacing, the connecting panels should be at the bottom.

As explained previously, if hum is pronounced

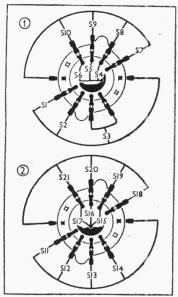
As explained previously, if hum is pronounced on test, reverse the field coil connections,

#### COMPONENTS AND VALUES

	RESISTORS	Values (ohm3)
R1	V1 fixed GB resistor	200
R2	V1 osc. grid stopper	50
R3	V1 osc. CG resistor	20,000
R4	V1 osc. anode HT feed	20,000
$R_5$	V1, V2 SG's HT feed	40,000
R6	V2 flxed GB resistor	200
R7	IF stopper	60,000
$\mathbf{R8}$	V3 signal diode load	500,000
R9	Part bass compensator	60,000
R10	Manual volume control,	00,000
	total	1,000,000*
R11	V3 pent. grid stopper	100,000
R12	V3 pent. GB and AVC de-	150
R13	lay resistors	300
R14	AVC line decoupling	1,000,000
R15	V3 AVC diode load	1,000,000
R16	Part tone control	3,000
R17	Surge limiter	100+
R18	Heater circuit ballast	8008

\* Centre-tapped.

† Two  $200\Omega$  resistors connected in parallel. § Tapped at  $600\Omega + 100\Omega + 100\Omega$  from V4 heater



Diagrams of the waveband switch units, drawn as seen from the rear of the underside of the chassis. The associated table is at the foot of col. 3.

	CAPACITORS	Values =
		(üF)
		(42)
C1	Aerial isolator	0.00026
C2	Earth isolator	0.05
C3	Small coupling	0.000006
C4		0.00009
C5	lst IF transformer tuning { capacitors	0.00009
C6	V1 osc. CG capacitor	0.0001
C7	V1 cathode by-pass	0.1
C8	Osc. MW fixed trimmer	0.00002
C9	Osc. LW fixed trimmer	0.00026
C10	Osc. SW1 trimmer	0.000005
C11	AVC line decoupling	0.000003
C12	Osc. SW1 tracker	0.005
C13	Osc. SW2 tracker	0.0013
C14	Osc. MW and LW tracker	0.000657
C15	V1 osc. anode coupling	0.0001
C16	V1, V2 SG's decoupling	0.0001
C17	V2 cathode by-pass	0.1
C18	2nd IF transformer tuning	0.00014
C20	capacitors	0.00014
C20	)	0.00014
C21	IF by-pass capacitors	0.00015
C22	AVC diode coupling	0.00002
C23*		25.0
C24	AF coupling to V3 pent	0.005
C25	Part tone compensator	0.005
C26	Part tone control	0.05
C27*	)	32.0
C28*		16.0
C29	V4 anode RF by-pass	0.1
C30±	Aerial SW1 trimmer	0.00003
C31 ±	Aerial MW trimmer	0.00003
C32†	Aerial circuit tuning	0 00000
C33†	Osc, circ. MW trimmer	0.00003
C34†	Osc. circ. LW trimmer	0.00003
C35‡	Oscillator circuit tuning	0 00000
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\* Electrolytic. † Variable. † Pre-set.

	OTHER COMPONENTS	Approx. Values (ohms)
L1	Aerial SW1 coupling	0.3
L2	- Aerial SW2 coupling	0.5
L3	Aerial MW and LW coupling	64.3
L4	Aerial SW1 tuning	_
L5	Aerial SW2 tuning	0.3
L6 .	Aerial MW tuning	4.0
L7	Aerial LW tuning	13.7
L8	Osc. SW1 reaction coil	43.0
L9	Osc. SW2 reaction coil	65.0
L10	Osc. MW reaction coil	13.5
L11	Osc. LW reaction coil	20.2
L12	Osc. circ. SW1 tuning	
L13	Osc, circ. SW2 tuning	0.4
L14	Osc. circ. MW tuning	2.5
L15	Osc. circ. LW tuning	3.2
L16	$\left. \left. \right. \right\}$ 1st IF trans. $\left\{ \left. \begin{array}{ll} \operatorname{Pri.} & \dots \\ \operatorname{Sec.} & \dots \end{array} \right. \right.$	7.0
L17	Sec	7.0
L18		10.0
L19	Sec	10.0
L20	Speaker speech coil	2.0
L21	Hum neutralising coil	0.1
L22	Speaker field coil	6,500.0
L23	HT smoothing choke	560.0
T1	Output trans. { Pri Sec	345.0
	Sec	0.3
S1-S21	Waveband switches	
S22 S23	Tone control switches	
S24	Mains switch, ganged R10	
F1,F2	Mains fuses, 1A	

#### **GENERAL NOTES**

Switches.—\$1-\$21 are the waveband switches, ganged in two rotary units beneath the chassis. These are indicated in our under-chassis view by numbers 1 and 2 in circles, with associated arrows showing the direction in which they are viewed in the diagrams in col. 1, where they are shown in detail and identified again by numbers in circles.

The short-circuiting switches like \$4, \$5, \$6, etc., which close always on the next band higher in wavelength to the one actually in use, that is to say, \$4 short-circuits the SW2 band while SW1 is in use, consist of a contact stud attached to a metal plate on the rotor wafer, the plate being connected by a flexible lead

to the AVC line in the case of the aerial circuit, and to the junction of L14 and

L15 in the oscillator circuit.

The table below gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control. A dash indicates open, and C, closed.

\$22, \$23 are the tone control switches, in a three-position unit beneath the chassis. This is indicated in our underchassis view and shown in detail in the diagram in col. 4, where it is drawn as seen from the rear of the underside of the chassis. In the fully anti-clockwise position of the control S22 is closed, giving maximum high-note attenuation; in the centre position, \$22 opens and \$23 closes, giving reduced attenuation; in the fully clockwise position both switches are open.

\$24 is the QMB mains switch, ganged with the volume control R10.

Coils .- The SW1 and SW2 aerial circuit coils L1, L2, L4, L5 are in a tubular unit on the chassis deck with C30 mounted on top. L4 is the thick wire winding, and L1 is interwound with it. The MW and LW aerial coils L3, L6, L7 are in a second unit on the chassis deck, with C31 mounted on top and the small coupling capacitor C3 mounted on the side. All are unscreened.

The SW1 and SW2 oscillator coils L8, L9, L12, L13 are in a tubular unit in the centre of the underside of the chassis, L12 being the thick wire winding and L8 being interwound with it. The MW and LW oscillator coils L10, L11, L14, L15 are in a second tubular unit beneath the chassis with their trimmers mounted directly on them. All are unscreened.

The first IF transformer L16, L17 is mounted on the chassis deck beside V2 holder, and the second one L18, L19 is in a partly screened compartment beneath the chassis. As is explained under "Chassis Divergencies," there are two alternative types of first IF transformer, one with variable dust-iron cores and one with fixed dust-iron cores. Our sample was of the latter type. The second IF transformer is air-cored.

Trimming adjustments are made in both cases in our sample type by softening the wax by heating and moving the outer coils only, to alter the inductance. In the alternative type the first IF transformer (on the chassis deck) is adjusted

#### Switch Table

Switch	SW1	SW2	MW	LW
S1	0   0   0   0   0   0	-		
S2		C	-	
S3			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	С
S4	C			_
S5		С		-
86			C	-
87	C			-
S8		C	-	-
S9	-		C	
S10	-		-	С
S11	С			
S12		C	_	
S13	-	-	С	
S14		_		C
S15	С		-	_ `
S16	- ,	С		-
S17	-		С	-
S18	С			-
S19		0   0   0   0   0   0	C	C     C
S20			С	
S21				C

by means of screws attached to the cores.

The HT smoothing choke L23 is mounted on the sub-baffle, but the output transformer T1 is mounted beneath the chassis.

Scale Lamps.—These are two MES-type lamps, with clear spherical bulbs, rated at 6.2 V, 0.3 A.

External Speaker. — The internal speaker speech coil is connected to the chassis by means of plugs, which have sockets inset at the top for an external speaker, and a pair of sockets at the rear of the chassis. A low impedance  $(2-4~\Omega)$  external speaker may thus be connected so that both speakers operate; or, if the internal speaker plugs are withdrawn from their sockets, those of the external speaker may replace them, muting the internal speaker.

Fuses F1, F2.—These are the standard  $1\frac{1}{4}$  in. glass type, rated at 1 A. They fit into holders mounted on the chassis deck.

Capacitor C3.—This is a small "top" aerial MW coupling, made by winding a thin enamelled copper wire over a thicker one, and it is mounted directly on to the L3, L6, L7 coil unit.

Capacitors C27, C28.—These are two dry electrolytics in a single rectangular waxed cardboard container mounted beneath the chassis. The red lead is the common positive; the brown lead is the negative of C28 (16  $\mu$ F) and goes to the HT negative line; the black lead that of C27 (32  $\mu$ F) and goes to chassis. C28 is rated at 500 V peak working, 600 V surge limiting; C27 is rated at 400 V peak working, 525 V surge limiting. When dealing with a console model it should be borne in mind that this unit has a com-

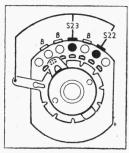


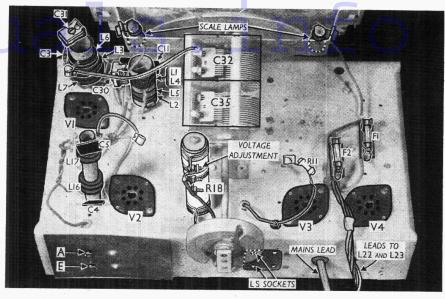
Diagram of the tone control switch unit, as seen from the rear of the underside of the chassis.

mon negative, as explained under "Console Modifications."

Capacitor C23.—This is a dry electrolytic in a tubular cardboard container mounted in a clip inside the second IF transformer screening compartment beneath the chassis. It is rated at 25  $\mu$ F, 25 V working, 35 V surge.

Chassis Divergencies.—The principal difference that may be found in some chassis as compared with our sample is that the first IF transformer may have adjustable dust-iron cores.

This is easily recognisable by its shape, as it then consists of two separate asemblies for primary and secondary windings mounted in a horizontal position on a vertical bracket, with core adjustment



Plan view of the chassis. In some samples, L16, L17 may be mounted in two separate units on a vertical bracket, with screwed core adjustments projecting rearwards.

screws projecting rearwards. In both types the upper winding is the secondary.

In some chassis also, C1 may be  $0.0003~\mu\mathrm{F}$ , instead of  $0.00026~\mu\mathrm{F}$  as in our case, and R17 may consist of two 400  $\Omega$  resistors connected in parallel, instead of two 200  $\Omega$  ones. In some cases, too, the valve range may be the same as that described for the console version.

#### CONSOLE MODEL MP/UC

There are several modifications in the console version as compared with the table model, but the principal differences concern the use of a different range of valves and the transfer of the HT smoothing choke L23 from the negative side of the HT circuit to the positive side.

As a result of the second item, the HT- line goes directly to chassis, and the electrolytic block C27, C28 requires a common negative lead instead of a common positive. It also becomes an 8  $\mu$ F + 8  $\mu$ F unit instead of 16  $\mu$ F + 32  $\mu$ F.

Several changes result from the change of valve range. R5 becomes 20,000  $\Omega$ , and feeds only V1 screen, V2 screen being fed directly from the HT positive line. R6 becomes 150  $\Omega$ , and R7 100,000  $\Omega$ . The valves are all Mullard, their types being quoted in the lower table under "Valve Analysis," and although their heater current rating is the same as for those in the table model, R18 is altered to a total of 650  $\Omega$ , including the two 100  $\Omega$  sections between the three voltage adjustment tappings, to accommolate the change in heater voltage drop.

The intermediate frequency is given in the MP/UC manual as 465 kc/s instead of 462 kc/s as in the table model, and C4, C5 and C18, C19 are all  $0.0001~\mu\text{F}$ .

#### CIRCUIT ALIGNMENT

IF Stages.—Remove the control grid (top cap) connector from V1, connect signal generator leads via a 0.1  $\mu$ F capaci-

tor between the connector and the top cap of the valve, and connect a 500,000  $\Omega$  resistor between the top cap of the valve and the AVC line.

Switch set to MW, tune to 500 m on scale, turn the volume control to maximum, feed in a 462 kc/s (649.4 m) signal, and adjust the outer coils only of L18 and L19, after softening the wax with a soldering iron, for maximum output. A stick of insulating material (dry wood will do) makes a convenient adjusting tool. In the console, the IF is 465 kc/s (645.16 m).

Now adjust L16, L17, using the same method if the transformer is of the same type as ours, or adjusting the core screws if the alternative type is used. Finally, it is advisable to seal the coils again with insulating varnish such as Durofix (the makers recommend British Celanese Solution 202) before leaving them, then remove resistor and replace V1 top cap connector.

RF and Oscillator Stages. — Transfer signal generator leads to A and E sockets, via a suitable dummy aerial. See that the glass scale sits squarely in its clamps, with the central "Pye" motif circle concentric with the pointer spindle. With the gang at maximum, the pointer should be horizontal.

MW.—Tune to 210 m on scale, feed in a 210 m (1,429 kc/s) signal, and adjust C33, then C31, for maximum output. Feed in a 520 m (576.9 kc/s) signal, and check calibration on the scale.

LW.—Switch set to LW, tune to 1,300 m on scale, feed in a 1,300 m (231 kc/s) signal, and adjust C34, gently rocking the gang for optimum results.

SW1.—Switch set to SW1, tune to 15 m on scale, feed in a 15 m (20 Mc/s) signal, and adjust C30 for maximum output, rocking the gang for optimum results. There are no adjustments for the SW2 band.