· TRADER ' **SERVICE** SHEET

PHILIPS 747A (Latest Type)

A N interesting point in the design of the latest Philips 747A receiver is the use of two separate diodes for A.V.C. purposes in order to overcome a form of distortion sometimes found when only one diode is employed. The receiver is a 4-valve (plus rectifier) A.C. 3-band superhet suitable for mains of 100-250 V, 50-100 C/S.

A very similar chassis is fitted in the 747AX receiver but this is arranged so that it can be operated on D.C. mains via a vibrator unit, and has a different mains input plug. In addition a similar chassis is employed in the 68A interesting point in the design of the latest

In addition, a similar chassis is employed in the 698A and 699A radiograms. This Service Sheet was prepared

and oggA radiograms. Ins Service Skeet was prepared on a 747A of the latest type.

It should be noted that some of the first models which were produced had an ordinary output pentode in place of the double diode pentode and do not use two diodes for A.V.C., the circuit being considerably different. These models are not covered here.

CIRCUIT DESCRIPTION

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Aerial input on M.W. and L.W. via coupling coils

12, 13 and condenser C4 to mixed coupled band- pass
filter. Primary coils L4, L5 are tuned by C38;
secondaries L9, L10 by C40. Coupling is effected by
condensers C6 (M.W.), C5 (L.W.) and coils L6, L7
which also form part of a selectivity circuit. On S.W.,
input is via coupling condenser C2 to single-tuned
circuit L8, C40. I.F. filtering by L1, C35 across aerial
circuit

circuit LS, C40. I.F. filtering by LI, C35 across aerial circuit.

First valve (V1, Mullard metallised FC4) is an octode operating as frequency changer with electron coupling. Oscillator grid coils LII (S.W.), LI2 (M.W.) and LI3 (L.W.) are tuned by C41; parallel trimming by C11 (S.W.), C42 (M.W.) and C43 (L.W.), series tracking by C13 (M.W.) and C12 (L.W.). Anode reaction by L14 (S.W.), L15 (M.W.) and L16 (L.W.). Second valve (V2, Mullard metallised VP4B), is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned-primary tuned-secondary transformer couplings C44, L17, L18, C45 and C46, L19, L20, C47.

Intermediate frequency 128 KC/S.

Diode second detector is not part of V3 but is part of double diode pentode output valve (V4, Mullard Pen4DD). Audio frequency component in rectified output is developed across load resistance R13 and passed via manual volume control R17, coupling condenser C20 (and on S.W. C21), variable R.C. tone filter R18, R19, C22, C23 and corrector circuit R20, C24 to C.G. of triode section of double diode triode valve (V3, Mullard metallised TDD4). Operating potential for cathode-ray tuning indicator (T.I., Mullard TV4) is obtained from potential divider R14, R15 across R13.

One diode of V3 is strapped to the cathode; the second, fed from V2 anode via C18, provides D.C. potential which is developed across load resistance E25 and fed back through decoupling circuit as G.B. to I.F. valve, to provide undelayed automatic volume control for this stage. A.V.C. to V1 is delayed, however, by a rather complicated system. The controlling G.B. potential is that at the second (delay) diode of V4 which is positively biased via its load resistance E32. While no signal is being received a very small voltage drop will occur, due to the diode current, as the internal resistance of the diode is low compared with R32. This condition is maintained until the negative potential of V3 A.V.C. diode rises, due to the strength of an incoming signal, to a value sufficient to neutralise, via R26, the opposite polarity of V4 delay diode, after which normal A.V.C. action will occur in proportion to the strength of the signal. On S.W., V1 is not controlled.

Resistance-capacity coupling by R24, C28 and R27 via R29 between V3 triode and pentode section of V4. G.B. for V4 is obtained from drop along R30 in H.T. negative lead to chassis. Fixed tone correction in anode circuit by C31. Provision for connection of itemal speaker transformer T1.

Negative feed-back circuit C32, L21, R33 between secondary of T1 and cathode circuit of V3 is coupled (except on S.W. and Gram.) by R22, L22, S22 short-circuits these two latter on S.W. and Gram. H.T. current is supplied by full-wave rectifying valve (V5, Philips 1821). Smoothing by iron-cored choke L24 and large capacity electrolytic condensers C30, C33.

C30, C33

DISMANTLING THE SET

A detachable bottom is fitted to the cabinet and upon removal (four screws with washers) gives access to most of the under-chassis components.

to most of the under-chassis components.

Removing Chassis.—If it should be necessary to remove the chassis from the cabinet, remove the four control knobs (recessed grub screws, two in each of the large knobs) and the four bolts (with washers) holding the chassis to the bottom of the cabinet. Then unsolder the earthing lead to the screen on the bottom of the cabinet and the leads from the T.I. to the scale lamps, and remove the bracket carrying the T.I. holder (screw with milled head). Now unsolder the leads from the output transformer and speaker.

Next free the scale lamp leads from the two cleats holding them to the sub-baffle and remove the scale assembly (four round-head wood screws with washers), when the chassis and scale assembly can be withdrawn together.

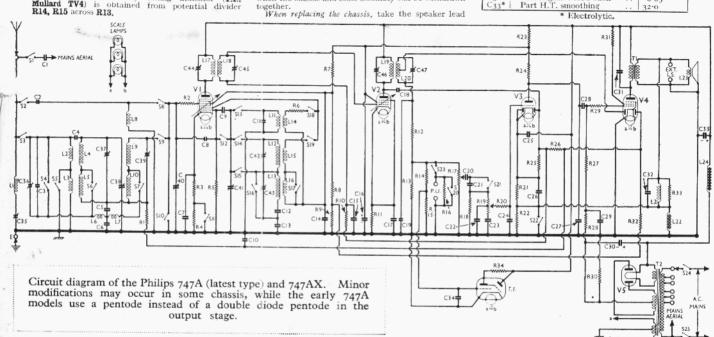
with green paint on it to the secondary contact nearer with green paint on it to the secondary contact nearer the back of the cabinet and to tags I and 2 (numbered from left to right) on the speaker terminal panel. The red-painted lead to the primary should go to the contact nearer the back of the cabinet. Note that the large control knob with a white dot should go on the spindle of the tone control.

Removing Speaker.—To remove the speaker from the cabinet, first remove the chassis, then slacken the four clamps (nuts, lock nuts and washers) holding it to the sub-baffle. When replacing, see that the terminal panel is at the top.

panel is at the top.

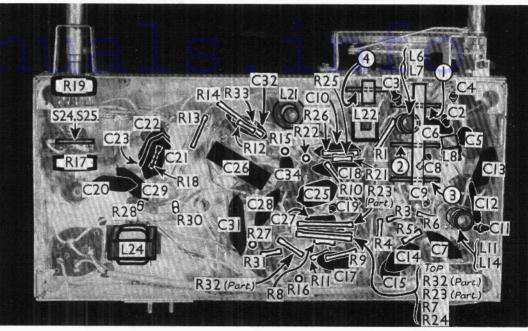
COMPONENTS AND VALUES

CONDENSERS C1 C2 Aerial S.W. series condenser C3 Mains aerial condenser C3 Mey and L.W. aerial coupling C5 C6 C7 C8 C8 C9 C9 V1 cathode by-pass C9 C10 OSc. circuit S.W. trinmer C11 OSc. circuit S.W. trinmer C12 C13 C14 C15 C15 C16 C15 C16 C17 C16 C18 C19			
C2		CONDENSERS	
C2	Cı	Mains aerial condenser	0:0005
C3		Aerial S.W. series condenser	
C4	C ₃	Image suppressor (fixed)	
Color	C4		
C6	C5	1	
C7	C6	Farts band-pass coupling	
C8		Vi cathode by-pass	
C10		Small coupling	
Osc. circuit S.W. trimmer			0.0001
C12			0.1
C13			0.0000064
C14			0.0002
Description			0.00149
C15	C14		
C16*			0.1
decoupling			0.001
C17	C10*	V2 S.G. and V3 triode anode	
Cab			32.0
C19			0.1
C20		Coupling to V ₃ A.V.C. diode	0.00003
C21 S.W. A.F. coupling to V3 triode		I.F. by-pass	
C22 C23 C24 C24 Parts variable T.C. filter 0.00025 0.00025 0.00006 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.001 0.001 0.002 0.003 0.002 0.002 0.002 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.003			0.002
C22 Parts variable T.C. filter 0°00025 C24 Part fixed T.C. filter 0°00064 C25 R.F. by-pass 0°0001 C26* V3 cathode by-pass 50°0 C27 I.F. by-pass 0°0004 C28 V3 triode to V4 A.F. coupling 0°02 C29 V4 C.G. decoupling 0°125 Part H.T. smoothing 32°0 C31 Fixed tone corrector 0°002 C32 Part negative feed-back 0°05 C33* Part H.T. smoothing 32°0	C21	S.W. A.F. coupling to V3	
C23	Can		
C24 Part fixed T.C. filter 0°0003 C25 R.F. by-pass 0°0016 C26* V3 cathode by-pass 50°0 C27 I.F. by-pass 0°0004 C28 V3 triode to V4 A.F. coupling 0°02 C30* Part H.T. smoothing 32°0 C31 Fixed tone corrector 0°002 C32 Part negative feed-back 0°05 C33* Part H.T. smoothing 32°0		Parts variable T.C. filter	
C25 R.F. by-pass 0.0016 C26* V3 cathode by-pass 50.0 C27 I.F. by-pass 50.0 C28 V3 triode to V4 A.F. coupling 0.02 C29 V4 C.G. decoupling 0.125 Part H.T. smoothing 32.0 C31 Fixed tone corrector 0.002 C32 Part negative feed-back 0.05 C33* Part H.T. smoothing 32.0			
C26* V3 cathode by-pass 50-0		P F by page	
C27 I.F. by-pass V. A.F. coupling 0.0004 C28 V3 triode to V. A.F. coupling 0.02 C29 V4 C.G. decoupling 0.125 C30* Part H.T. smoothing 32.0 C31 Fixed tone corrector 0.002 C32 Part negative feed-back 0.05 C33* Part H.T. smoothing 32.0		Va cathoda hu man	
C28			
C20		Va triode to V. A.E. counting	
C30* Part H.T. smoothing		V4 C.G. decoupling	
C ₃₁ Fixed tone corrector 0.002		Part H T smoothing	
C ₃₂ Part negative feed-back 0.05 C ₃₃ * Part H.T. smoothing 32.0	Car	Fixed tone corrector	
C33* Part H.T. smoothing 32.0	C32		
		Part H T smoothing	
	-,,,		34.0



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Under-chassis view. R23 and R32 each consist of two resistors. The four waveswitch change units are indicated, and shown in detail overleaf. **S24** and \$25 are the mains switches, ganged with R17.



	CONDENSERS (Continued)	Values (µF)
C34 C35‡ C35‡ C36‡ C37‡ C38† C39‡ C40† C41† C42‡ C43‡ C45‡ C46‡ C46‡ C46‡	T.I. feed decoupling	0.05 0.00017 0.00003 0.00003 0.00049 0.00003 0.00049 0.00003 0.00003 0.00003 0.000017 0.00017

† \	/ariable. ‡ Pre-set.	
	RESISTANCES	Values (ohms)
Rı	VI pent. C.G. decoupling	100,000
R2	VI pent, C.G. stopper	32
R ₃	Vr fixed G.B. resistance	250
R ₄	Radio muting on gram	10,000
R ₅	Vr osc. C.G. resistance	50,000
R6	VI osc. anode S.W. stabiliser	50
	Parts VI, V2 S.G.'s, VI osc.	
R7	anode, and V ₃ triode anode	10,000
R8	H.T. feed; V4 A.V.C. delay	32,000
R9	diode pos. bias potentio-	64,000
	meter	
Rio	V2 C.G. decoupling	2,000,000
RII	V2 fixed G.B. resistance	400
RIZ	I.F. stopper	250,000
R13	V4 signal diode load	1,600,000
R14	T.I. control potential divider	5,000,000
R15		1,600,000
R16	Pick-up shunt	100,000
Ri7	Manual volume control	500,000
R18	Part of variable T.C. filter	800,000
Rig	Variable tone control, total	600,000
R20	Part fixed T.C. filter	160,000
R21	V ₃ triode G.B. resistance	3,200
R22	Part negative feed-back circuit	20
R23	Part of pot. with R7, R8 and	
Day	R9	10,000*
R24 R25	V3 triode load resistance	100,000
R25	V3 A.V.C. diode load	500,000
1,20	V3 A.V.C. diode and V4 delay diode coupling	Y 000 000
R27	V4 pent. C.G. resistance	1,000,000
R28	V4 pent. C.G. decoupling	500,000
R20	V4 pent. C.G. decoupling V4 pent. C.G. stopper	320,000
R30	V4 G.B. resistance	1,000
R31	V. CC IIT to A	125
R32	V. dolan diada land	9,000,000†
R33	Part negative feed-back circuit	800
R34	TT and TTT food	2,000,000
1.34	1.1. anode H.1. feed	2,000,000

^{*} Two 20,000 O in parallel. † One 5 MO and one 4 MO in serie

	OTHER COMPONENTS	Approx. Values (ohms)	
Li L2 L3	Aerial L.F. filter coil	140.0 40.0 100.0	
L ₄ L ₅ L ₆	Band-pass primary coils	4°5 48·0	
L ₇ L ₈	Band-pass coupling coils Aerial S.W. tuning coil	I.O.	
L ₁₀	Band-pass secondary coils	0.05 4.5 48.0	
LII	Osc. circuit S.W. tuning coil Osc. circuit M.W. tuning coil	0.05	
LI3 LI4	Osc. circuit L.W. tuning coil Osc. anode S.W. reaction coil	35·0 40·0	
L15 L16	Osc. anode M.W. reaction coil Osc. anode L.W. reaction coil	4.5	
L17 L18	st I.F. trans. Sec	135·0 135·0	
L19 L20	and I.F. trans. { Pri Sec., total	135·0 135·0	
L2I L22	Parts negative feed-back { circuit	3.0	
L23 L24	Speaker speech coil	3°5 375°0	
Tı	Speaker input trans. { Pri. Sec	800·0	
T2	Mains trans. { Pri., total Heater sec Rect. heat. sec H.T. sec., total	43.0 0.05 0.15	
S ₁ S ₂ -S ₂₂	Mains aerial switch	245.0	
S23 S24	Gram. P.U. switch		
S25	Mains switches, ganged R17		
	3441345 4514134616		

VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receiver when it was operating on mains of 231 V, using the 220 V tapping on the mains transformer. The receiver was tuned to the lowest wavelength on the medium band and the volume control was at maximum, but there was no

Voltages were measured on the 400 V scale of a model 7 Universal Avometer, chassis being negative.

Valve	Anode Voltage (V)	Anode Current (mA)	Screen Voltage (V)	Screen Curren (mA)
V1 FC ₄ V2 VP4B	265 Oscil 76 265	1.4) lator 1.9) 7.4	82 	4.7
V ₃ TDĎ ₄ V ₄ Pen ₄ DD V ₅ 1821	62 245 275†	34.0	265	6·o

† Each anode, A.C.

GENERAL NOTES

Switches .- \$1 is the mains aerial switch, mounted on Switches.—\$\mathbf{S}\$1 is the mains aerial switch, mounted on a bracket at the rear of the chassis, just above the \$\mathbf{A}\$ and \$\mathbf{E}\$ sockets. Two contacts of the switch unit are blank, while the other two forming the switch are closed when the lever control is moved so as to cover the aerial socket.

82-823 are the waveband and pick-up switches, ganged in four rotary units beneath the chassis. These are indicated in our under-chassis view, and are shown in detail in the diagrams on page viii. There is a good deal of interconnection between the switches, particularly on the fourth unit, which we have indicated

the state of the fourth unit, which we have make the sac clearly as possible.

The table (page viii) gives the switch positions for the four control settings, starting from fully anti-clockwise. A dash indicates open, and **C**, closed.

\$24 and \$25 are the Q.M.B. mains switches, ganged with the volume control R17.

Coils.—L1; L2-L5; L9 L10; L12, L13, L15, L16 and the I.F. transformers L17, L18 and L19, L20 are in six screened units on the chassis deck. All but the fourth of these have a trimmer at the top of their cans. The fourth has two trimmers.

L6, L7; L8; and L11, L14 are on three small un-reened tubular formers beneath the chassis. L21, L22 and L24 are also beneath the chassis.

Scale Lamps.—These are three Philips M.E.S. types with tubular bulbs, type 8042-07.

External Speaker.—Two sockets are provided at the rear of the chassis for a low impedance (5.5 O) external speaker.

Resistances R23, R32.—R23 consists of two 20,000 O resistors in parallel, and R32 of a 4 MO and 5 MO in

Components R2, R20, C24 and R29.—R2 is inside the top cap connector of V1, R20 and C24 are inside the top cap connector of V3, and R29 is inside the top-cap connector of V4.

T.I. Connections.—The TV4 is fitted with a side contact base, with two contacts blank. Starting with the blank contact in the group of four close together, and proceeding anti-clockwise, looking at the underside of the holder, the connections are: 1, blank; 2 and 3, heater; 4, cathode; 5, blank, 6, grid; 7, target; 8, anode.

R34 is connected directly across contacts 7 and 8 on the holder.

V4 Connections.—The Pen₄DD has a 7-pin base with connections differing from usual. The anode and cathode are interchanged, so that pin z is cathode and pin 6 is anode.

Chassis Divergencies.—We have examined circuit diagrams of the 797A and 797AX, and neither agrees entirely with our own chassis, which resembles most nearly the 797AX. The early 797A chassis had an ordinary pentode for \(\forall \)4, and not a double diode pentode, and this, of course, affects the A.F. end of the set considerably.

Some of the values for components do not agree

Continued overleaf

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PHILIPS 747A Continued

with the makers' figures for the 707 AX, but the differences are not important.

R33 may be 320 O. L22 may not be present, and C25 may not be present.

The radiogram models are similar in the main, but again certain component values in the A.F. end may

be different.

be different.

To cover all the divergencies here would be very confusing, and, working from this Service Sheet the competent engineer should not find serious difficulty in following any of the divergent chassis.

CIRCUIT ALIGNMENT

It is not necessary to remove the chassis when aligning; merely place the receiver on its left side, and remove the bottom plate and the back of the cabinet.

cabinet.*

L.F. Stages.—Connect up an earth wire, switch set to L.W., turn volume and tuning controls to maximum. Connect signal generator via a 0·032 μF condenser to control grid (top cap) of Ψ1 (leaving existing top cap connection) and chassis. Feed in a r28 KC/S signal. Connect a 25,000 O resistor and 0·1 μF condenser in series, between top cap of Ψ2 and chassis. Adjust C44 for maximum output. Connect the resistor and condenser between anode of Ψ1 and chassis, and adjust C45 for maximum output. Connect the resistor and condenser across L20, and adjust C46 for maximum output. Connect resistor and condenser between anode of Ψ2 and chassis, and adjust C47 for maximum output.

Seal trimmers with wax, remove resistor and con-denser, and signal generator coupling condenser.

R.F. and Oscillator Stages .- If chassis has not been removed from cabinet, the usual method employing a 15 degree jig cannot be used. In this case, ordinary scale settings may be used, providing calibration is not suspected of being inaccurate.

M.W.-Switch set to M.W., turn volume control to **M.W.**—Switch set to M.W., turn volume control to maximum, and tune to 208 m. on scale. Connect signal generator to **A** and **E** sockets via a dummy aerial, and feed in a 208 m. $(\tau_1.442 \text{ KC/S})$ signal. Connect 25,000 Oresistor and $0\cdot1 \mu\text{F}$ condenser in series between top cap of **V2** and chassis. Adjust **C42**, **C39** and **C37** for maximum output. Re-adjust **C39**, then **C42**, and then seal all three trimmers.

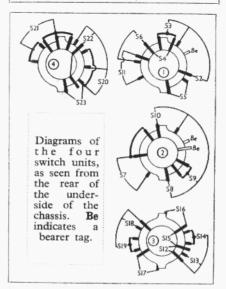
L.W.—Switch set to L.W. Feed in a 395 KC/S (760 m.) signal, tune it in, and adjust **C43** for maximum output, then re-seal.

Image Suppressor.—Switch set to M.W. Feed in a strong 1,000 KC/S (300 m.) signal, tune set to 403 m. on scale, and ajdust C36 for minimum output, then

I.F. Filter.—Switch set to L.W., feed in a strong 128 KC/S signal, turn tuning condenser to maximum, and adjust C35 for minimum output, then re-seal.

SWITCH TABLE AND DIAGRAM

Switch	S.W.	M.W.	L.W.	Gram.
S2 S3 S4 S5 S6 S7	C	C	C	C
S5 S6 S7 S8 S9	C	C		C
S10 S11 S12 S13	C	CCC	CCC	C
S14 S15 S16 S17		C C	C	C
S18 S19 S20 S21	C	CCC	CCC	C
S22 S23	C	-		C C



MAINTENANCE PROBLEMS

Unusual Cause of Distortion

KB397 receiver was received with A the complaint that signals intermittently became very distorted.

On test this was found to be the case. and it was noticed that if the metallising of the detector valve was held with the hand, the distortion would disappear.

This effect seemed to point out bad filtering of R.F. currents to earth, so the chassis was removed and the detector circuit examined, when it was noticed that an extra .ooi µF by-pass condenser had been fitted some time as an extra

This was connected one end to the anode of the detector and the other end was taken to an earthing tag some six inches away.

This looked harmless enough, but the fact that the chassis was subject to hand capacity as well as the valve metallising. showed that R.F. currents were flowing somewhere where they should not!

It was decided to fit the by-pass condenser by its tags straight between anode and cathode of the detector valve, in spite of the fact that the cathode was earthed.

This did the trick, as the distortion disappeared, and neither the valve nor the chassis showed the previous symptoms of hand capacity. Evidently the sixinch earth return lead of the by-pass condenser was radiating R.F. energy and causing the effects mentioned.

I don't know whether other service engineers have had any experience in re-aligning of the cheaper Philips and Mullard models in which the trimmers take the form of small tubes with wire wrapped round the outsides, capacity

being adjusted by winding or unwinding turns. A more fiddling job I have never met. I took the point up with the makers, who, I understand, are bringing it to the notice of the designs section .- R.A.COATES. WHITRY.

SCALE LAMP CONNECTIONS HOLDER C46 C30 VOLTAGE! LEADS MAINS CONNECTOR

Plan view of the chassis. Note the components inside the valve top cap connectors. R34 is connected two of the tags on the T.I. holder. \$1 is the mains aerial switch.

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