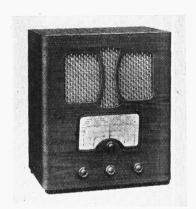
# TRADER SERVICE SHEET A B B A 180

# **3-VALVE AC RECEIVER**



OVERING a short-wave range of 16·5-50 m, the Alba 801 is a 3-valve (plus rectifier) AC 3-band receiver, suitable for mains of 190-250 V, 40-100 C/S. Provision is made for the connection of an extension speaker.

### CIRCUIT DESCRIPTION

Aerial input via coupling coils L1 (SW), plus L2 (MW), plus L3 (LW) to single-tuned circuits comprising L4 (SW), L5 (MW), plus L6 (LW), tuned by C17, which precede variable-mu pentode valve (V1, Mullard metallised VP4B)

operating as RF amplifier with gain control by potentiometer **R2** which varies GB applied. One end of **R2** is connected to the aerial lead so that the aerial circuit is progressively damped as **V1** gain is reduced.

Tuned-secondary transformer coupling by L10, L13, C21 (SW), L11, L14 (MW), plus L12, L15 (LW) tuned by C21, between V1 and pentode detector valve (V2, Mullard metallised SP4B) which operates on grid leak system with C5, R3. C4 removes a peak which occurred on MW, whilst LW coupling coil L12 operates as an RF choke on MW. Reaction is applied from anode by coils L7 (SW), L8 (MW), plus L9 (LW), and controlled by variable condenser C18. RF filtering in anode circuit by C8 (SW) and C3 (MW and LW).

Resistance-capacity coupling by **R6**, **C9** and **R7**, via RF stopper **R8**, between **V2** and pentode output valve (**V3**, **Mullard PenA4**). Fixed tone correction in anode circuit by **C10**. Provision for connection of high impedance external speaker across primary of internal speaker input transformer **T1** 

input transformer T1.

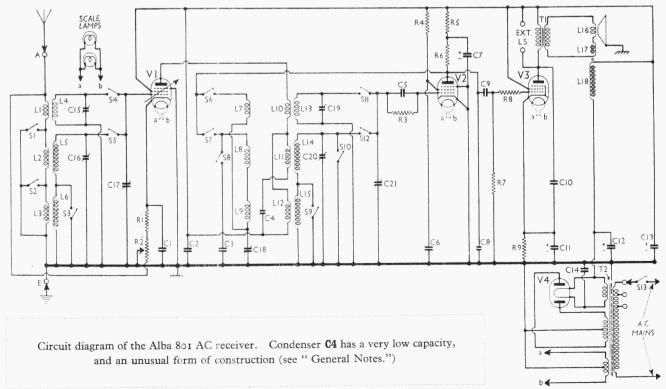
HT current is supplied by full-wave rectifying valve (V4, Mullard DW4/350). Smoothing by speaker field L18 and dry electrolytic condensers C12, C13. RF filtering in rectifier circuit by C14.

### **COMPONENTS AND VALUES**

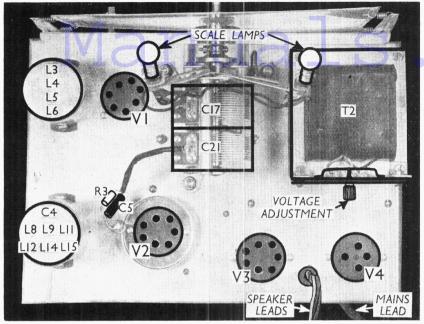
RESISTANCES			Values (ohms)	
Rı	Vi fixed GB resistar			150
R <sub>2</sub>	VI gain and aerial sh	unt co	ntrol	25,000
R <sub>3</sub>	V <sub>2</sub> CG resistance			1,000,000
R4	V <sub>2</sub> SG HT feed			500,000
R5	V2 anode decoupling	g		25,000
R6	V2 anode load			100,000
R7	V <sub>3</sub> CG resistance			250,000
R8	V <sub>3</sub> CG RF stopper			100,000
Ro	V <sub>3</sub> GB resistance			150

		17-1
	CONDENSERS	Values (µF)
		(/ /
Cı	Vi cathode by-pass	0.1
C <sub>2</sub>	HT circuit RF by-pass	O.I
C3	V2 anode MW and LW RF	
	by-pass	0.0002
C <sub>4</sub>	Part of V1 anode MW coupling	
ν'	circuit	Very low
C <sub>5</sub>	V2 CG condenser	0.0001
C6	V2 SG decoupling	0.1
C7*	V2 anode decoupling	2.0
C8	V2 anode SW RF by-pass	0.000012
Co	V2 to V3 AF coupling	0.01
Cio	Fixed tone corrector	0.01
CII*	V3 cathode by-pass	25.0
C12*	HT smoothing	8.0
C13*	(	12.0
C14	V <sub>4</sub> heater RF by-pass	0.002
C15#	Aerial circuit SW trimmer	0.00003
C16‡	Aerial circuit MW trimmer	0.00003
C17†	Aerial circuit tuning	
C18†	Reaction control	0.0001
C19#	RF trans. SW trimmer	0.00003
C20‡	RF trans. MW trimmer	0.00003
C21†	RF trans. sec. tuning	

\* Electrolytic. † Variable. ‡ Pre-set.



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Plan view of the chassis. R3 and C5 are connected in the lead to the top connector of V2.

	OTHER COMPONENTS	Approx. Values (ohms)
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11	Aerial SW coupling coil Aerial MW coupling coil Aerial LW coupling coil Aerial SW tuning coil Aerial SW tuning coil Aerial LW tuning coil SW reaction coil LW reaction coil LW reaction coil RF trans. SW primary RF trans. MW primary	0.6 0.2 40.0 0.05 1.5 9.0 20.0 0.6 1.6 20.0
LI2	RF trans. LW primary	40.0
LI3	RF trans. SW secondary	0.02
LI4	RF trans. MW secondary	1.2
LIS	RF trans. LW secondary	13.0
L16	Speaker speech coil	2.0
Li7	Hum neutralising coil	0.12
L18 Tr	Speaker field coil	1,000.0
11	1 000	0.5
	(Pri., total	53.0
T <sub>2</sub>	Mains Heater sec.	0.3
	trans.   Rect. heat. sec.	0.4
	HT sec., total	500.0
S1-S12	Waveband switches	
SI3	Mains switch, ganged R2	- contains

### DISMANTLING THE SET

Removing Chassis.—To remove the chassis from the cabinet, remove the four control knobs (recessed grub screws) and the four bolts (with washers and rubber washers) holding the chassis to the bottom of the cabinet, when the chassis can be withdrawn to the extent of the speaker leads, which is sufficient for normal purposes.

When replacing, see that there is a rubber washer on each of the chassis bolts, between the chassis and the bottom of the cabinet.

If it is desired to free the chassis entirely, unsolder the speaker leads and when replacing, connect them as follows:-F, blue; 3, black; 1 and F joined, red. The white lead goes to the earthing tag on one of the screws holding the transformer to the speaker frame.

Removing Speaker.—To remove the speaker from the cabinet, unsolder the

leads and remove the nuts from the four ornamentally-headed screws and the two round-head wood screws holding the sub-baffle to the front of the cabinet. When replacing, see that the transformer is on the right and connect the leads as above.

### **VALVE ANALYSIS**

Valve voltages and currents given in the table (col. 3) are those measured in our receiver when it was operating on mains of 228 V, using the 220 V tapping on the mains transformer. The receiver was tuned to the lowest wavelength on the medium band and the volume control

was at maximum, but the reaction control was at minimum. There was no signal

Voltages were measured on the 400 V scale of a model 7 Universal Avometer, chassis being negative.

Valve	Anode	Anode	Screen	Screen
	Voltage	Current	Voltage	Current
	(V)	(mA)	(V)	(mA)
V <sub>1</sub> VP <sub>4</sub> B V <sub>2</sub> SP <sub>4</sub> B V <sub>3</sub> PenA <sub>4</sub> V <sub>4</sub> DW <sub>4</sub> / <sub>3</sub> 50	271 98 252 311†	7.0 1.2 41.0	271 37 271 —	2·8 0·4 6·4

† Each anode, AC.

GENERAL NOTES
Switches.—\$1-\$12 are the waveband switches, in two rotary units beneath the chassis. These are indicated in our under-chassis view, and shown in detail in the diagrams on page IV. The table (page IV) give the switch positions for the three control settings, starting from fully anti-clockwise. A dash indicates open, and C closed.

\$13 is the QMB mains switch, ganged with the gain control R2.

Coils.—L1, L2 and L7, L10, L13 are in two unscreened units beneath the chassis. L3-L6 and L8, L9, L11, L12, L14, L15 are in two screened units on the chassis deck. The latter also contains

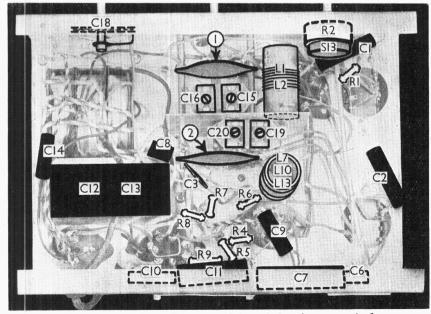
Condenser C4.—This is a small capacity, formed of a pair of wires wound in one of the slots in the lower coil former of the second screened coil unit. Superficially it resembles an ordinary coil, but it can be recognised by the fact that it is wound in the narrowest slot in the lower former, and has a pinkish colour.

Scale Lamps.—These are two Osram

MES types, rated at 6.2 V, 0.3 A.

External Speaker.—Two terminals are provided on the internal speaker connection panel for a high resistance (about 7,000 O) external speaker.

Condensers C12, C13.—These are Continued overleaf



Under-chassis view. Diagrams of the switch units are overleaf.

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## AUTOMATIC TUNING—3A (Continued from page 1)

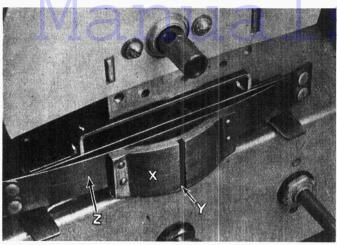


Fig. 2. — The gate mechanism of the new Philco dial. The dial itself has been removed, and the lettered parts are described in the text.

which gives as the dial is swung round until the dog comes opposite the slot. A sharp click is heard as the spring jumps forward, holding the dog firmly into the gate. The gate is so designed that there is practically no displacement sideways when the dog is engaged.

As indicated earlier in this article, great accuracy and freedom from back-lash is essential for the satisfactory operation of a tuner of this type. At a radius of 2 17 in. (the maximum dog radius) a movement of 0.0045 in. produces a displacement of tuning 1 KC/S. This is the maximum that can be tolerated and equals o.009 in. possible movement of the dog, since the tuning can be displaced I KC/S in either direction.

Since a certain amount of play is essential in the push-button bearing to provide easy movement, the maximum permissible play was calculated, and was found to be 0.0045 in., since the ratio of overhang of the dog to the length of its bearing is 1:2.

This, of course, does not take into account possible shake or play in other parts. Thus the accuracy of all parts has to be of a high order, and as an example the push-button has a permissible variation of 0.0005 in. and is actually being made with a variation of 0.0002 in. (two ten-thousandth parts of an inch). human hair is twenty times thicker than

Other points worthy of mention in the dial are the curved stop-plates, which serve the triple function of keeping the manual tuning cord in position, acting as counter balance weights, and providing maximum and minimum safety stops. These are heavy section steel plates,

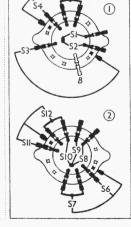
signal, and adjust C20, then C16, for maximum output.

Switch set to SW, tune to 20 m on scale, feed in a 20 m (15 MC/S) signal, and adjust C19, then C15, for maximum

There are no LW alignment adjustments.

### **SWITCH DIAGRAMS**

Switch diagrams, seen from the front of the under-side of the chassis.



### ALBA 801 - Continued

two dry electrolytics in a single carton beneath the chassis, with a common negative (black) lead. The red lead is the positive of C12 (8 $\mu$ F) and the yellow the positive of C13 (12 $\mu$ F).

CIRCUIT ALIGNMENT
With gang at maximum, scale pointer should be horizontal. When aligning, keep gain control at maximum, and reaction control at a point where the set is just short of oscillation. Connect signal generator to **A** and **E** sockets.

Switch set to MW, tune to 200 m on

scale, feed in a 200 m (1,500 KC/S)

### SWITCH TABLE

Switch	sw	MW	LW
Si	C	-	
S1 S2 S3 S4 S5 S6 S7 S8 S9 S10 S11	-	č	
S5 S6	-	C	C
S7	_	C	C
S9	C	C	
SII SII SI2	č	-	_
512		U	C

curved to conform to the dial radius, and are riveted to the dial itself.

The drive cord, which is stretched tight by springs, is located between these plates and a flange on the dial. As they are mounted on the lower half of the dial, they compensate for the extra weight of the upper part, providing static balance. This prevents the dial moving round of its own accord after tuning; as the whole has to be free running, this precaution is very necessary.

Had stops not been provided the gang condenser would be subject to severe knocks at its maximum and minimum capacities, and if any slip occurred between the dial and the gang spindle, all station settings would immediately be upset. To prevent this, little spring check-plates are provided on the gang condenser, which engage with the stop plates so that there is no reaction at all on the gang condenser shaft. This is a complete solution to this form of slip and allows dialling to be carried out without fear of upsetting the adjustment of all the buttons.

On the electrical side, quite apart from questions of stability, it was necessary to arrange for the medium wave and long wave calibrations to line up in such a way that certain buttons could be allotted the dual function of selecting either a medium or long wave station.

As far as electrical stability is concerned. Philco use four special thermal compensating condensers in order to ensure that no noticeable frequency drift occurs during temperature changes at any wavelength. Condensers of this type were described in article 6 of this series (April 16, 1938). Two of these are associated with the RF coils and two with the first IF transformer.

### MAINTENANCE HINT

### More Valve Trouble

N Ultra 22 superhet developed A intermittently a low-pitched crackling noise, on which variation of the volume control had no effect. With a strong station tuned in, the neon tuning indicator column was seen to shorten during the period of crackling, suggesting that the AVC bias was being reduced.

As the noise persisted with the volume control at minimum, the output stage became suspect. All resistors and condensers were checked, and found OK.

A little thinking indicated that a reduction in AVC bias in this case might be caused by a rise in the delay voltage.
A prolonged voltage reading taken from the output valve cathode to chassis, showed that during the period of crackling, the bias voltage increased. An intermittently open grid seemed the possible fault then, but shorting the grid direct to chassis made no appreciable difference to the bias voltage.

The output valve itself then came under suspicion. The grid cap was unsoldered, and the lead from the interior of the valve was found not to have been tinned properly. Retinning and resoldering the cap cured the trouble. The writer has since had many similar cases with various types of valves.—
H. T. COPELAND, KENTON.

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